

# M11/N11 Corridor Study Needs Assessment Appendices

# **Appendix A**

## **Traffic Modelling Report**



# M11/N11 Corridor Study (J4 M50 – J14 Coynes Cross)

Traffic Modelling Report

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**M11/N11 Corridor Study**

**Final Report**

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## Chapter 1 Introduction

### 1.1 Overview

A Local Area Model (LAM) has been developed to inform the Needs Assessment Report for the M11/N11 Corridor Study on behalf of Transport Infrastructure Ireland (TII). This Traffic Modelling Report (TMR) outlines the development, calibration, validation and traffic projections for the LAM.

### 1.2 Traffic Model Study Area

The study area for the M11/N11 Corridor Study is illustrated in Figure 1.1. The section of the M11/N11 under consideration is approximately 22km in length and encompasses the following:

- M11 from Junction 4 (M50/M11) to Junction 6 (Bray Central); and
- N11 from Junction 6 (Bray Central) to Junction 14 (Coyne's Cross).

The M11 section between the M50 and N11 is at present up to the standard required for a TEN-T road in terms of road quality. However, it is included as part of the needs assessment in order to assess its performance from an operational and capacity perspective.

To the east, the study area is physically constrained by the Irish Sea and to the west by the Wicklow Mountains. As a result there is no comparative north-south alternative to the M11/N11 corridor while east-west crossings are also limited. The study area lies within the functional areas of:

- Dun Laoghaire – Rathdown County Council (DLRCC); and
- Wicklow County Council (WCC).

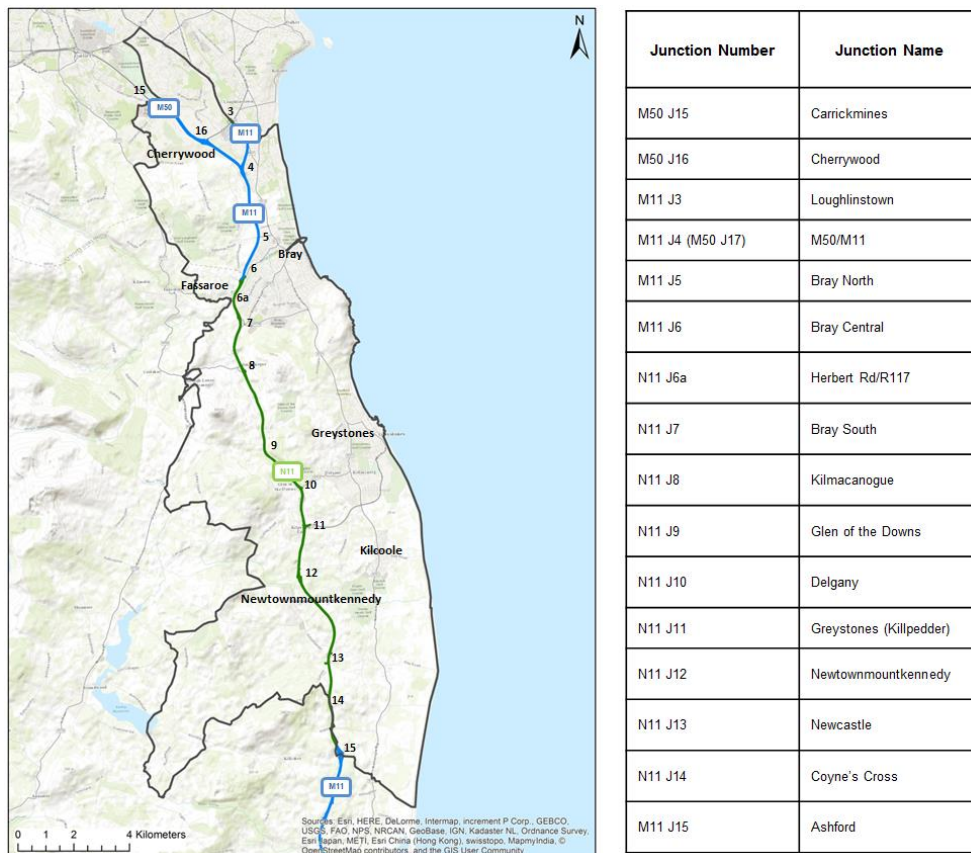


Figure 1.1: M11/N11 TEN-T Corridor Model Study Area

## Chapter 2 Data Collection

### 2.1 Introduction

In order to develop a Traffic Model, a significant level of traffic data is required to ensure that the model can replicate existing traffic patterns and volumes. This section of the TMR describes the collation of traffic data for the construction of the Base Year (2015) M11/N11 Local Area Model.

### 2.2 National Transport Model

The starting point for the development of the Base Year LAM was the 2013 Base Year National Transport Model<sup>1</sup> (NTpM), which was developed by Transport Infrastructure Ireland (TII). The NTpM is a strategic multi-modal variable demand model used by TII to assess the impact of infrastructure or policy changes at National, Regional and local level. Within the NTpM there are four modules, which are as follows:

- National Traffic Model (NTM);
- National Rail Model (NRM);
- National Bus Model (NBM); and
- Variable Demand Model (VDM).

The three assignment models (NTM, NRM & NBM) are used to assign the demand for travel represented by the demand matrices to the network, generating travel costs (e.g. time, distance, tolls, fares) for each mode. A brief overview of the Variable Demand Model is provided in the following section.

The role of the Variable Demand Model (VDM) is to assess, if required, the impact of a change in the transport network or change in the cost of travel (e.g. fuel costs, fares) upon the demand for travel (mode switching, induced demand etc.). Table 5.1.1 of PAG Unit 5.1: Construction of Transport Models provides guidance on when variable demand modelling is required.

The VDM operates at a national level as it requires the full cost of a trip between an origin and destination; therefore any assessment of potential demand responses arising from major schemes proposed within the M11/N11 study area is undertaken within the NTpM and not the LAM. However, any demand responses identified as a result of the proposed scheme are incorporated into the LAM using demand matrix adjustment techniques during the ensuing analysis.

### 2.3 National Traffic Model

The starting point in the development of the Base Year M11/N11 LAM was the 2013 Base Year National Traffic Model (NTM), which was developed by TII. The NTM is a strategic (macroscopic) traffic model developed using the transportation modelling software VISUM. The model covers the entire National and Regional road network and is used by TII as a tool in the appraisal of potential road schemes, land-use proposals and policy changes. The NTM provides demand data for Light (Car & LGV) and Heavy (OGV1, OGV2 and PSV) vehicles for the following time periods:

- Average AM Peak Hour (07:00 – 09:00); and
- Average Inter Peak Hour (12:00 – 14:00).

The NTM model also provides the basic road network for use in the M11/N11 model.

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<sup>1</sup> TII National Transport Model documentation - <http://www.tii.ie/tii-library/strategic-planning/>

## 2.4 Traffic Surveys

In order to complete the study, a substantial quantum of traffic survey was commissioned within the study area. A summary of the traffic survey data that was collated, as part of the development of the 2015 M11/N11 model, is outlined below:

- 18 Automatic Traffic Counts (ATC) on major links within the local road network carried out between Monday 18<sup>th</sup> and Sunday 24<sup>th</sup> of May 2015 including 14 ATC link counts on the M11/N11 and 4 on R761;
- Origin-Destination (O-D) surveys were carried out on Thursday 14<sup>th</sup> May 2015 at 9 sites from N11 J6 Bray Central to J7 Bray South between 07:00 – 19:00;
- 35 junction turning counts at major junctions within the study area undertaken on Wednesday 13<sup>th</sup> May 2015 from 07:00 – 19:00;
- Traffic data from 4 TII Traffic Monitoring Units was also examined as part of the model development; and
- A significant quantum of journey time data was also collated using the O-D points shown in Figure 2.1 below.

Figures 2.1 to 2.5 illustrate the location of the traffic surveys.



Figure 2.1 – M11 / N11 Automatic Traffic Counts on major links at OD site locations.



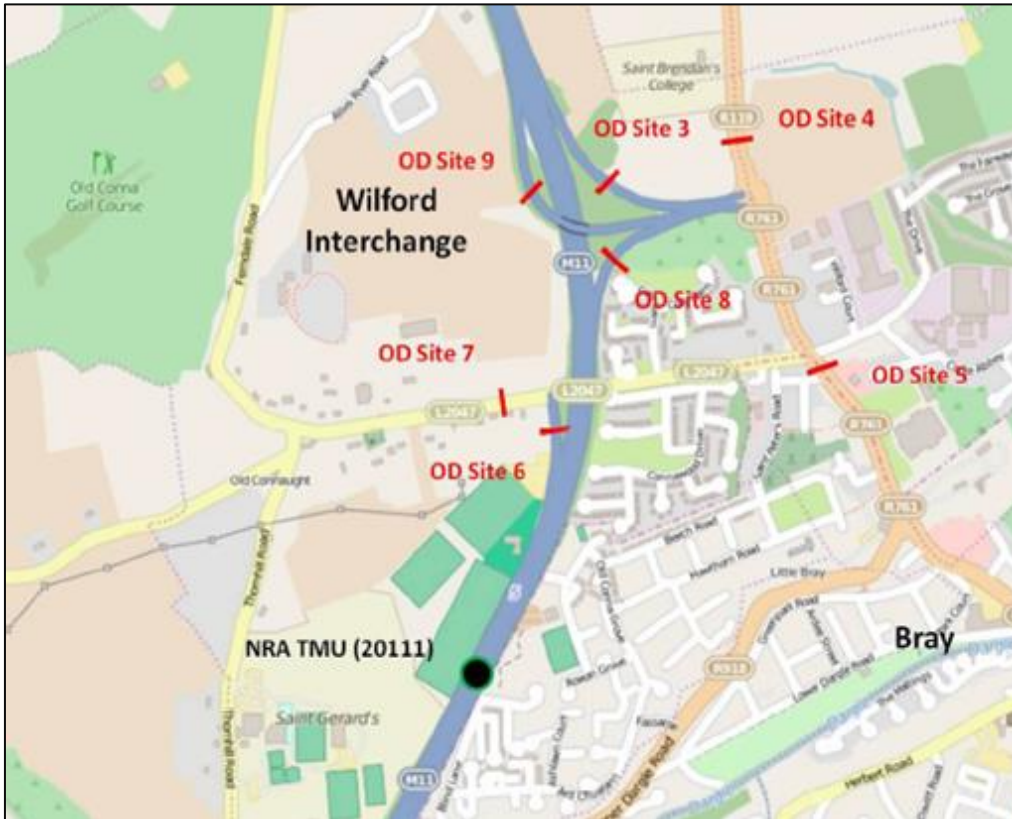


Figure 2.2 – M11 / N11 Automatic Traffic Counts on major links at OD site locations

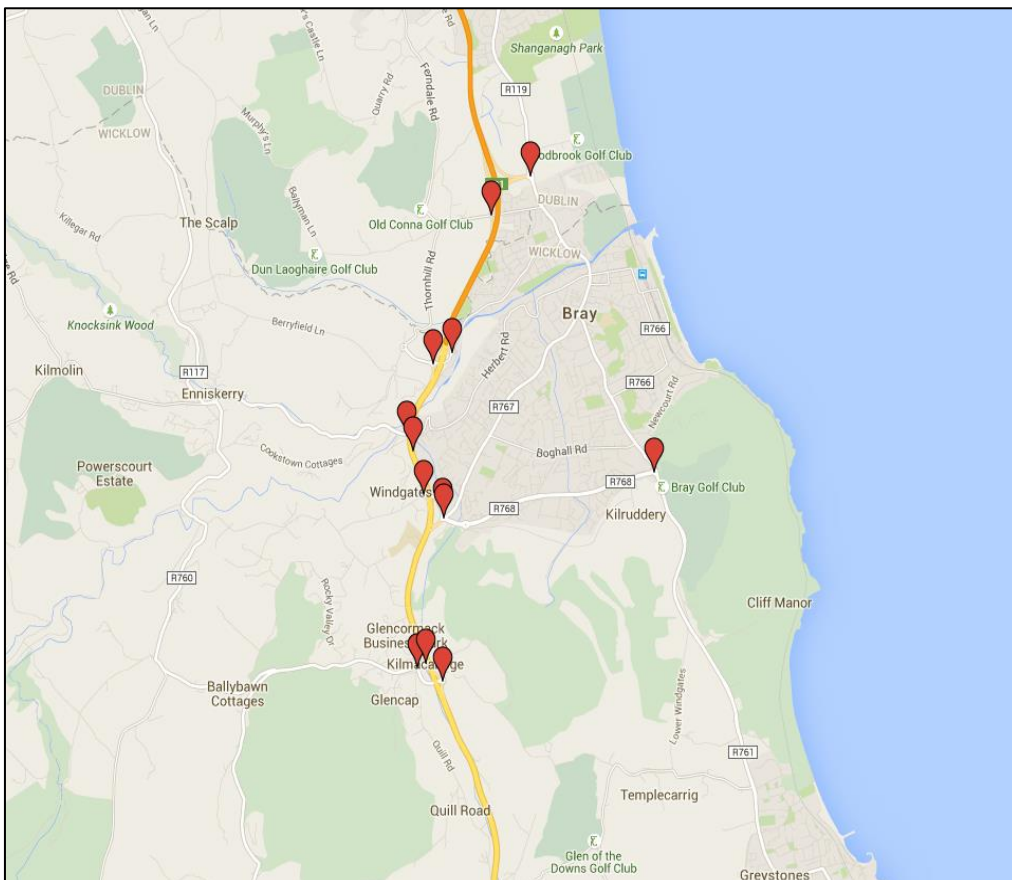


Figure 2.3 – M11 / N11 Traffic Counts at Major Junctions (Study Area North)

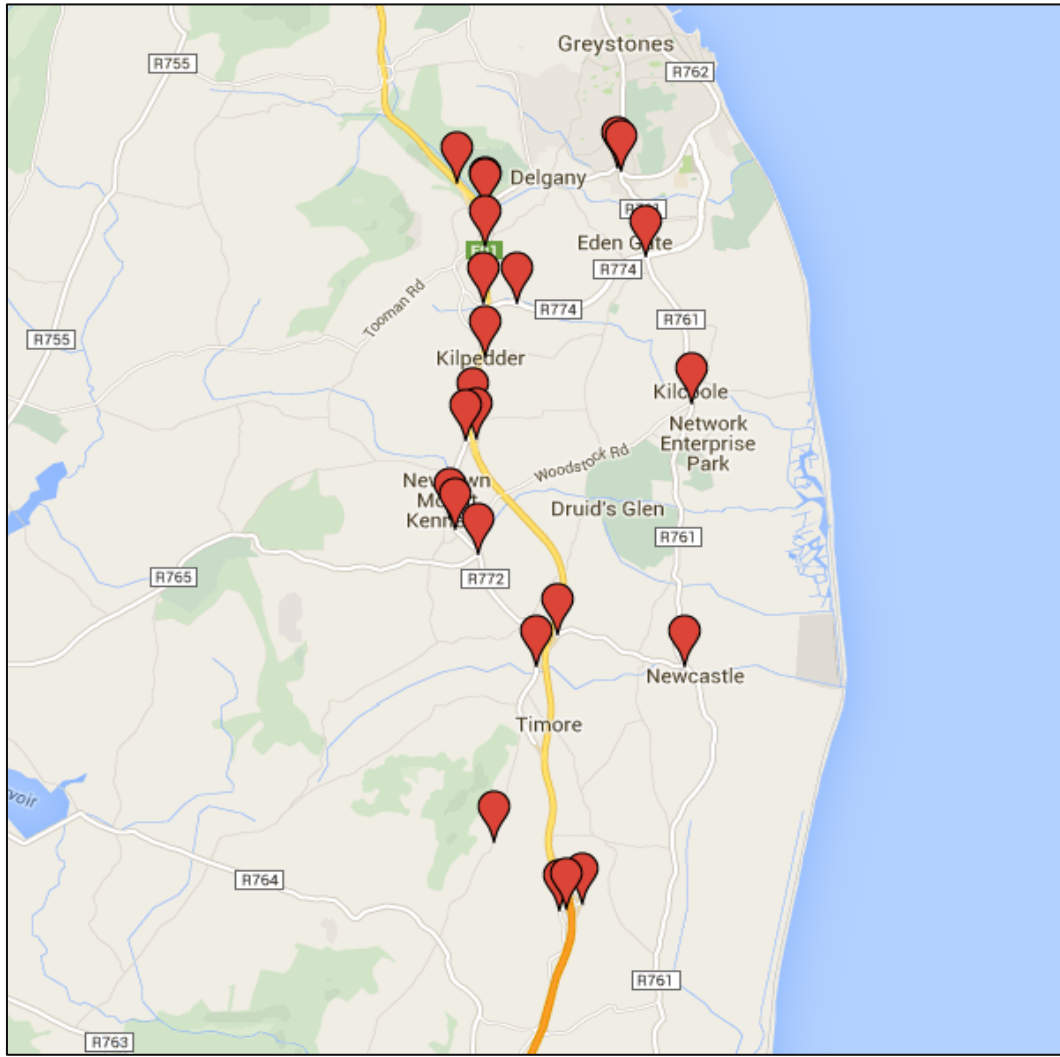


Figure 2.4 – M11 / N11 Traffic Counts at Major Junctions (Study Area South)

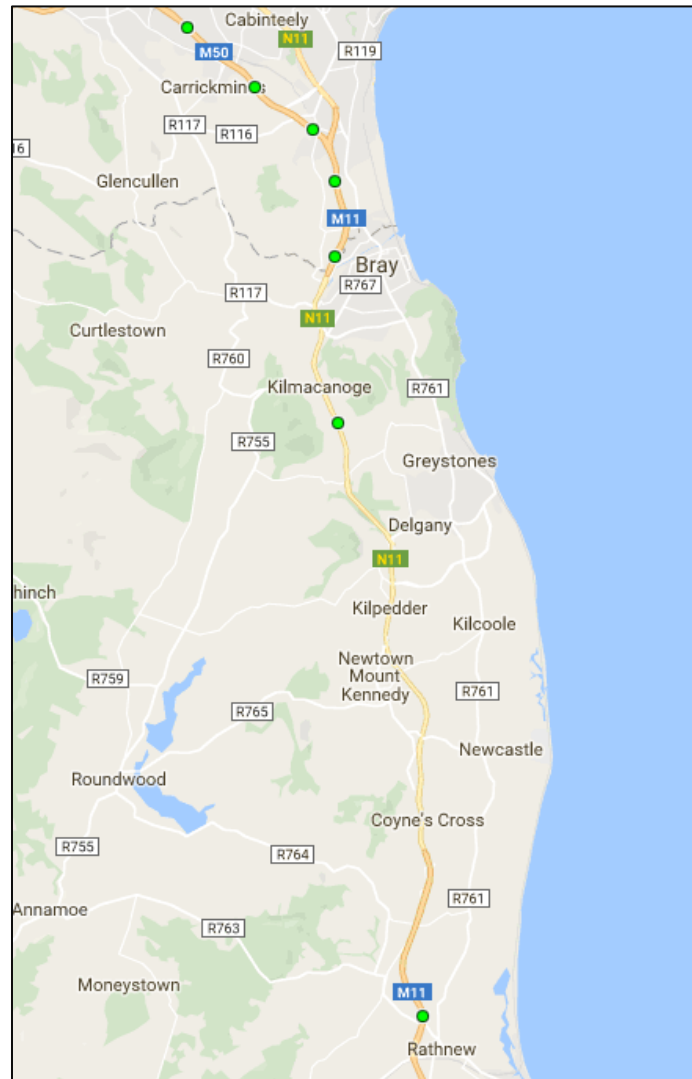


Figure 2.5 – TII TMUs within the M11/N11 Study Area.

## 2.5 An Post GeoDirectory

An Post supply a geocoded dataset which shows the location of each residence and commercial property in Ireland. The dataset was utilised to assist in the zone splitting process. Figure 2.6 below shows the location of every residence (shown as a red dot) and commercial property (shown as a blue dot) within the study area.

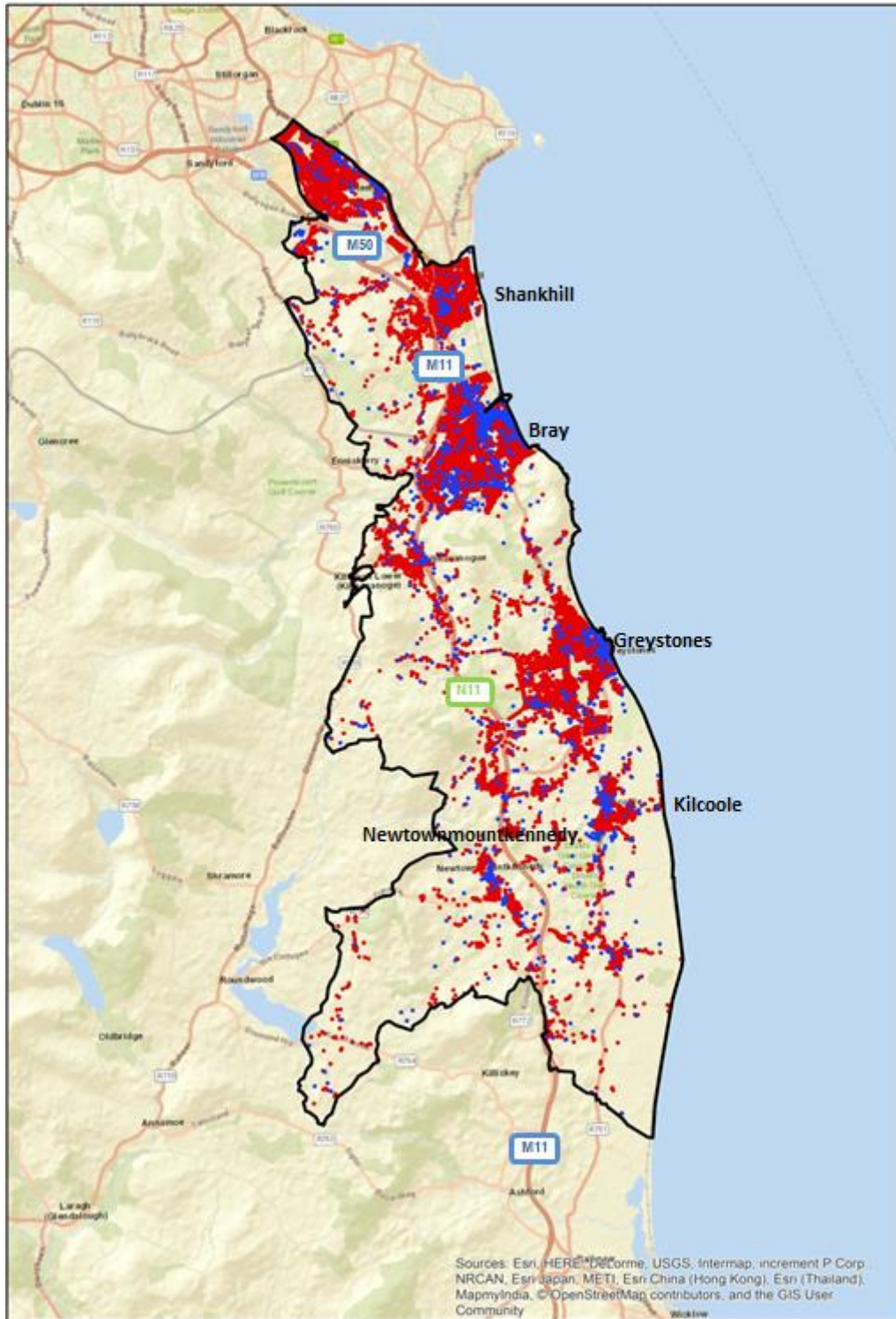


Figure 2.6 – An Post Geocoding Information in the M11/N11 Study Area

## Chapter 3 Model Development

### 3.1 Overview

This section of the report describes the development, calibration and validation of the 2015 M11/N11 LAM's which were developed for the following time periods:

- AM Peak Hour (08:00 – 09:00); and
- PM Peak Hour (17:00 – 18:00).

Assignment (fixed demand) models were developed using VISUM (V15.00-07).

### 3.2 Network Development

The TII NTpM was used as a starting point for developing the M11/N11 LAM's. The initial step was to identify the extent of the study area for the LAM. The likely area of influence was identified and cordoned out of the 2013 NTM.

#### 3.2.1 Refinement of the LAM Road Network

Once the study area had been cordoned from the NTM, the road network was further refined to reflect the 2015 road network conditions (i.e. inclusion of further detail such as speed limits, banned turns, addition of local road links between the N11 corridor and the R761, lane provision at junctions etc.). This information was collected through site observations and aerial mapping. The resultant 2015 LAM network is illustrated in Figure 3.1.

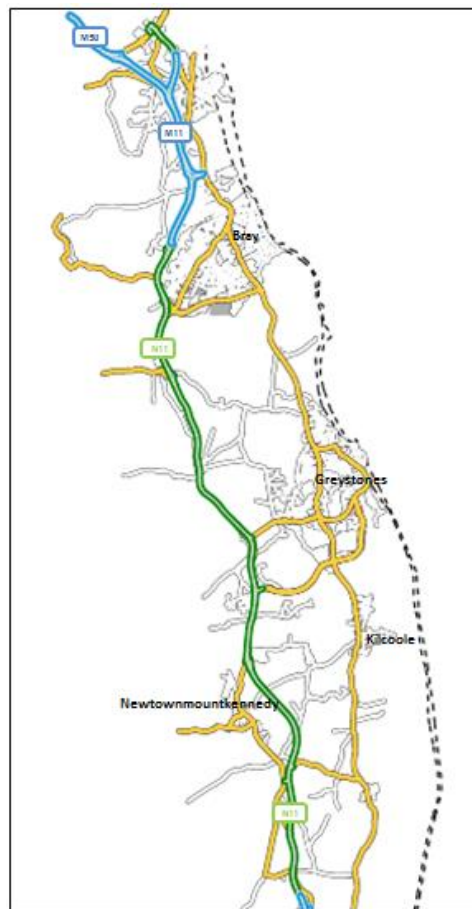


Figure 3.1 - Refined M11/N11 Road Network

3.2.2 Refinement of the LAM Zone Structure

In order to obtain suitable detail within the M11/N11 LAM, a more detailed zoning system than that used in the NTM was required. The zoning system in the NTM is based on the aggregation of Electoral Divisions (EDs), which are quite large for a more local study of the M11/N11 corridor (Figure 3.3). The refined zoning system in the LAM is shown in Figure 3.2.

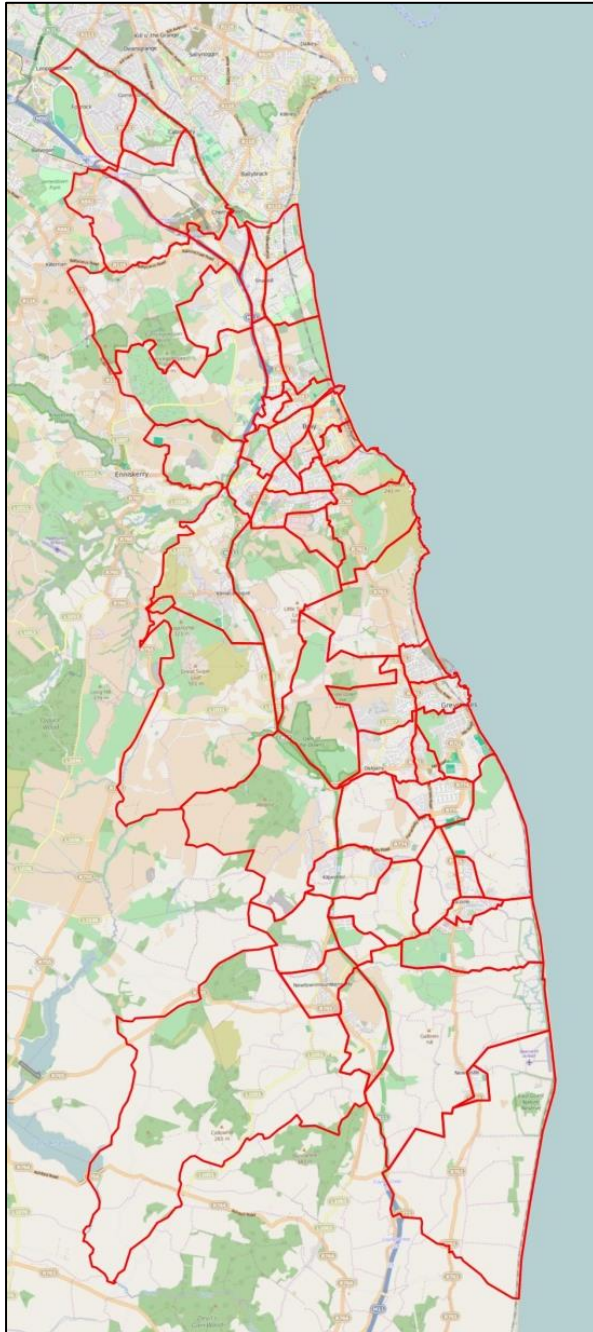


Figure 3.2 – LAM Zone Structure



Figure 3.3 – NTM Zone Structure

This initial zone splitting process was undertaken based on An Post geocoding information. The An Post data shows the location of postal address points (both residential and commercial) and formed the basis for allocation of trip ends for larger zones into relevant subzones and is shown in Figure 2.6 of the previous chapter.

The original model cordoned from the NTM contained 19 zones, which included 4 internal zones and 15 external zones. The disaggregation of the various zones (shown above), produces a model containing a total of 72 zones, including 57 internal zones and 15 external zones, as shown In Figure 3.4 below.

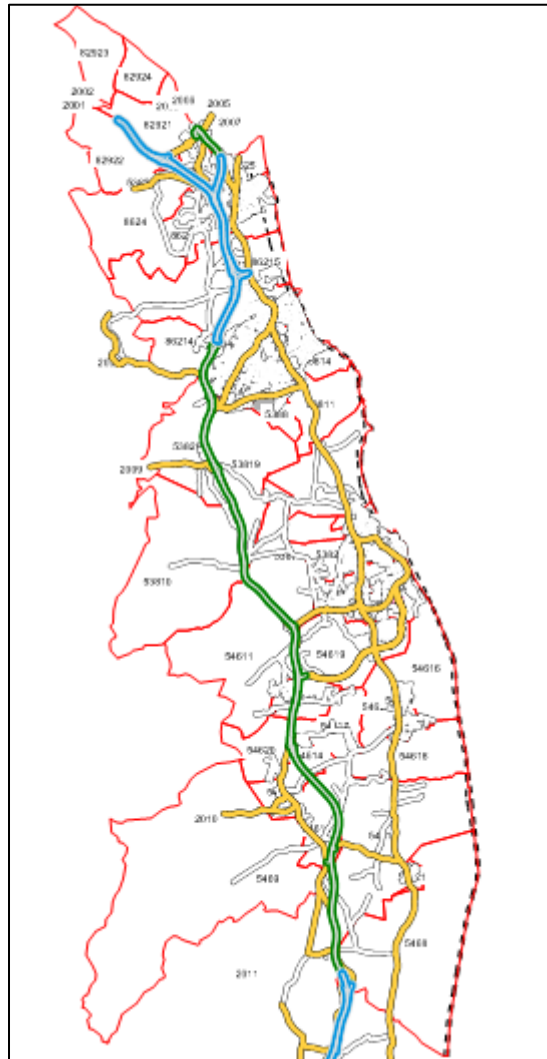


Figure 3.4 - Refined M11/N11 zoning system

### 3.2.3 Link Travel Times

The total travel time of a trip from origin to destination is a function of both link travel time and junction delay. Link travel times in the network are determined by a predefined volume-delay function (VDF) in VISUM, which describes the relationship between current traffic volumes (q) and the capacity of the link (qmax). The VDF used in this model is based on the Bureau of Public Roads 3 (BPR 3) function:

$$t_{cur} = \begin{cases} t_0 * (1 + a * sat^b) & , \text{ if } sat \leq sat_{crit} \\ t_0 * (1 + a * sat^b) + (q - q_{max}) * d & , \text{ if } sat > sat_{crit} \end{cases}$$

where:  $t_0$  = free flow travel time (based on link length (km and free flow speed ( $v_0$ ))  
 $sat = q / (q_{max} * c)$

The VDF function is globally applied to all links in the network as the capacity (q) and free flow speed (v0) of each link (input during network development) feed directly into the VDF. A VDF is applied to each link classification in the model based on adjusted a, b, c and d parameter values which reflect the quality of that road type.

### 3.2.4 Junction Delay

Delay at all junctions is calculated using the Turns Volume-Delay method, which considers the free-flow turning travel time (t0) of each turn.

### 3.2.4 Matrix Development

The following time periods have been developed for the M11/N11 traffic model:

- Morning peak from 08:00 – 09:00 (AM Peak Period); and
- Evening peak from 17:00 – 18:00 (PM Peak Period).

'Prior' AM Peak and PM Peak hour Light and Heavy vehicle matrices were cordoned from the 2013 NTM. The matrices were disaggregated or split to provide a more refined LAM zoning system as discussed in Section 3.1.2 above. The process of zone splitting was undertaken using VISUM, whereby origin and destination trip ends were allocated to the sub-zones based on An Post geocoding information supplied by Wicklow County Council whilst maintaining the equivalent distribution of the larger zones. The An Post data shows the location of postal address points and formed the basis for allocation of trip ends for larger zones into relevant subzones.

The resultant 'Prior' matrices were then adjusted during the calibration process using matrix estimation methods to reflect 2015 demand.

Each of these matrices were then modified during the calibration process using the 2015 traffic survey data ascertained for each peak, using the select link analysis tool in VISUM. Further information on the calibration process is provided in Chapter 4.

## 3.3 Assignment Model

The assignment model applies the demand for travel, represented by the trip matrices, to the supply, in the form of the road network. The 'generalised cost' of a journey, represented by a combination of time and distance, is compared in a route choice algorithm, and a stable output produced, where ideally, all possible routes between an origin and destination have the same 'cost'. Generalised cost is computed as follows:

$$\text{Generalised Cost} = \text{Value of Time} * \text{Time} + \text{Vehicle Operating Cost} * \text{Distance}$$

The economic parameters used in the M11/N11 traffic model are outlined in Table 3.1. These are fully compliant with parameters set out in PAG and in the DTTAS Common Appraisal Framework.



Table 3.1: Generalised Cost Economic Parameters (2015)

| Peak hour | User Class | Value of Time (VoT)* |       | Vehicle Operating Cost (VOC) |       |
|-----------|------------|----------------------|-------|------------------------------|-------|
|           |            | Cents/sec            | €/hr  | Cents/metre                  | €/km  |
| AM and PM | Car        | 0.5280               | 19.01 | 0.0103                       | 0.103 |
|           | HGV        | 0.9032               | 32.51 | 0.0416                       | 0.416 |
| Inter     | Car        | 0.5161               | 18.58 | 0.0101                       | 0.101 |
|           | HGV        | 0.9319               | 33.55 | 0.0370                       | 0.370 |

\*Average 2015 VoT for Commuting, Working & Non-Working Trip Purposes

For the purpose of the assignment in the VISUM software, a scalar of 1000 is applied to the VoT and VOC. The Route Choice Algorithm selected is based on Equilibrium Lohse. This starts with an 'all or nothing' assignment, and assigns in an iterative fashion, with drivers consecutively including information gained during their last journey for the next route choice. The assignment terminates when a stable solution is calculated.

## Chapter 4 Model Calibration

### 4.1 Introduction

Following the development of the base year models, the process of calibrating and validating the models was undertaken.

### 4.2 Calibration

The purpose of model calibration is to ensure that the model assignments reflect the existing travel situation. Calibration is an iterative process, whereby the model is continually revised to ensure that the most accurate replication of the base year conditions is represented.

### 4.3 Matrix Estimation

Matrix Estimation (ME) is the process in which the number of trips assigned along a model link is adjusted to match an observed total. Using transportation modelling software (VISUM in this case) it is possible to perform this operation at numerous locations in a single matrix estimation run, adjusting large sections of the trip matrix to match observed demand.

“TFlow Fuzzy” is the matrix estimation tool provided in VISUM, designed to automatically adjust trip matrices to match modelled volumes to observed volumes along multiple links or turns. Prior to the TFlow Fuzzy process, numerical parameters are set to form tolerance values, calculated as a percentage of the observed volumes, in order to ensure accuracy within the matrix estimation process.

The subject models were calibrated utilising flow bundle analysis, whereby flow bundle matrices were extracted, examined and subsequently adjusted to match observed flows up and downstream of the point at which the flow bundle was taken.

#### 4.3.1 Calibration Criteria and Link Flow Calibration Results

The model calibration process has been undertaken based on the requirements of the TII *PAG Unit 5.2: Construction of Traffic Models* and with reference to the calibration criteria outlined in Table 5.2.2 of that document. The PAG specify the acceptable values for modelled and observed flow comparisons and suggests how calibration should relate to the magnitude of the values being compared. A summary of these targets is shown in Table 4.1.

Table 4.1 - Model Calibration Criteria: Individual Flows

| Class Test | Criteria and Measures                                |  | Guideline      |
|------------|--|--|----------------|
|            | <i>Assigned Hourly Flows vs. Observed Flows:</i>     |  |                |
| 1          | Individual flows within 100 vph for flows <700 vph   |  | > 85% of cases |
| 2          | Individual flows within 15% for flows 700 – 2700 vph |  |                |
| 3          | Individual flows within 400 vph for flows > 2700     |  |                |

The standard method used to compare modelled values against observations on a link, involves the calculation of the Geoff E. Havers (GEH) statistic (Chi-squared statistic), incorporating both relative and absolute errors. The GEH statistic is a measure of comparability that takes account of not only the difference between the observed and modelled flows, but also the significance of this difference with respect to the size of the observed flow. The GEH statistic is calculated as follows:

$$GEH = \sqrt{\frac{(M - O)^2}{0.5(M + O)}}$$

Where *M* = Modelled Flow and *O* = Observed Flow.

Guidance in the Project Appraisal Guidelines sets out the following criteria shown in Table 4.2.

Table 4.2 - Model Calibration Criteria: GEH Values

| Criteria and Measure |                           | Requirement    |
|----------------------|---------------------------|----------------|
| GEH statistic        | Individual flows: GEH < 5 | > 85% of cases |

A total of 23 links flows were used in the calibration process, the results of which are summarised in Tables 4.3 and 4.4. The results in full can be found in Appendix A of this report.

Table 4.3 - Link Calibration Results: Individual Flows

| % of Calibration Sites Meeting Individual Flow Criteria |               |        |         |          |
|---|---------------|--------|---------|----------|
| Time Period   | Link Flows    |        |         | Required |
|   | Total Traffic | Lights | Heavies |          |
| AM Peak   | 100%          | 100%   | 100%    | >85%     |
| PM Peak   | 100%          | 100%   | 100%    | >85%     |

Table 4.4 - Link Calibration Results: GEH Values

| % of Calibration Sites with GEH < 5 |               |        |         |          |
|-------------------------------------|---------------|--------|---------|----------|
| Time Period                         | Link Flows    |        |         | Required |
|                                     | Total Traffic | Lights | Heavies |          |
| AM Peak                             | 91%           | 96%    | 100%    | >85%     |
| PM Peak                             | 96%           | 96%    | 96%     | >85%     |

The comparison of modelled and observed flows demonstrates that the AM and PM Peak period models match the flow criteria for all user classes. Likewise, the GEH results show that the AM Peak and PM Peak period models also match the criteria for all user classes. The results therefore confirm that the models have been calibrated to a standard compliant with the PAG criteria for all user classes and all time periods.

#### 4.3.2 Trip Length Distribution

The output trip matrix from the matrix estimation process must be checked to ensure that the process has not significantly altered trip distance distribution. It is possible that in seeking to increase the flow along a particular link, the matrix estimation process might add significant numbers of trips between the two zones at either end of the link in question. This could have the effect of creating excessive short distance trips while longer distance trips are unaffected, which in turn would push the trip distance distribution toward short trips.

To check the output of the matrix estimation process, the trip length distributions (TLD) from before (pre) and after (post) matrix estimation are compared. The trip length distributions for each peak hour for Light Vehicles are represented as histograms in Figure 4.1 to 4.2.

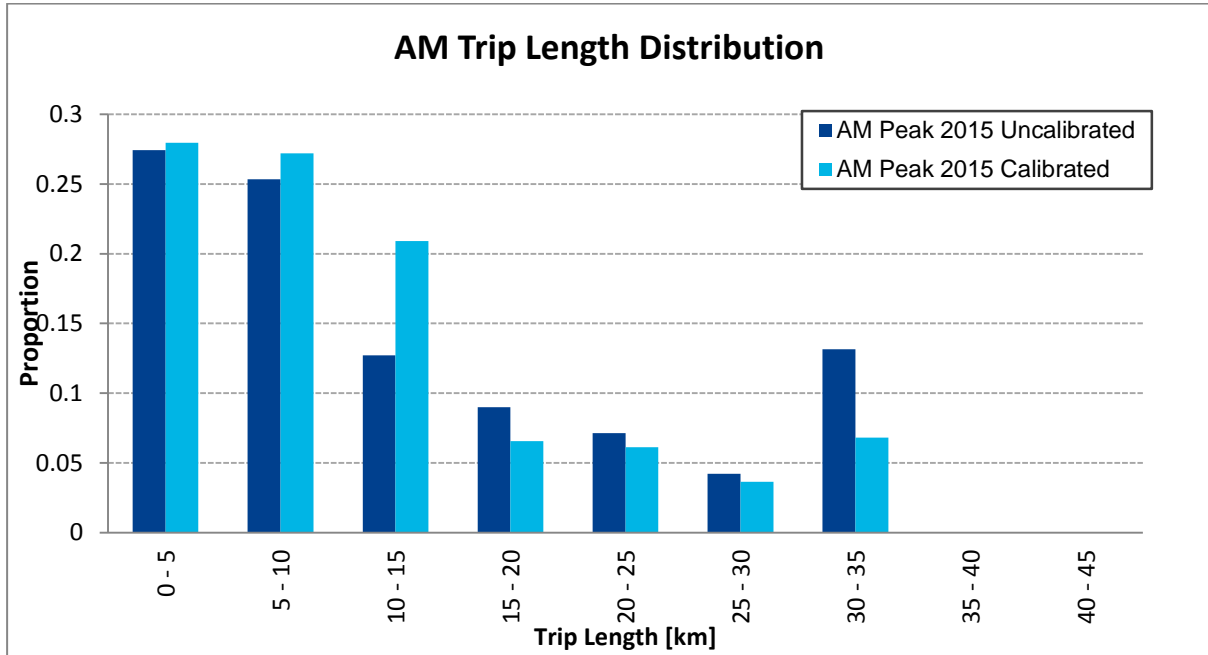


Figure 4.1 - TLD AM Peak Hour (LV)

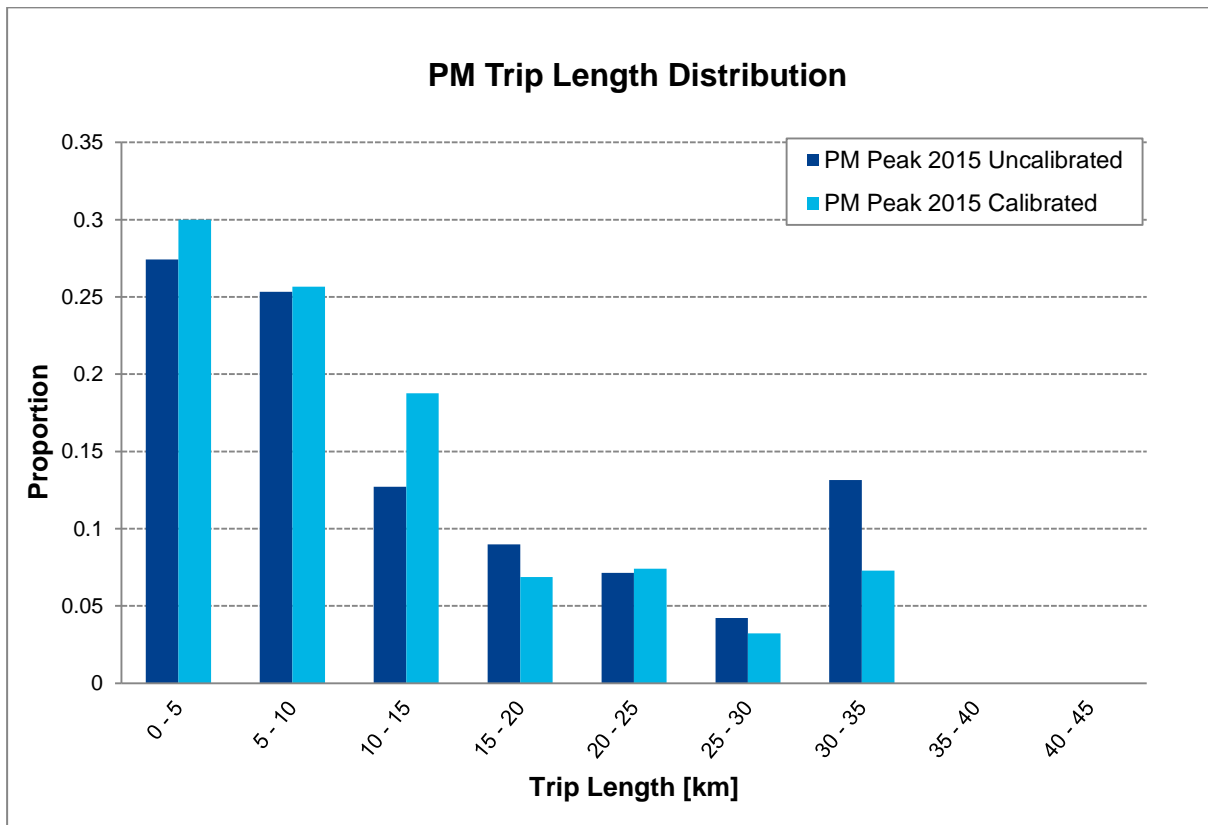


Figure 4.2 - TLD PM Peak Hour (LV)

In Figures 4.1 and 4.2 above, it can be observed that there is a reduction in longer (30-35 KM) trips, combined with a corresponding increase in shorter (10-15KM) trips. This occurs when the strategic level National Transport Model zones are broken down into the more detailed Local Area Model zones and trips reduce in length as there is less distance to travel.

#### 4.4 Model Validation

Model validation comprises the comparison of calibrated flows against an independent data set which was not used as part of the calibration process. Validation checks included:

- Additional link flows;
- Turning flow validation;

##### 4.4.1 Validation of Link Flows

The results of the validation check for 14 links are outlined below. The detailed summary tables are included in Appendix A. Using the same criteria as link flow calibration in Section 4.2.1 above, the link flow validation statistics are shown in Tables 4.5 and 4.6.

Table 4.5 - Validation Results: Link Flows

| % of Validation Sites Meeting Individual Flow Criteria |               |        |         |          |
|--|---------------|--------|---------|----------|
| Time Period  | Link Flows    |        |         | Required |
|  | Total Traffic | Lights | Heavies |          |
| AM Peak  | 93%           | 100%   | 100%    | >85%     |
| PM Peak  | 93%           | 93%    | 100%    | >85%     |

Table 4.6 - Validation Results: GEH Values

| % of Calibration Sites with GEH < 5 |               |        |         |          |
|-------------------------------------|---------------|--------|---------|----------|
| Time Period                         | Link Flows    |        |         | Required |
|                                     | Total Traffic | Lights | Heavies |          |
| AM Peak                             | 93%           | 86%    | 100%    | >85%     |
| PM Peak                             | 86%           | 93%    | 100%    | >85%     |

The comparison of modelled and observed flows demonstrates that the AM and PM peak period models exceed the flow criteria for all user classes. Likewise, the GEH results show that the AM Peak and PM Peak period models also exceed the criteria for all user classes. Therefore, the model is deemed validated in terms of link flows.

##### 4.3.2 Validation of Turning Flows

The observed and modelled turning volumes for 79 turning flows were compared at each of the validation sites in accordance with the criteria above. The permissible difference was calculated for each value (based on the observed figure) and compared with that which had been modelled. Validation results are included in Appendix A and are summarised in Tables 4.7 and 4.8 below:

Table 4.7: Validation Results: Turning Flows

| % of Validation Sites meeting the flow criteria |               |        |         |          |
|---|---------------|--------|---------|----------|
| Time Period                                     | Link Flows    |        |         | Required |
|   | Total Traffic | Lights | Heavies |          |
| AM Peak   | 95%           | 97%    | 100%    | >85%     |
| PM Peak   | 97%           | 96%    | 100%    | >85%     |

Table 4.8: Validation Results: Turning Flow GEH Values

| % of Validation Sites meeting the flow criteria |               |        |         |          |
|---|---------------|--------|---------|----------|
| Time Period                                     | Link Flows    |        |         | Required |
|   | Total Traffic | Lights | Heavies |          |
| AM Peak   | 82%           | 85%    | 99%     | >85%     |
| PM Peak   | 85%           | 86%    | 97%     | >85%     |

The comparison against the validation counts shows that all peak period models meet the TII criteria for junction turns. However, in the AM peak, the validation results for total traffic are marginally below the required values but the model is fit for purpose.

## Chapter 5 Future Year Model Development

### 5.1 Overview

This section of the report summarises the development of the future year Local Area Models used to inform the needs assessment of the M11/N11 corridor.

### 5.2 Future Year Demand

Two future years have been used as part of the needs assessment, 2030 and 2050. These years represent the planned completion of the core and comprehensive TEN-T networks respectively. The projected growth in demand on the National Road network in both 2030 and 2050 is based on the TII National Transport Model (NTpM) 'Central' growth scenario. Full details of the projection of traffic in the NTpM are provided in the *National Transport Model Demographic and Economic Forecasting Report – September 2014*<sup>2</sup>. Table 5.1 provides a summary of the four future year scenarios developed to inform the need assessment study.

Table 5.1: Baseline (Do-Minimum) Scenarios

| NTpM Growth Scenario | Year | Peak Hour          |
|----------------------|------|--------------------|
| TII Central Growth   | 2030 | AM (08:00 – 09:00) |
|                      |      | PM (17:00 – 18:00) |
|                      | 2050 | AM (08:00 – 09:00) |
|                      |      | PM (17:00 – 18:00) |

### 5.3 Demographic Projections

The total population and employment projections for the study area used in the development for TII NTpM for 2030 and 2050 are summarised in Table 5.2. A population growth of approximately 0.95% per annum is projected up to 2030 reducing to 0.3% per annum between 2030 and 2050. Employment grows at 1.2% up to 2030 and reduces significantly to 0.1% per annum beyond 2030.

Table 5.2: NTpM Population & Employment Projections

| Demographic | Year   |        |         | Percentage Growth |             |
|-------------|--------|--------|---------|-------------------|-------------|
|             | 2015   | 2030   | 2050    | 2015 - 2030       | 2015 - 2050 |
| Population  | 85,595 | 98,522 | 104,288 | 15%               | 21%         |
| Employment  | 34,869 | 41,346 | 41,913  | 19%               | 20%         |

### 5.4 Travel Demand Projections

The NTpM converts the projected demographics presented in Table 5.2 into peak hour vehicular trips for the study area. Table 5.3 and 5.4 provide a summary of the trip matrix total for the base and future year scenarios in the AM and PM peak hour respectively.

<sup>2</sup> <http://www.tii.ie/tii-library/strategic-planning/>

Table 5.3: TII Growth in AM Peak Hour Trip Demand

| Demand | Year   |        |        | Percentage Growth |             |
|--------|--------|--------|--------|-------------------|-------------|
|        | 2015   | 2030   | 2050   | 2015 - 2030       | 2015 - 2050 |
| Cars   | 17,154 | 21,038 | 22,451 | 23%               | 30%         |
| HGV    | 567    | 820    | 1,145  | 45%               | 102%        |

Table 5.4: TII Growth in PM Peak Hour Trip Demand

| Demand | Year   |        |        | Percentage Growth |             |
|--------|--------|--------|--------|-------------------|-------------|
|        | 2015   | 2030   | 2050   | 2015 - 2030       | 2015 - 2050 |
| Cars   | 17,257 | 21,126 | 22,343 | 22%               | 29%         |
| HGV    | 450    | 650    | 910    | 44%               | 102%        |

## 5.5 Future Modal Splits

In order to reflect the level of trip demand that would occur in the Study Area for the forecast year of 2030 it was necessary to ascertain the impacts that future changes in public transport provision would have on the overall level of car based demand in the Study Area.

For this purpose, the NTA provided information on the modal splits for the Study Area of the M11/N11 Study based on their Base Year 2012 and 2035 Do-Minimum Eastern Regional Models.

### 5.5.1 2035 Do-Minimum Eastern Regional Model

The Do-Minimum scenario for the NTA strategy was provided by the NTA using outputs from the 'Do-Minimum' scenario of their Eastern Regional Model, which includes the following schemes:

- Major completed transport schemes delivered between 2012-2015;
- Luas Cross City;
- Phoenix Park Tunnel; and
- DART frequency increases on the Northern and South Eastern lines;

Further detail on the schemes included in the NTA's 2035 Do-Minimum Eastern Regional Model is provided in the "Transport Modelling Report for the Transport Strategy for the Greater Dublin Area 2016 to 2035", National Transport Authority (October 2015).

### 5.5.2 Application of Mode Share Data to Forecast Demand

The analysis of the 2035 NTA's Do-Minimum Scenario revealed that all the public transport improvements proposed in the scenario would be in place by 2030.

Whilst the majority of the public transport interventions included in the scenario occur outside the M11/N11 study area any mode share impacts generated by the implementation of the schemes were required to be reflected in the 2030 and 2050 demand matrices. An exercise was therefore undertaken to reflect the reduction in car trip demand associated with the implementation of the public transport interventions in the 2030 and 2050 demand matrices. Tables 5.5 and 5.6 summarise the reduction in car trip demand in the 2030 and 2050 AM and PM peak periods across the study area as a result of the increased public transport provision.



*Table 5.5: Impact of committed public transport proposals on 2030 AM/PM Peak Hour Car Demand*

| Peak Hour | 2030 (vehs) | 2030 with PT (vehs) | Percentage Reduction in Demand |
|-----------|-------------|---------------------|--------------------------------|
| AM        | 21,038      | 20,464              | -3%                            |
| PM        | 21,126      | 20,573              | -3%                            |

*Table 5.6: Impact of committed public transport proposals on 2050 AM/PM Peak Hour Car Demand*

| Peak Hour | 2050 (vehs) | 2050 with PT (vehs) | Percentage Reduction in Demand |
|-----------|-------------|---------------------|--------------------------------|
| AM        | 22,498      | 21,980              | -2%                            |
| PM        | 22,343      | 21,745              | -3%                            |

### 5.5.3 Final Demand Matrices

The final 2030 and 2050 AM and PM peak period trip demand matrix totals for the study area are presented in Table 5.7 and Table 5.8 respectively. These represent TII projections with the NTA mode splits resulting from the NTA Do-Minimum scenario taken into account.

*Table 5.7: AM Peak Final Trip Demand Matrix Totals*

| Demand | Year   |        |        | Percentage Growth |             |
|--------|--------|--------|--------|-------------------|-------------|
|        | 2015   | 2030   | 2050   | 2015 - 2030       | 2015 - 2050 |
| Cars   | 17,154 | 20,464 | 21,980 | 19%               | 28%         |
| HGV    | 567    | 820    | 1,146  | 45%               | 102%        |

*Table 5.8: PM Peak Final Trip Demand Matrix Totals*

| Demand | Year   |        |        | Percentage Growth |             |
|--------|--------|--------|--------|-------------------|-------------|
|        | 2015   | 2030   | 2050   | 2015 - 2030       | 2015 - 2050 |
| Cars   | 17,257 | 20,573 | 21,745 | 19%               | 26%         |
| HGV    | 450    | 650    | 910    | 44%               | 102%        |

## 5.6 Future Year Trip Distribution

A process was set up to assign future year trip end growth in each NTM zone to the associated LAM zones by allocating growth based on county development plans, local area plans (where available) and previous relevant studies including the following:

- Wicklow County Development Plan (Draft) 2016 – 2022
- Dun Laoghaire Rathdown County Development Plan (Draft) 2016 – 2022
- M50/M11 Corridor study Report (TII, 2012)

Following this process, future year trip distribution was undertaken utilising the furness distribution method. In order to carry out the trip distribution process it was first necessary to 'seed' the cells with no trips in the base year matrices with very small numbers (0.01 vehicles) to allow for future year trips between those specific cells. Otherwise any cell with a zero will remain zero irrespective of the factor applied. As part of the trip distribution process the matrix totals were doubly constrained to the mean

of the forecast trip end totals. Adjustments were also made to account for zones where there is expected to be significant increases to trips within the zone, i.e. increased internal traffic. For example, future housing and commercial development in the LAM zone 53816 (Fassaroe area) is expected to generate increased internal traffic as people will be able to live and work in this area.

### **5.7 Future Year Network Development**

A future year 'Do-Minimum' network should include the existing road network plus any committed infrastructure improvements in the study area. As there is no significant road improvements committed currently within the study area, the 'Do-Minimum' future network for the M11/N11 Corridor Study consists of the existing road network, which is assumed to be maintained over time.

The final demand matrices referenced in Section 5.4.3 above were then applied to the future year network to assess the anticipated level of network performance in 2030 and 2050.

### **5.8 2030 Do-Minimum**

The 2030 Do-Minimum traffic volumes for the AM and PM peak periods are provided in Table 5.9. The number of lanes for each section and the practical capacity is also shown.

Table 5.9: 2030 Do-Minimum M11/N11 Peak Hour Demand Flows (Source: 2030 Do-Minimum M11/N11 LAM)

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00) – Northbound<br>(vehicles/hour) |                    |               | PM Peak (17:00 – 18:00) – Southbound<br>(vehicles/hour) |                    |               |
|------|--------------|----------------------------------|--------------|---|--------------------|---------------|---|--------------------|---------------|
|      |              |                                  |              | Demand Flow   | Practical Capacity |               | Demand Flow   | Practical Capacity |               |
|      |              |                                  |              |   | GDA Average        | Link Specific |   | GDA Average        | Link Specific |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 3,390   | 3,400              | 4,600         | 2,968   | 3,400              | 4,600         |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 2,021   | 3,400              | 3,400         | 1,617   | 3,400              | 3,400         |
|      | 4 – 5        | M50/M11 – Bray North             | 2+1          | 5,411   | 5,100              | 6,300         | 4,584   | 5,100              | 6,300         |
|      | 5 – 6        | Bray North – Bray Central        | 2            | <b>4,714</b>  | 3,400              | 4,600         | <b>4,085</b>  | 3,400              | 3,850         |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117 | 2            | <b>4,855</b>  | 3,400              | 3,550         | <b>4,143</b>  | 3,400              | 3,200         |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 2            | <b>4,866</b>  | 3,400              | 3,550         | <b>4,054</b>  | 3,400              | 3,200         |
|      | 7 – 8        | Bray South - Kilmacanogue        | 2            | <b>3,978</b>  | 3,400              | 3,550         | <b>3,564</b>  | 3,400              | 3,200         |
|      | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 3,270   | 3,400              | 3,550         | 3,103   | 3,400              | 3,550         |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 3,232   | 3,400              | 3,550         | 3,068   | 3,400              | 3,550         |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 2,796   | 3,400              | 3,550         | 2,888   | 3,400              | 3,550         |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 2,653   | 3,400              | 3,550         | 2,679   | 3,400              | 3,550         |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 2,040   | 3,400              | 3,550         | 2,160   | 3,400              | 3,550         |
| M11  | 13 – 14      | Newcastle – Coyne's Cross        | 2            | 2,125   | 3,400              | 3,550         | 2,366   | 3,400              | 3,550         |
|      | 14 – 15      | Coyne's Cross - Ashford          | 2            | 2,227   | 3,400              | 4,600         | 2,465   | 3,400              | 4,600         |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

The traffic flow volumes highlighted in red represent the links that are operating at or above 95% of the link specific practical capacity in the 2030 Do-Minimum scenario. The key issues are as follows:

#### AM Peak Hour

- Volumes on the M11/N11 northbound carriageway exceed capacity from Junction 8 (Kilmacanogue) to Junction 5 (Bray North/Wilford).

#### PM Peak Hour

- Volumes on the M11/N11 southbound carriageway exceed capacity from Junction 5 (Bray North/Wilford) to Junction 8 (Kilmacanogue).

### 5.9 2050 Do-Minimum

Table 5.10 present the AM Peak (Northbound) and PM Peak (Southbound) hour flows on the mainline sections of the M11/N11 corridor in the 2050 Do-Minimum scenario. The number of lanes and practical capacity for each section is also shown. The traffic flow volumes highlighted in red show the links that are operating at or above 95% of the link specific practical capacity in the 2050 Do-Minimum scenario. No additional sections in 2050 beyond those highlighted in the 2030 assessment operate above practical capacity.

Table 5.10: 2050 Do-Minimum M11/N11 Peak Hour Flows (Source: 2050 Do-Minimum M11/N11 LAM)

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00) – Northbound (vehicles/hour) |                    |               | PM Peak (17:00 – 18:00) – Southbound (vehicles/hour) |                    |               |
|------|--------------|----------------------------------|--------------|--|--------------------|---------------|--|--------------------|---------------|
|      |              |                                  |              | Demand Flow (vehs)                                   | Practical Capacity |               | Demand Flow (vehs)                                   | Practical Capacity |               |
|      |              |                                  |              |  | GDA Average        | Link Specific |  | GDA Average        | Link Specific |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 3,678  | 3,400              | 4,600         | 3,218  | 3,400              | 4,600         |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 2,168  | 3,400              | 3,400         | 1,693  | 3,400              | 3,400         |
|      | 4 – 5        | M50/M11 – Bray North             | 2+1          | 5,846  | 5,100              | 6,300         | 4,910  | 5,100              | 6,300         |
|      | 5 – 6        | Bray North – Bray Central        | 2            | <b>5,013</b>   | 3,400              | 4,600         | <b>4,300</b>   | 3,400              | 3,850         |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117 | 2            | <b>5,038</b>   | 3,400              | 3,550         | <b>4,468</b>   | 3,400              | 3,200         |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 2            | <b>5,077</b>   | 3,400              | 3,550         | <b>4,379</b>   | 3,400              | 3,200         |
|      | 7 – 8        | Bray South - Kilmacanogue        | 2            | <b>3,959</b>   | 3,400              | 3,550         | <b>3,811</b>   | 3,400              | 3,200         |
|      | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 3,326  | 3,400              | 3,550         | 3,292  | 3,400              | 3,550         |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 3,273  | 3,400              | 3,550         | 3,255  | 3,400              | 3,550         |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 2,915  | 3,400              | 3,550         | 3,089  | 3,400              | 3,550         |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 2,785  | 3,400              | 3,550         | 2,844  | 3,400              | 3,550         |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 2,084  | 3,400              | 3,550         | 2,261  | 3,400              | 3,550         |
| M11  | 13 – 14      | Newcastle – Coyne's Cross        | 2            | 2,209  | 3,400              | 3,550         | 2,488  | 3,400              | 3,550         |
|      | 14 – 15      | Coyne's Cross - Ashford          | 2            | 2,319  | 3,400              | 4,600         | 2,585  | 3,400              | 4,600         |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

## 5.10 Network Statistics

Table 5.11 outlines a comparison of the modelled network statistics for the 2015 Base Models and the 2030 and 2050 Do-Minimum models for the AM and PM peak periods. As can be seen from the network statistics, by 2030, in the AM peak the network will experience an increase in vehicle kilometres (23%), travel time (23%) and network delay (34%). In the 2050 AM peak the network will experience a significant increase in vehicle kilometres (34%), travel time (39%) and most significantly network delay (66%).

Similarly, in the 2030 PM peak the network will experience an increase in vehicle kilometres (22%), travel time (23%) but most significantly in network delay (37%). In the 2050 PM peak the network will experience a significant increase in vehicle kilometres (27%), travel time (32%) and most significantly network delay (63%).

Table 5.11: AM & PM Peak Hour Modelled Network Statistics

| Scenario       | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|----------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM        | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2030 AM Do-Min | 21,284                | 5,740                   | 16.18                          | 248,432             | 1,333             |
| 2050 AM Do-Min | 23,125                | 6,444                   | 16.72                          | 270,556             | 1,656             |
|                |                       |                         |                                |                     |                   |
| 2015 PM        | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2030 PM Do-Min | 21,223                | 5,451                   | 15.41                          | 244,970             | 1,102             |
| 2050 PM Do-Min | 22,655                | 5,873                   | 15.55                          | 254,009             | 1,318             |

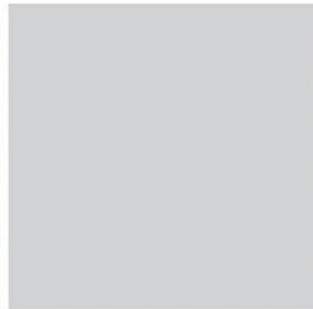
## 5.11 Summary of Future 'Do-Minimum' Needs Assessment

The needs assessment of the M11/N11 corridor has demonstrated the following:

- The existing capacity of the M11/N11 mainline corridor will need to be increased as far south as Junction 8 (Kilmacanogue) in order to cater for the projected demand in 2030/2050 based on current traffic growth projections;
- There is no need for additional mainline or junction capacity on the N11 between Junction 8 (Kilmacanogue) and Junction 14 (Coynes Cross) based on current traffic growth projections. However, to bring this section of the corridor up to the required standard existing direct accesses and left on / left off junctions should be closed or reconfigured; and
- Upgrades will need to be made to the regional/local road network to provide improved access between the existing M11/N11 mainline junctions and the regional/local road network.

This study has also confirmed the more detailed junction analysis undertaken as part of some of the previous studies which highlighted that the capacity/operation of the existing M11/N11 mainline junctions (6, 6a, 7 and 8) need to be improved to address existing issues at these locations.

## Appendices



*Appendix A*  
**Calibration & Validation**



### AM Peak Link Calibration

| NTM AM Total Link Flow Calibration |               |               |            |            |           |            |             |           |             |             |  |
|------------------------------------|---------------|---------------|------------|------------|-----------|------------|-------------|-----------|-------------|-------------|--|
| Counts :                           |               | 23            | RESULT =   | 91%        |           | RESULT =   | 100%        |           |             |             |  |
| Total Traffic                      |               |               | REQD =     | 85%        |           | REQD =     | 85%         |           |             |             |  |
| Link Number                        | Obs           | Mod           |            | GEH        | GEH TEST  | CLASS TEST | Target Diff | Flow Test | ACT DIFF    | FACTOR      |  |
| 3508                               | 217           | 287           | -70        | 4.4        | 1         | 1          | 100         | 1         | 70          | 1.32        |  |
| 3510                               | 200           | 203           | -3         | 0.2        | 1         | 1          | 100         | 1         | 3           | 1.02        |  |
| 3784                               | 1244          | 1228          | 16         | 0.5        | 1         | 2          | 187         | 1         | -16         | 0.99        |  |
| 51220                              | 3846          | 3538          | 308        | 5.1        | 0         | 2          | 577         | 1         | -308        | 0.92        |  |
| 52363                              | 71            | 48            | 23         | 3.0        | 1         | 1          | 100         | 1         | -23         | 0.68        |  |
| 52441                              | 1453          | 1382          | 71         | 1.9        | 1         | 2          | 218         | 1         | -71         | 0.95        |  |
| 52632                              | 941           | 898           | 43         | 1.4        | 1         | 2          | 141         | 1         | -43         | 0.95        |  |
| 52670                              | 3851          | 3581          | 270        | 4.4        | 1         | 2          | 578         | 1         | -270        | 0.93        |  |
| 52754                              | 1724          | 1710          | 14         | 0.3        | 1         | 2          | 259         | 1         | -14         | 0.99        |  |
| 52784                              | 1140          | 1101          | 39         | 1.2        | 1         | 2          | 171         | 1         | -39         | 0.97        |  |
| 52905                              | 1745          | 1698          | 47         | 1.1        | 1         | 2          | 262         | 1         | -47         | 0.97        |  |
| 52913                              | 949           | 929           | 20         | 0.7        | 1         | 2          | 142         | 1         | -20         | 0.98        |  |
| 724504088                          | 1777          | 1660          | 117        | 2.8        | 1         | 2          | 267         | 1         | -117        | 0.93        |  |
| 749747405                          | 1495          | 1577          | -82        | 2.1        | 1         | 2          | 224         | 1         | 82          | 1.05        |  |
| 749848473                          | 3721          | 3521          | 200        | 3.3        | 1         | 2          | 558         | 1         | -200        | 0.95        |  |
| 751080053                          | 4168          | 4010          | 158        | 2.5        | 1         | 2          | 625         | 1         | -158        | 0.96        |  |
| 752699003                          | 1975          | 2153          | -178       | 3.9        | 1         | 2          | 296         | 1         | 178         | 1.09        |  |
| 2147479948                         | 73            | 146           | -73        | 7.0        | 0         | 1          | 100         | 1         | 73          | 2.00        |  |
| 2147480163                         | 2053          | 2047          | 6          | 0.1        | 1         | 2          | 308         | 1         | -6          | 1.00        |  |
| 2147481635                         | 2505          | 2469          | 36         | 0.7        | 1         | 2          | 376         | 1         | -36         | 0.99        |  |
| 2147481702                         | 2538          | 2502          | 36         | 0.7        | 1         | 2          | 381         | 1         | -36         | 0.99        |  |
| 2147481718                         | 2064          | 2117          | -53        | 1.2        | 1         | 2          | 310         | 1         | 53          | 1.03        |  |
| 2147481724                         | 85            | 75            | 10         | 1.1        | 1         | 1          | 100         | 1         | -10         | 0.88        |  |
|                                    | <b>39,835</b> | <b>38,880</b> | <b>955</b> | <b>4.8</b> | <b>21</b> |            |             | <b>23</b> | <b>-955</b> | <b>0.98</b> |  |

### PM Peak Link Calibration

| NTM PM Total Link Flow Calibration |               |               |              |            |           |            |             |           |               |             |  |
|------------------------------------|---------------|---------------|--------------|------------|-----------|------------|-------------|-----------|---------------|-------------|--|
| Counts :                           |               | 23            | RESULT =     | 96%        |           | RESULT =   | 100%        |           |               |             |  |
| Total Traffic                      |               |               | REQD =       | 85%        |           | REQD =     | 85%         |           |               |             |  |
| Link Number                        | Obs           | Mod           |              | GEH        | GEH TEST  | CLASS TEST | Target Diff | Flow Test | ACT DIFF      | FACTOR      |  |
| 3508                               | 274           | 287           | -13          | 0.8        | 1         | 1          | 100         | 1         | 13            | 1.05        |  |
| 3510                               | 534           | 450           | 84           | 3.8        | 1         | 1          | 100         | 1         | -84           | 0.84        |  |
| 3784                               | 2528          | 2513          | 15           | 0.3        | 1         | 2          | 379         | 1         | -15           | 0.99        |  |
| 51220                              | 2242          | 2013          | 229          | 5.0        | 1         | 2          | 336         | 1         | -229          | 0.90        |  |
| 52363                              | 56            | 45            | 11           | 1.5        | 1         | 1          | 100         | 1         | -11           | 0.80        |  |
| 52441                              | 3136          | 2872          | 264          | 4.8        | 1         | 2          | 470         | 1         | -264          | 0.92        |  |
| 52632                              | 1865          | 1749          | 116          | 2.7        | 1         | 2          | 280         | 1         | -116          | 0.94        |  |
| 52670                              | 2328          | 2135          | 193          | 4.1        | 1         | 2          | 349         | 1         | -193          | 0.92        |  |
| 52754                              | 994           | 1041          | -47          | 1.5        | 1         | 2          | 149         | 1         | 47            | 1.05        |  |
| 52784                              | 2177          | 2096          | 81           | 1.8        | 1         | 2          | 327         | 1         | -81           | 0.96        |  |
| 52905                              | 1005          | 1019          | -14          | 0.4        | 1         | 2          | 151         | 1         | 14            | 1.01        |  |
| 52913                              | 1973          | 1878          | 95           | 2.2        | 1         | 2          | 296         | 1         | -95           | 0.95        |  |
| 724504088                          | 3522          | 3412          | 110          | 1.9        | 1         | 2          | 528         | 1         | -110          | 0.97        |  |
| 749747405                          | 836           | 865           | -29          | 1.0        | 1         | 2          | 125         | 1         | 29            | 1.03        |  |
| 749848473                          | 2194          | 1946          | 248          | 5.5        | 0         | 2          | 329         | 1         | -248          | 0.89        |  |
| 751080053                          | 2488          | 2370          | 118          | 2.4        | 1         | 2          | 373         | 1         | -118          | 0.95        |  |
| 752699003                          | 3698          | 3741          | -43          | 0.7        | 1         | 2          | 555         | 1         | 43            | 1.01        |  |
| 2147479948                         | 149           | 154           | -5           | 0.4        | 1         | 1          | 100         | 1         | 5             | 1.03        |  |
| 2147480163                         | 1331          | 1267          | 64           | 1.8        | 1         | 2          | 200         | 1         | -64           | 0.95        |  |
| 2147481635                         | 1325          | 1318          | 7            | 0.2        | 1         | 2          | 199         | 1         | -7            | 0.99        |  |
| 2147481702                         | 1443          | 1359          | 84           | 2.2        | 1         | 2          | 216         | 1         | -84           | 0.94        |  |
| 2147481718                         | 1203          | 1131          | 72           | 2.1        | 1         | 2          | 180         | 1         | -72           | 0.94        |  |
| 2147481724                         | 38            | 54            | -16          | 2.4        | 1         | 1          | 100         | 1         | 16            | 1.42        |  |
|                                    | <b>37,339</b> | <b>35,715</b> | <b>1,624</b> | <b>8.5</b> | <b>22</b> |            |             | <b>23</b> | <b>-1,624</b> | <b>0.96</b> |  |

### AM Peak Turn Calibration

| NTM AM Total Turn Flow Calibration |      |      |      |        |          |            |             |           |          |        |
|------------------------------------|------|------|------|--------|----------|------------|-------------|-----------|----------|--------|
| Counts :                           |      | 149  |      |        | RESULT = |            | 89%         |           | RESULT = |        |
| Total Traffic                      |      |      |      | REQD = |          | 85%        |             | REQD =    |          | 94%    |
| Link Number                        | Obs  | Mod  | Diff | GEH    | GEH TEST | CLASS TEST | Target Diff | Flow Test | ACT DIFF | FACTOR |
| 200002069                          | 452  | 348  | 104  | 5.2    | 0        | 1          | 100         | 0         | -104     | 0.77   |
| 121890833                          | 17   | 18   | -1   | 0.2    | 1        | 1          | 100         | 1         | 1        | 1.06   |
| 121890833                          | 170  | 199  | -29  | 2.1    | 1        | 1          | 100         | 1         | 29       | 1.17   |
| 121894356                          | 580  | 497  | 83   | 3.6    | 1        | 1          | 100         | 1         | -83      | 0.86   |
| 121891635                          | 170  | 156  | 14   | 1.1    | 1        | 1          | 100         | 1         | -14      | 0.92   |
| 121891957                          | 594  | 560  | 34   | 1.4    | 1        | 1          | 100         | 1         | -34      | 0.94   |
| 121892733                          | 378  | 428  | -50  | 2.5    | 1        | 1          | 100         | 1         | 50       | 1.13   |
| 121892733                          | 52   | 40   | 12   | 1.8    | 1        | 1          | 100         | 1         | -12      | 0.77   |
| 121892444                          | 646  | 684  | -38  | 1.5    | 1        | 1          | 100         | 1         | 38       | 1.06   |
| 121892862                          | 205  | 215  | -10  | 0.7    | 1        | 1          | 100         | 1         | 10       | 1.05   |
| 121605493                          | 635  | 656  | -21  | 0.8    | 1        | 1          | 100         | 1         | 21       | 1.03   |
| 121605493                          | 186  | 206  | -20  | 1.4    | 1        | 1          | 100         | 1         | 20       | 1.11   |
| 121894771                          | 24   | 8    | 16   | 4.0    | 1        | 1          | 100         | 1         | -16      | 0.33   |
| 121890870                          | 356  | 327  | 29   | 1.6    | 1        | 1          | 100         | 1         | -29      | 0.92   |
| 121898192                          | 473  | 395  | 78   | 3.7    | 1        | 1          | 100         | 1         | -78      | 0.84   |
| 121893478                          | 222  | 203  | 19   | 1.3    | 1        | 1          | 100         | 1         | -19      | 0.91   |
| 121897940                          | 445  | 426  | 19   | 0.9    | 1        | 1          | 100         | 1         | -19      | 0.96   |
| 121894049                          | 215  | 334  | -119 | 7.2    | 0        | 1          | 100         | 0         | 119      | 1.55   |
| 121893447                          | 313  | 316  | -3   | 0.2    | 1        | 1          | 100         | 1         | 3        | 1.01   |
| 121891402                          | 568  | 445  | 123  | 5.5    | 0        | 1          | 100         | 0         | -123     | 0.78   |
| 121891402                          | 260  | 287  | -27  | 1.6    | 1        | 1          | 100         | 1         | 27       | 1.10   |
| 121894401                          | 430  | 325  | 105  | 5.4    | 0        | 1          | 100         | 0         | -105     | 0.76   |
| 121895862                          | 1219 | 1193 | 26   | 0.7    | 1        | 2          | 183         | 1         | -26      | 0.98   |
| 121890589                          | 348  | 321  | 27   | 1.5    | 1        | 1          | 100         | 1         | -27      | 0.92   |
| 121894203                          | 175  | 200  | -25  | 1.8    | 1        | 1          | 100         | 1         | 25       | 1.14   |
| 121895931                          | 320  | 269  | 51   | 3.0    | 1        | 1          | 100         | 1         | -51      | 0.84   |
| 121622881                          | 380  | 313  | 67   | 3.6    | 1        | 1          | 100         | 1         | -67      | 0.82   |
| 121891434                          | 937  | 1027 | -90  | 2.9    | 1        | 2          | 141         | 1         | 90       | 1.10   |
| 121606598                          | 243  | 278  | -35  | 2.2    | 1        | 1          | 100         | 1         | 35       | 1.14   |
| 121606598                          | 108  | 84   | 24   | 2.4    | 1        | 1          | 100         | 1         | -24      | 0.78   |
| 121890242                          | 487  | 473  | 14   | 0.6    | 1        | 1          | 100         | 1         | -14      | 0.97   |
| 121897835                          | 248  | 282  | -34  | 2.1    | 1        | 1          | 100         | 1         | 34       | 1.14   |
| 121891058                          | 31   | 62   | -31  | 4.5    | 1        | 1          | 100         | 1         | 31       | 2.00   |
| 121892018                          | 84   | 86   | -2   | 0.2    | 1        | 1          | 100         | 1         | 2        | 1.02   |
| 121892534                          | 69   | 62   | 7    | 0.9    | 1        | 1          | 100         | 1         | -7       | 0.90   |
| 121891057                          | 124  | 62   | 62   | 6.4    | 0        | 1          | 100         | 1         | -62      | 0.50   |
| 121895433                          | 71   | 84   | -13  | 1.5    | 1        | 1          | 100         | 1         | 13       | 1.18   |
| 121895434                          | 115  | 107  | 8    | 0.8    | 1        | 1          | 100         | 1         | -8       | 0.93   |
| 121891476                          | 111  | 94   | 17   | 1.7    | 1        | 1          | 100         | 1         | -17      | 0.85   |
| 121893621                          | 19   | 14   | 5    | 1.2    | 1        | 1          | 100         | 1         | -5       | 0.74   |
| 121893620                          | 354  | 438  | -84  | 4.2    | 1        | 1          | 100         | 1         | 84       | 1.24   |
| 121893620                          | 20   | 14   | 6    | 1.5    | 1        | 1          | 100         | 1         | -6       | 0.70   |
| 121897125                          | 114  | 91   | 23   | 2.3    | 1        | 1          | 100         | 1         | -23      | 0.80   |
| 121897125                          | 223  | 232  | -9   | 0.6    | 1        | 1          | 100         | 1         | 9        | 1.04   |
| 121897606                          | 259  | 361  | -102 | 5.8    | 0        | 1          | 100         | 0         | 102      | 1.39   |
| 121890192                          | 5    | 0    | 5    | 3.2    | 1        | 1          | 100         | 1         | -5       | 0.00   |
| 121890192                          | 12   | 14   | -2   | 0.6    | 1        | 1          | 100         | 1         | 2        | 1.17   |
| 121897488                          | 237  | 248  | -11  | 0.7    | 1        | 1          | 100         | 1         | 11       | 1.05   |
| 121897488                          | 2    | 0    | 2    | 2.0    | 1        | 1          | 100         | 1         | -2       | 0.00   |
| 121893839                          | 9    | 0    | 9    | 4.2    | 1        | 1          | 100         | 1         | -9       | 0.00   |
| 121892073                          | 26   | 14   | 12   | 2.7    | 1        | 1          | 100         | 1         | -12      | 0.54   |
| 121890941                          | 9    | 0    | 9    | 4.2    | 1        | 1          | 100         | 1         | -9       | 0.00   |
| 121892699                          | 260  | 215  | 45   | 2.9    | 1        | 1          | 100         | 1         | -45      | 0.83   |
| 121896733                          | 1062 | 1054 | 8    | 0.2    | 1        | 2          | 159         | 1         | -8       | 0.99   |
| 121896733                          | 181  | 81   | 100  | 8.7    | 0        | 1          | 100         | 1         | -100     | 0.45   |
| 121890227                          | 700  | 585  | 115  | 4.5    | 1        | 2          | 105         | 0         | -115     | 0.84   |
| 121894922                          | 355  | 301  | 54   | 3.0    | 1        | 1          | 100         | 1         | -54      | 0.85   |
| 121893526                          | 306  | 377  | -71  | 3.8    | 1        | 1          | 100         | 1         | 71       | 1.23   |
| 121892821                          | 291  | 260  | 31   | 1.9    | 1        | 1          | 100         | 1         | -31      | 0.89   |
| 121892821                          | 247  | 282  | -35  | 2.2    | 1        | 1          | 100         | 1         | 35       | 1.14   |
| 121892291                          | 204  | 169  | 35   | 2.6    | 1        | 1          | 100         | 1         | -35      | 0.83   |
| 121894272                          | 104  | 49   | 55   | 6.3    | 0        | 1          | 100         | 1         | -55      | 0.47   |
| 121894272                          | 213  | 228  | -15  | 1.0    | 1        | 1          | 100         | 1         | 15       | 1.07   |
| 121893173                          | 360  | 547  | -187 | 8.8    | 0        | 1          | 100         | 0         | 187      | 1.52   |
| 121897587                          | 386  | 456  | -70  | 3.4    | 1        | 1          | 100         | 1         | 70       | 1.18   |
| 121897884                          | 189  | 107  | 82   | 6.7    | 0        | 1          | 100         | 1         | -82      | 0.57   |
| 121891330                          | 768  | 738  | 30   | 1.1    | 1        | 2          | 115         | 1         | -30      | 0.96   |
| 121897588                          | 507  | 550  | -43  | 1.9    | 1        | 1          | 100         | 1         | 43       | 1.08   |
| 121896281                          | 309  | 361  | -52  | 2.8    | 1        | 1          | 100         | 1         | 52       | 1.17   |
| 121896281                          | 84   | 61   | 23   | 2.7    | 1        | 1          | 100         | 1         | -23      | 0.73   |
| 121892466                          | 14   | 2    | 12   | 4.2    | 1        | 1          | 100         | 1         | -12      | 0.14   |
| 121892466                          | 395  | 347  | 48   | 2.5    | 1        | 1          | 100         | 1         | -48      | 0.88   |

|            |               |               |              |            |            |   |     |            |               |             |
|------------|---------------|---------------|--------------|------------|------------|---|-----|------------|---------------|-------------|
| 121891498  | 376           | 393           | -17          | 0.9        | 1          | 1 | 100 | 1          | 17            | 1.05        |
| 121891498  | 292           | 298           | -6           | 0.3        | 1          | 1 | 100 | 1          | 6             | 1.02        |
| 121891499  | 195           | 225           | -30          | 2.1        | 1          | 1 | 100 | 1          | 30            | 1.15        |
| 121891048  | 108           | 63            | 45           | 4.9        | 1          | 1 | 100 | 1          | -45           | 0.58        |
| 121891072  | 243           | 327           | -84          | 5.0        | 1          | 1 | 100 | 1          | 84            | 1.35        |
| 121893996  | 199           | 204           | -5           | 0.4        | 1          | 1 | 100 | 1          | 5             | 1.03        |
| 121891661  | 45            | 0             | 45           | 9.5        | 0          | 1 | 100 | 1          | -45           | 0.00        |
| 121891608  | 369           | 407           | -38          | 1.9        | 1          | 1 | 100 | 1          | 38            | 1.10        |
| 121891608  | 33            | 57            | -24          | 3.6        | 1          | 1 | 100 | 1          | 24            | 1.73        |
| 121892702  | 96            | 115           | -19          | 1.8        | 1          | 1 | 100 | 1          | 19            | 1.20        |
| 121891660  | 27            | 25            | 2            | 0.4        | 1          | 1 | 100 | 1          | -2            | 0.93        |
| 121892947  | 44            | 40            | 4            | 0.6        | 1          | 1 | 100 | 1          | -4            | 0.91        |
| 121891598  | 94            | 79            | 15           | 1.6        | 1          | 1 | 100 | 1          | -15           | 0.84        |
| 121894677  | 53            | 40            | 13           | 1.9        | 1          | 1 | 100 | 1          | -13           | 0.75        |
| 121891629  | 51            | 0             | 51           | 10.1       | 0          | 1 | 100 | 1          | -51           | 0.00        |
| 121642466  | 169           | 163           | 6            | 0.5        | 1          | 1 | 100 | 1          | -6            | 0.96        |
| 121621121  | 513           | 606           | -93          | 3.9        | 1          | 1 | 100 | 1          | 93            | 1.18        |
| 121890684  | 739           | 612           | 127          | 4.9        | 1          | 2 | 111 | 0          | -127          | 0.83        |
| 121890378  | 548           | 422           | 126          | 5.7        | 0          | 1 | 100 | 0          | -126          | 0.77        |
| 121895710  | 575           | 558           | 17           | 0.7        | 1          | 1 | 100 | 1          | -17           | 0.97        |
| 121895710  | 303           | 326           | -23          | 1.3        | 1          | 1 | 100 | 1          | 23            | 1.08        |
| 121899789  | 31            | 12            | 19           | 4.1        | 1          | 1 | 100 | 1          | -19           | 0.39        |
| 121899789  | 123           | 157           | -34          | 2.9        | 1          | 1 | 100 | 1          | 34            | 1.28        |
| 121899789  | 40            | 54            | -14          | 2.0        | 1          | 1 | 100 | 1          | 14            | 1.35        |
| 2000002261 | 1             | 0             | 1            | 1.4        | 1          | 1 | 100 | 1          | -1            | 0.00        |
| 2000002257 | 7             | 0             | 7            | 3.7        | 1          | 1 | 100 | 1          | -7            | 0.00        |
| 2000002265 | 95            | 47            | 48           | 5.7        | 0          | 1 | 100 | 1          | -48           | 0.49        |
| 2000002265 | 47            | 59            | -12          | 1.6        | 1          | 1 | 100 | 1          | 12            | 1.26        |
| 2000002277 | 41            | 24            | 17           | 3.0        | 1          | 1 | 100 | 1          | -17           | 0.59        |
| 2000002282 | 34            | 50            | -16          | 2.5        | 1          | 1 | 100 | 1          | 16            | 1.47        |
| 2000002288 | 39            | 29            | 10           | 1.7        | 1          | 1 | 100 | 1          | -10           | 0.74        |
| 2000002288 | 191           | 153           | 38           | 2.9        | 1          | 1 | 100 | 1          | -38           | 0.80        |
| 2000002297 | 8             | 17            | -9           | 2.5        | 1          | 1 | 100 | 1          | 9             | 2.13        |
| 2000002297 | 63            | 57            | 6            | 0.8        | 1          | 1 | 100 | 1          | -6            | 0.90        |
| 2000002307 | 587           | 513           | 74           | 3.2        | 1          | 1 | 100 | 1          | -74           | 0.87        |
| 121894612  | 43            | 55            | -12          | 1.7        | 1          | 1 | 100 | 1          | 12            | 1.28        |
| 2000002316 | 22            | 0             | 22           | 6.6        | 0          | 1 | 100 | 1          | -22           | 0.00        |
| 2000002243 | 93            | 90            | 3            | 0.3        | 1          | 1 | 100 | 1          | -3            | 0.97        |
| 2000002243 | 11            | 34            | -23          | 4.8        | 1          | 1 | 100 | 1          | 23            | 3.09        |
| 121895000  | 39            | 51            | -12          | 1.8        | 1          | 1 | 100 | 1          | 12            | 1.31        |
| 121895000  | 41            | 28            | 13           | 2.2        | 1          | 1 | 100 | 1          | -13           | 0.68        |
| 2000002468 | 160           | 176           | -16          | 1.2        | 1          | 1 | 100 | 1          | 16            | 1.10        |
| 2000002468 | 86            | 52            | 34           | 4.1        | 1          | 1 | 100 | 1          | -34           | 0.60        |
| 2000002478 | 79            | 79            | 0            | 0.0        | 1          | 1 | 100 | 1          | 0             | 1.00        |
| 2000002472 | 28            | 33            | -5           | 0.9        | 1          | 1 | 100 | 1          | 5             | 1.18        |
| 2000002493 | 89            | 96            | -7           | 0.7        | 1          | 1 | 100 | 1          | 7             | 1.08        |
| 2000002493 | 69            | 38            | 31           | 4.2        | 1          | 1 | 100 | 1          | -31           | 0.55        |
| 121892794  | 565           | 574           | -9           | 0.4        | 1          | 1 | 100 | 1          | 9             | 1.02        |
| 121892794  | 85            | 69            | 16           | 1.8        | 1          | 1 | 100 | 1          | -16           | 0.81        |
| 2000002518 | 271           | 299           | -28          | 1.7        | 1          | 1 | 100 | 1          | 28            | 1.10        |
| 2000002518 | 487           | 473           | 14           | 0.6        | 1          | 1 | 100 | 1          | -14           | 0.97        |
| 121895919  | 194           | 199           | -5           | 0.4        | 1          | 1 | 100 | 1          | 5             | 1.03        |
| 2000002520 | 175           | 200           | -25          | 1.8        | 1          | 1 | 100 | 1          | 25            | 1.14        |
| 121892555  | 2482          | 2469          | 13           | 0.3        | 1          | 2 | 372 | 1          | -13           | 0.99        |
| 121892555  | 30            | 27            | 3            | 0.6        | 1          | 1 | 100 | 1          | -3            | 0.90        |
| 2000002531 | 56            | 29            | 27           | 4.1        | 1          | 1 | 100 | 1          | -27           | 0.52        |
| 2000002555 | 1172          | 1196          | -24          | 0.7        | 1          | 2 | 176 | 1          | 24            | 1.02        |
| 2000002555 | 44            | 14            | 30           | 5.6        | 0          | 1 | 100 | 1          | -30           | 0.32        |
| 2000002555 | 443           | 375           | 68           | 3.4        | 1          | 1 | 100 | 1          | -68           | 0.85        |
| 2000002390 | 24            | 18            | 6            | 1.3        | 1          | 1 | 100 | 1          | -6            | 0.75        |
| 121892925  | 218           | 235           | -17          | 1.1        | 1          | 1 | 100 | 1          | 17            | 1.08        |
| 121890590  | 1523          | 1468          | 55           | 1.4        | 1          | 2 | 228 | 1          | -55           | 0.96        |
| 121890590  | 45            | 42            | 3            | 0.5        | 1          | 1 | 100 | 1          | -3            | 0.93        |
| 2000002557 | 1234          | 1192          | 42           | 1.2        | 1          | 2 | 185 | 1          | -42           | 0.97        |
| 2000002556 | 111           | 79            | 32           | 3.3        | 1          | 1 | 100 | 1          | -32           | 0.71        |
| 2000002558 | 144           | 116           | 28           | 2.5        | 1          | 1 | 100 | 1          | -28           | 0.81        |
| 2000002560 | 36            | 25            | 11           | 2.0        | 1          | 1 | 100 | 1          | -11           | 0.69        |
| 2000002377 | 3             | 0             | 3            | 2.4        | 1          | 1 | 100 | 1          | -3            | 0.00        |
| 2000002565 | 52            | 49            | 3            | 0.4        | 1          | 1 | 100 | 1          | -3            | 0.94        |
| 2000002565 | 199           | 204           | -5           | 0.4        | 1          | 1 | 100 | 1          | 5             | 1.03        |
| 2000002564 | 8             | 0             | 8            | 4.0        | 1          | 1 | 100 | 1          | -8            | 0.00        |
| 121891556  | 1             | 8             | -7           | 3.3        | 1          | 1 | 100 | 1          | 7             | 8.00        |
| 121891556  | 4             | 6             | -2           | 0.9        | 1          | 1 | 100 | 1          | 2             | 1.50        |
| 2000002549 | 23            | 0             | 23           | 6.8        | 0          | 1 | 100 | 1          | -23           | 0.00        |
| 2000002571 | 124           | 95            | 29           | 2.8        | 1          | 1 | 100 | 1          | -29           | 0.77        |
| 2000002573 | 64            | 41            | 23           | 3.2        | 1          | 1 | 100 | 1          | -23           | 0.64        |
| 2000002573 | 8             | 0             | 8            | 4.0        | 1          | 1 | 100 | 1          | -8            | 0.00        |
|            | <b>37,649</b> | <b>36,632</b> | <b>1,017</b> | <b>5.3</b> | <b>132</b> |   |     | <b>140</b> | <b>-1,017</b> | <b>0.97</b> |

### PM Peak Turn Calibration

| NTM PM Total Turn Flow Calibration |     |        |      |          |          |            |             |           |          |        |  |
|------------------------------------|-----|--------|------|----------|----------|------------|-------------|-----------|----------|--------|--|
| Counts :                           |     | 149    |      | RESULT = |          | 86%        |             | RESULT =  |          | 97%    |  |
| Total Traffic                      |     | REQU = |      | 85%      |          | REQU =     |             | 85%       |          |        |  |
| Link Number                        | Obs | Mod    | Diff | GEH      | GEH TEST | CLASS TEST | Target Diff | Flow Test | ACT DIFF | FACTOR |  |
| 2000002069                         | 252 | 192    | 60   | 4.0      | 1        | 1          | 100         | 1         | -60      | 0.76   |  |
| 121890833                          | 55  | 48     | 7    | 1.0      | 1        | 1          | 100         | 1         | -7       | 0.87   |  |
| 121890833                          | 338 | 244    | 94   | 5.5      | 0        | 1          | 100         | 1         | -94      | 0.72   |  |
| 121894356                          | 673 | 787    | -114 | 4.2      | 1        | 1          | 100         | 0         | 114      | 1.17   |  |
| 121891635                          | 141 | 120    | 21   | 1.8      | 1        | 1          | 100         | 1         | -21      | 0.85   |  |
| 121891957                          | 822 | 689    | 133  | 4.8      | 1        | 2          | 123         | 0         | -133     | 0.84   |  |
| 121892733                          | 266 | 219    | 47   | 3.0      | 1        | 1          | 100         | 1         | -47      | 0.82   |  |
| 121892733                          | 45  | 33     | 12   | 1.9      | 1        | 1          | 100         | 1         | -12      | 0.73   |  |
| 121892444                          | 532 | 544    | -12  | 0.5      | 1        | 1          | 100         | 1         | 12       | 1.02   |  |
| 121892862                          | 340 | 356    | -16  | 0.9      | 1        | 1          | 100         | 1         | 16       | 1.05   |  |
| 121605493                          | 794 | 860    | -66  | 2.3      | 1        | 2          | 119         | 1         | 66       | 1.08   |  |
| 121605493                          | 270 | 289    | -19  | 1.1      | 1        | 1          | 100         | 1         | 19       | 1.07   |  |
| 121894771                          | 17  | 11     | 6    | 1.6      | 1        | 1          | 100         | 1         | -6       | 0.65   |  |
| 121890870                          | 309 | 311    | -2   | 0.1      | 1        | 1          | 100         | 1         | 2        | 1.01   |  |
| 121898192                          | 683 | 550    | 133  | 5.4      | 0        | 1          | 100         | 0         | -133     | 0.81   |  |
| 121893478                          | 337 | 280    | 57   | 3.2      | 1        | 1          | 100         | 1         | -57      | 0.83   |  |
| 121897940                          | 446 | 362    | 84   | 4.2      | 1        | 1          | 100         | 1         | -84      | 0.81   |  |
| 121894049                          | 120 | 68     | 52   | 5.4      | 0        | 1          | 100         | 1         | -52      | 0.57   |  |
| 121893447                          | 397 | 381    | 16   | 0.8      | 1        | 1          | 100         | 1         | -16      | 0.96   |  |
| 121891402                          | 374 | 438    | -64  | 3.2      | 1        | 1          | 100         | 1         | 64       | 1.17   |  |
| 121891402                          | 204 | 202    | 2    | 0.1      | 1        | 1          | 100         | 1         | -2       | 0.99   |  |
| 121894401                          | 594 | 636    | -42  | 1.7      | 1        | 1          | 100         | 1         | 42       | 1.07   |  |
| 121895862                          | 847 | 910    | -63  | 2.1      | 1        | 2          | 127         | 1         | 63       | 1.07   |  |
| 121890589                          | 341 | 412    | -71  | 3.7      | 1        | 1          | 100         | 1         | 71       | 1.21   |  |
| 121894203                          | 223 | 241    | -18  | 1.2      | 1        | 1          | 100         | 1         | 18       | 1.08   |  |
| 121895931                          | 271 | 202    | 69   | 4.5      | 1        | 1          | 100         | 1         | -69      | 0.75   |  |
| 121622881                          | 526 | 613    | -87  | 3.6      | 1        | 1          | 100         | 1         | 87       | 1.17   |  |
| 121891434                          | 789 | 826    | -37  | 1.3      | 1        | 2          | 118         | 1         | 37       | 1.05   |  |
| 121606598                          | 35  | 62     | -27  | 3.9      | 1        | 1          | 100         | 1         | 27       | 1.77   |  |
| 121606598                          | 117 | 113    | 4    | 0.4      | 1        | 1          | 100         | 1         | -4       | 0.97   |  |
| 121890242                          | 340 | 359    | -19  | 1.0      | 1        | 1          | 100         | 1         | 19       | 1.06   |  |
| 121897835                          | 139 | 96     | 43   | 4.0      | 1        | 1          | 100         | 1         | -43      | 0.69   |  |
| 121891058                          | 59  | 80     | -21  | 2.5      | 1        | 1          | 100         | 1         | 21       | 1.36   |  |
| 121892018                          | 51  | 69     | -18  | 2.3      | 1        | 1          | 100         | 1         | 18       | 1.35   |  |
| 121892534                          | 96  | 80     | 16   | 1.7      | 1        | 1          | 100         | 1         | -16      | 0.83   |  |
| 121891057                          | 89  | 80     | 9    | 1.0      | 1        | 1          | 100         | 1         | -9       | 0.90   |  |
| 121895433                          | 109 | 88     | 21   | 2.1      | 1        | 1          | 100         | 1         | -21      | 0.81   |  |
| 121895434                          | 213 | 186    | 27   | 1.9      | 1        | 1          | 100         | 1         | -27      | 0.87   |  |
| 121891476                          | 74  | 100    | -26  | 2.8      | 1        | 1          | 100         | 1         | 26       | 1.35   |  |
| 121893621                          | 45  | 27     | 18   | 3.0      | 1        | 1          | 100         | 1         | -18      | 0.60   |  |
| 121893620                          | 320 | 252    | 68   | 4.0      | 1        | 1          | 100         | 1         | -68      | 0.79   |  |
| 121893620                          | 45  | 27     | 18   | 3.0      | 1        | 1          | 100         | 1         | -18      | 0.60   |  |
| 121897125                          | 93  | 53     | 40   | 4.7      | 1        | 1          | 100         | 1         | -40      | 0.57   |  |
| 121897125                          | 322 | 339    | -17  | 0.9      | 1        | 1          | 100         | 1         | 17       | 1.05   |  |
| 121897606                          | 273 | 226    | 47   | 3.0      | 1        | 1          | 100         | 1         | -47      | 0.83   |  |
| 121890192                          | 7   | 0      | 7    | 3.7      | 1        | 1          | 100         | 1         | -7       | 0.00   |  |
| 121890192                          | 16  | 27     | -11  | 2.4      | 1        | 1          | 100         | 1         | 11       | 1.69   |  |
| 121897488                          | 374 | 390    | -16  | 0.8      | 1        | 1          | 100         | 1         | 16       | 1.04   |  |
| 121897488                          | 8   | 30     | -22  | 5.0      | 0        | 1          | 100         | 1         | 22       | 3.75   |  |
| 121893839                          | 13  | 0      | 13   | 5.1      | 0        | 1          | 100         | 1         | -13      | 0.00   |  |
| 121892073                          | 42  | 27     | 15   | 2.6      | 1        | 1          | 100         | 1         | -15      | 0.64   |  |
| 121890941                          | 19  | 0      | 19   | 6.2      | 0        | 1          | 100         | 1         | -19      | 0.00   |  |
| 121892699                          | 410 | 356    | 54   | 2.8      | 1        | 1          | 100         | 1         | -54      | 0.87   |  |
| 121896733                          | 741 | 794    | -53  | 1.9      | 1        | 2          | 111         | 1         | 53       | 1.07   |  |
| 121896733                          | 463 | 511    | -48  | 2.2      | 1        | 1          | 100         | 1         | 48       | 1.10   |  |
| 121890227                          | 649 | 696    | -47  | 1.8      | 1        | 1          | 100         | 1         | 47       | 1.07   |  |
| 121894922                          | 417 | 443    | -26  | 1.3      | 1        | 1          | 100         | 1         | 26       | 1.06   |  |
| 121893526                          | 581 | 572    | 9    | 0.4      | 1        | 1          | 100         | 1         | -9       | 0.98   |  |
| 121892821                          | 281 | 281    | 0    | 0.0      | 1        | 1          | 100         | 1         | 0        | 1.00   |  |
| 121892821                          | 94  | 96     | -2   | 0.2      | 1        | 1          | 100         | 1         | 2        | 1.02   |  |
| 121892291                          | 39  | 47     | -8   | 1.2      | 1        | 1          | 100         | 1         | 8        | 1.21   |  |
| 121894272                          | 55  | 71     | -16  | 2.0      | 1        | 1          | 100         | 1         | 16       | 1.29   |  |
| 121894272                          | 189 | 263    | -74  | 4.9      | 1        | 1          | 100         | 1         | 74       | 1.39   |  |
| 121893173                          | 226 | 269    | -43  | 2.7      | 1        | 1          | 100         | 1         | 43       | 1.19   |  |
| 121897587                          | 617 | 698    | -81  | 3.2      | 1        | 1          | 100         | 1         | 81       | 1.13   |  |
| 121897884                          | 330 | 239    | 91   | 5.4      | 0        | 1          | 100         | 1         | -91      | 0.72   |  |
| 121891330                          | 456 | 465    | -9   | 0.4      | 1        | 1          | 100         | 1         | 9        | 1.02   |  |
| 121897588                          | 633 | 720    | -87  | 3.3      | 1        | 1          | 100         | 1         | 87       | 1.14   |  |
| 121896281                          | 310 | 328    | -18  | 1.0      | 1        | 1          | 100         | 1         | 18       | 1.06   |  |
| 121896281                          | 68  | 26     | 42   | 6.1      | 0        | 1          | 100         | 1         | -42      | 0.38   |  |
| 121892466                          | 13  | 39     | -26  | 5.1      | 0        | 1          | 100         | 1         | 26       | 3.00   |  |
| 121892466                          | 394 | 410    | -16  | 0.8      | 1        | 1          | 100         | 1         | 16       | 1.04   |  |
| 121891498                          | 313 | 251    | 62   | 3.7      | 1        | 1          | 100         | 1         | -62      | 0.80   |  |

|           |               |               |            |            |            |   |     |            |           |             |
|-----------|---------------|---------------|------------|------------|------------|---|-----|------------|-----------|-------------|
| 121891498 | 313           | 251           | 62         | 3.7        | 1          | 1 | 100 | 1          | -62       | 0.80        |
| 121891498 | 195           | 149           | 46         | 3.5        | 1          | 1 | 100 | 1          | -46       | 0.76        |
| 121891499 | 279           | 359           | -80        | 4.5        | 1          | 1 | 100 | 1          | 80        | 1.29        |
| 121891048 | 121           | 118           | 3          | 0.3        | 1          | 1 | 100 | 1          | -3        | 0.98        |
| 121891072 | 242           | 336           | -94        | 5.5        | 0          | 1 | 100 | 1          | 94        | 1.39        |
| 121893996 | 381           | 459           | -78        | 3.8        | 1          | 1 | 100 | 1          | 78        | 1.20        |
| 121891661 | 99            | 71            | 28         | 3.0        | 1          | 1 | 100 | 1          | -28       | 0.72        |
| 121891608 | 228           | 227           | 1          | 0.1        | 1          | 1 | 100 | 1          | -1        | 1.00        |
| 121891608 | 66            | 96            | -30        | 3.3        | 1          | 1 | 100 | 1          | 30        | 1.45        |
| 121892702 | 63            | 65            | -2         | 0.3        | 1          | 1 | 100 | 1          | 2         | 1.03        |
| 121891660 | 38            | 42            | -4         | 0.6        | 1          | 1 | 100 | 1          | 4         | 1.11        |
| 121892947 | 92            | 72            | 20         | 2.2        | 1          | 1 | 100 | 1          | -20       | 0.78        |
| 121891598 | 79            | 53            | 26         | 3.2        | 1          | 1 | 100 | 1          | -26       | 0.67        |
| 121894677 | 98            | 83            | 15         | 1.6        | 1          | 1 | 100 | 1          | -15       | 0.85        |
| 121891629 | 92            | 72            | 20         | 2.2        | 1          | 1 | 100 | 1          | -20       | 0.78        |
| 121642466 | 104           | 95            | 9          | 0.9        | 1          | 1 | 100 | 1          | -9        | 0.91        |
| 121621121 | 621           | 641           | -20        | 0.8        | 1          | 1 | 100 | 1          | 20        | 1.03        |
| 121890684 | 543           | 557           | -14        | 0.6        | 1          | 1 | 100 | 1          | 14        | 1.03        |
| 121890378 | 343           | 348           | -5         | 0.3        | 1          | 1 | 100 | 1          | 5         | 1.01        |
| 121895710 | 830           | 675           | 155        | 5.7        | 0          | 2 | 125 | 0          | -155      | 0.81        |
| 121895710 | 287           | 327           | -40        | 2.3        | 1          | 1 | 100 | 1          | 40        | 1.14        |
| 121899789 | 35            | 22            | 13         | 2.4        | 1          | 1 | 100 | 1          | -13       | 0.63        |
| 121899789 | 214           | 232           | -18        | 1.2        | 1          | 1 | 100 | 1          | 18        | 1.08        |
| 121899789 | 13            | 18            | -5         | 1.3        | 1          | 1 | 100 | 1          | 5         | 1.38        |
| 200002261 | 3             | 0             | 3          | 2.4        | 1          | 1 | 100 | 1          | -3        | 0.00        |
| 200002257 | 3             | 0             | 3          | 2.4        | 1          | 1 | 100 | 1          | -3        | 0.00        |
| 200002265 | 22            | 60            | -38        | 5.9        | 0          | 1 | 100 | 1          | 38        | 2.73        |
| 200002265 | 119           | 75            | 44         | 4.5        | 1          | 1 | 100 | 1          | -44       | 0.63        |
| 200002277 | 32            | 31            | 1          | 0.2        | 1          | 1 | 100 | 1          | -1        | 0.97        |
| 200002282 | 11            | 39            | -28        | 5.6        | 0          | 1 | 100 | 1          | 28        | 3.55        |
| 200002288 | 11            | 20            | -9         | 2.3        | 1          | 1 | 100 | 1          | 9         | 1.82        |
| 200002288 | 119           | 101           | 18         | 1.7        | 1          | 1 | 100 | 1          | -18       | 0.85        |
| 200002297 | 7             | 8             | -1         | 0.4        | 1          | 1 | 100 | 1          | 1         | 1.14        |
| 200002297 | 66            | 95            | -29        | 3.2        | 1          | 1 | 100 | 1          | 29        | 1.44        |
| 200002307 | 495           | 522           | -27        | 1.2        | 1          | 1 | 100 | 1          | 27        | 1.05        |
| 121894612 | 33            | 34            | -1         | 0.2        | 1          | 1 | 100 | 1          | 1         | 1.03        |
| 200002316 | 31            | 0             | 31         | 7.9        | 0          | 1 | 100 | 1          | -31       | 0.00        |
| 200002243 | 150           | 128           | 22         | 1.9        | 1          | 1 | 100 | 1          | -22       | 0.85        |
| 200002243 | 9             | 20            | -11        | 2.9        | 1          | 1 | 100 | 1          | 11        | 2.22        |
| 121895000 | 66            | 25            | 41         | 6.1        | 0          | 1 | 100 | 1          | -41       | 0.38        |
| 121895000 | 36            | 11            | 25         | 5.2        | 0          | 1 | 100 | 1          | -25       | 0.31        |
| 200002468 | 194           | 250           | -56        | 3.8        | 1          | 1 | 100 | 1          | 56        | 1.29        |
| 200002468 | 127           | 85            | 42         | 4.1        | 1          | 1 | 100 | 1          | -42       | 0.67        |
| 200002478 | 35            | 0             | 35         | 8.4        | 0          | 1 | 100 | 1          | -35       | 0.00        |
| 200002472 | 42            | 64            | -22        | 3.0        | 1          | 1 | 100 | 1          | 22        | 1.52        |
| 200002493 | 73            | 109           | -36        | 3.8        | 1          | 1 | 100 | 1          | 36        | 1.49        |
| 200002493 | 37            | 24            | 13         | 2.4        | 1          | 1 | 100 | 1          | -13       | 0.65        |
| 121892794 | 377           | 369           | 8          | 0.4        | 1          | 1 | 100 | 1          | -8        | 0.98        |
| 121892794 | 40            | 42            | -2         | 0.3        | 1          | 1 | 100 | 1          | 2         | 1.05        |
| 200002518 | 151           | 128           | 23         | 1.9        | 1          | 1 | 100 | 1          | -23       | 0.85        |
| 200002518 | 340           | 359           | -19        | 1.0        | 1          | 1 | 100 | 1          | 19        | 1.06        |
| 121895919 | 113           | 117           | -4         | 0.4        | 1          | 1 | 100 | 1          | 4         | 1.04        |
| 200002520 | 223           | 241           | -18        | 1.2        | 1          | 1 | 100 | 1          | 18        | 1.08        |
| 121892555 | 1421          | 1318          | 103        | 2.8        | 1          | 2 | 213 | 1          | -103      | 0.93        |
| 121892555 | 55            | 32            | 23         | 3.5        | 1          | 1 | 100 | 1          | -23       | 0.58        |
| 200002531 | 43            | 63            | -20        | 2.7        | 1          | 1 | 100 | 1          | 20        | 1.47        |
| 200002555 | 789           | 885           | -96        | 3.3        | 1          | 2 | 118 | 1          | 96        | 1.12        |
| 200002555 | 45            | 45            | 0          | 0.0        | 1          | 1 | 100 | 1          | 0         | 1.00        |
| 200002555 | 450           | 415           | 35         | 1.7        | 1          | 1 | 100 | 1          | -35       | 0.92        |
| 200002390 | 12            | 52            | -40        | 7.1        | 0          | 1 | 100 | 1          | 40        | 4.33        |
| 121892925 | 483           | 489           | -6         | 0.3        | 1          | 1 | 100 | 1          | 6         | 1.01        |
| 121890590 | 1144          | 1244          | -100       | 2.9        | 1          | 2 | 172 | 1          | 100       | 1.09        |
| 121890590 | 44            | 77            | -33        | 4.2        | 1          | 1 | 100 | 1          | 33        | 1.75        |
| 200002557 | 829           | 874           | -45        | 1.5        | 1          | 2 | 124 | 1          | 45        | 1.05        |
| 200002556 | 85            | 85            | 0          | 0.0        | 1          | 1 | 100 | 1          | 0         | 1.00        |
| 200002558 | 137           | 160           | -23        | 1.9        | 1          | 1 | 100 | 1          | 23        | 1.17        |
| 200002560 | 53            | 44            | 9          | 1.3        | 1          | 1 | 100 | 1          | -9        | 0.83        |
| 200002377 | 10            | 0             | 10         | 4.5        | 1          | 1 | 100 | 1          | -10       | 0.00        |
| 200002565 | 90            | 83            | 7          | 0.8        | 1          | 1 | 100 | 1          | -7        | 0.92        |
| 200002565 | 381           | 459           | -78        | 3.8        | 1          | 1 | 100 | 1          | 78        | 1.20        |
| 200002564 | 5             | 0             | 5          | 3.2        | 1          | 1 | 100 | 1          | -5        | 0.00        |
| 121891556 | 3             | 5             | -2         | 1.0        | 1          | 1 | 100 | 1          | 2         | 1.67        |
| 121891556 | 16            | 0             | 16         | 5.7        | 0          | 1 | 100 | 1          | -16       | 0.00        |
| 200002549 | 7             | 5             | 2          | 0.8        | 1          | 1 | 100 | 1          | -2        | 0.71        |
| 200002571 | 155           | 112           | 43         | 3.7        | 1          | 1 | 100 | 1          | -43       | 0.72        |
| 200002573 | 117           | 63            | 54         | 5.7        | 0          | 1 | 100 | 1          | -54       | 0.54        |
| 200002573 | 22            | 0             | 22         | 6.6        | 0          | 1 | 100 | 1          | -22       | 0.00        |
|           | <b>35,608</b> | <b>35,694</b> | <b>-86</b> | <b>0.5</b> | <b>128</b> |   |     | <b>145</b> | <b>86</b> | <b>1.00</b> |

### AM Peak Link Validation

| NTM AM Total Link Flow Validation |               |               |            |            |           |            |             |           |             |             |  |
|-----------------------------------|---------------|---------------|------------|------------|-----------|------------|-------------|-----------|-------------|-------------|--|
| Counts :                          |               | 14            |            | RESULT =   |           | 93%        |             | RESULT =  |             | 93%         |  |
| Total Traffic                     |               |               |            | REQD =     |           | 85%        |             | REQD =    |             | 85%         |  |
| Link Number                       | Obs           | Mod           |            | GEH        | GEH TEST  | CLASS TEST | Target Diff | Flow Test | ACT DIFF    | FACTOR      |  |
| 3790                              | 1249          | 1192          | 57         | 1.6        | 1         | 2          | 187         | 1         | -57         | 0.95        |  |
| 52041                             | 1871          | 1867          | 4          | 0.1        | 1         | 2          | 281         | 1         | -4          | 1.00        |  |
| 52401                             | 1646          | 1617          | 29         | 0.7        | 1         | 2          | 247         | 1         | -29         | 0.98        |  |
| 52456                             | 2051          | 1972          | 79         | 1.8        | 1         | 2          | 308         | 1         | -79         | 0.96        |  |
| 52718                             | 1164          | 1032          | 132        | 4.0        | 1         | 2          | 175         | 1         | -132        | 0.89        |  |
| 52938                             | 1065          | 968           | 97         | 3.0        | 1         | 2          | 160         | 1         | -97         | 0.91        |  |
| 590511931                         | 1229          | 1364          | -135       | 3.7        | 1         | 2          | 184         | 1         | 135         | 1.11        |  |
| 726245138                         | 746           | 790           | -44        | 1.6        | 1         | 2          | 112         | 1         | 44          | 1.06        |  |
| 740146667                         | 2673          | 2433          | 240        | 4.7        | 1         | 2          | 401         | 1         | -240        | 0.91        |  |
| 2147479948                        | 132           | 112           | 20         | 1.8        | 1         | 1          | 100         | 1         | -20         | 0.85        |  |
| 2147480014                        | 653           | 608           | 45         | 1.8        | 1         | 1          | 100         | 1         | -45         | 0.93        |  |
| 2147480014                        | 342           | 443           | -101       | 5.1        | 0         | 1          | 100         | 0         | 101         | 1.30        |  |
| 2147481701                        | 2969          | 2713          | 256        | 4.8        | 1         | 2          | 445         | 1         | -256        | 0.91        |  |
| 2147481719                        | 2064          | 2191          | -127       | 2.8        | 1         | 2          | 310         | 1         | 127         | 1.06        |  |
|                                   | <b>19,854</b> | <b>19,302</b> | <b>552</b> | <b>3.9</b> | <b>13</b> |            |             | <b>13</b> | <b>-552</b> | <b>0.97</b> |  |

### PM Peak Link Validation

| NTM PM Total Link Flow Validation |               |               |              |            |           |            |             |           |               |             |  |
|-----------------------------------|---------------|---------------|--------------|------------|-----------|------------|-------------|-----------|---------------|-------------|--|
| Counts :                          |               | 14            |              | RESULT =   |           | 86%        |             | RESULT =  |               | 93%         |  |
| Total Traffic                     |               |               |              | REQD =     |           | 85%        |             | REQD =    |               | 85%         |  |
| Link Number                       | Obs           | Mod           |              | GEH        | GEH TEST  | CLASS TEST | Target Diff | Flow Test | ACT DIFF      | FACTOR      |  |
| 3790                              | 2745          | 2481          | 264          | 5.2        | 0         | 2          | 412         | 1         | -264          | 0.90        |  |
| 52041                             | 3363          | 3215          | 148          | 2.6        | 1         | 2          | 504         | 1         | -148          | 0.96        |  |
| 52401                             | 953           | 1026          | -73          | 2.3        | 1         | 2          | 143         | 1         | 73            | 1.08        |  |
| 52456                             | 3714          | 3697          | 17           | 0.3        | 1         | 2          | 557         | 1         | -17           | 1.00        |  |
| 52718                             | 2419          | 2285          | 134          | 2.8        | 1         | 2          | 363         | 1         | -134          | 0.94        |  |
| 52938                             | 2303          | 1879          | 424          | 9.3        | 0         | 2          | 345         | 0         | -424          | 0.82        |  |
| 590511931                         | 2221          | 2341          | -120         | 2.5        | 1         | 2          | 333         | 1         | 120           | 1.05        |  |
| 726245138                         | 1477          | 1399          | 78           | 2.1        | 1         | 2          | 222         | 1         | -78           | 0.95        |  |
| 740146667                         | 1652          | 1506          | 146          | 3.7        | 1         | 2          | 248         | 1         | -146          | 0.91        |  |
| 2147479948                        | 84            | 120           | -36          | 3.6        | 1         | 1          | 100         | 1         | 36            | 1.43        |  |
| 2147480014                        | 394           | 446           | -52          | 2.5        | 1         | 1          | 100         | 1         | 52            | 1.13        |  |
| 2147480014                        | 587           | 593           | -6           | 0.2        | 1         | 1          | 100         | 1         | 6             | 1.01        |  |
| 2147481701                        | 1729          | 1552          | 177          | 4.4        | 1         | 2          | 259         | 1         | -177          | 0.90        |  |
| 2147481719                        | 1203          | 1185          | 18           | 0.5        | 1         | 2          | 180         | 1         | -18           | 0.99        |  |
|                                   | <b>24,844</b> | <b>23,725</b> | <b>1,119</b> | <b>7.2</b> | <b>12</b> |            |             | <b>13</b> | <b>-1,119</b> | <b>0.95</b> |  |

### AM Peak Turn Validation

| AM Total Turning Flow Validation |               |               |       |        |          |            |             |           |          |        |
|----------------------------------|---------------|---------------|-------|--------|----------|------------|-------------|-----------|----------|--------|
| Counts :                         |               | 79            |       |        | RESULT = |            | 82%         |           | 95%      |        |
| Total Traffic                    |               |               |       | REQD = |          | 85%        |             | REQD =    |          | 85%    |
| Link Number                      | Obs           | Mod           | Diff  | GBH    | GEH TEST | CLASS TEST | Target Diff | Flow Test | ACT DIFF | FACTOR |
| 2000002072                       | 243           | 231           | 12    | 0.8    | 1        | 1          | 100         | 1         | -12      | 0.95   |
| 2000002065                       | 534           | 523           | 11    | 0.5    | 1        | 1          | 100         | 1         | -11      | 0.98   |
| 2000002066                       | 482           | 423           | 59    | 2.8    | 1        | 1          | 100         | 1         | -59      | 0.88   |
| 2000002071                       | 482           | 423           | 59    | 2.8    | 1        | 1          | 100         | 1         | -59      | 0.88   |
| 2000002070                       | 662           | 566           | 96    | 3.9    | 1        | 1          | 100         | 1         | -96      | 0.85   |
| 2000002070                       | 62            | 87            | -25   | 2.9    | 1        | 1          | 100         | 1         | 25       | 1.40   |
| 2000002069                       | 346           | 345           | 1     | 0.1    | 1        | 1          | 100         | 1         | -1       | 1.00   |
| 2000002068                       | 345           | 345           | 0     | 0.0    | 1        | 1          | 100         | 1         | 0        | 1.00   |
| 121895468                        | 207           | 282           | -75   | 4.8    | 1        | 1          | 100         | 1         | 75       | 1.36   |
| 121891052                        | 9             | 0             | 9     | 4.2    | 1        | 1          | 100         | 1         | -9       | 0.00   |
| 121898092                        | 90            | 67            | 23    | 2.6    | 1        | 1          | 100         | 1         | -23      | 0.74   |
| 121892862                        | 54            | 0             | 54    | 10.4   | 0        | 1          | 100         | 1         | -54      | 0.00   |
| 121894501                        | 419           | 447           | -28   | 1.3    | 1        | 1          | 100         | 1         | 28       | 1.07   |
| 121890193                        | 301           | 316           | -15   | 0.9    | 1        | 1          | 100         | 1         | 15       | 1.05   |
| 121890193                        | 15            | 12            | 3     | 0.8    | 1        | 1          | 100         | 1         | -3       | 0.80   |
| 121890515                        | 379           | 439           | -60   | 3.0    | 1        | 1          | 100         | 1         | 60       | 1.16   |
| 121890383                        | 37            | 14            | 23    | 4.6    | 1        | 1          | 100         | 1         | -23      | 0.38   |
| 121896748                        | 180           | 203           | -23   | 1.7    | 1        | 1          | 100         | 1         | 23       | 1.13   |
| 121893478                        | 127           | 160           | -33   | 2.8    | 1        | 1          | 100         | 1         | 33       | 1.26   |
| 121892820                        | 345           | 260           | 85    | 4.9    | 1        | 1          | 100         | 1         | -85      | 0.75   |
| 121895471                        | 482           | 473           | 9     | 0.4    | 1        | 1          | 100         | 1         | -9       | 0.98   |
| 121893943                        | 402           | 360           | 42    | 2.2    | 1        | 1          | 100         | 1         | -42      | 0.90   |
| 121894400                        | 1212          | 1210          | 2     | 0.1    | 1        | 2          | 182         | 1         | -2       | 1.00   |
| 121891012                        | 1219          | 1192          | 27    | 0.8    | 1        | 2          | 183         | 1         | -27      | 0.98   |
| 121898508                        | 170           | 156           | 14    | 1.1    | 1        | 1          | 100         | 1         | -14      | 0.92   |
| 121605492                        | 434           | 550           | -116  | 5.2    | 0        | 1          | 100         | 0         | 116      | 1.27   |
| 121641080                        | 93            | 24            | 69    | 9.0    | 0        | 1          | 100         | 1         | -69      | 0.26   |
| 121891475                        | 102           | 92            | 10    | 1.0    | 1        | 1          | 100         | 1         | -10      | 0.90   |
| 121893878                        | 75            | 86            | -11   | 1.2    | 1        | 1          | 100         | 1         | 11       | 1.15   |
| 121893236                        | 302           | 316           | -14   | 0.8    | 1        | 1          | 100         | 1         | 14       | 1.05   |
| 121892073                        | 313           | 316           | -3    | 0.2    | 1        | 1          | 100         | 1         | 3        | 1.01   |
| 121894922                        | 518           | 399           | 119   | 5.6    | 0        | 1          | 100         | 0         | -119     | 0.77   |
| 121893526                        | 538           | 554           | -16   | 0.7    | 1        | 1          | 100         | 1         | 16       | 1.03   |
| 121890062                        | 522           | 534           | -12   | 0.5    | 1        | 1          | 100         | 1         | 12       | 1.02   |
| 121892991                        | 401           | 350           | 51    | 2.6    | 1        | 1          | 100         | 1         | -51      | 0.87   |
| 121639135                        | 133           | 134           | -1    | 0.1    | 1        | 1          | 100         | 1         | 1        | 1.01   |
| 121892291                        | 144           | 158           | -14   | 1.1    | 1        | 1          | 100         | 1         | 14       | 1.10   |
| 121897587                        | 309           | 201           | 108   | 6.8    | 0        | 1          | 100         | 0         | -108     | 0.65   |
| 121891499                        | 184           | 154           | 30    | 2.3    | 1        | 1          | 100         | 1         | -30      | 0.84   |
| 121894696                        | 293           | 263           | 30    | 1.8    | 1        | 1          | 100         | 1         | -30      | 0.90   |
| 121894696                        | 27            | 1             | 26    | 6.9    | 0        | 1          | 100         | 1         | -26      | 0.04   |
| 121891048                        | 279           | 305           | -26   | 1.5    | 1        | 1          | 100         | 1         | 26       | 1.09   |
| 121891072                        | 4             | 98            | -94   | 13.2   | 0        | 1          | 100         | 1         | 94       | 24.50  |
| 121893802                        | 55            | 56            | -1    | 0.1    | 1        | 1          | 100         | 1         | 1        | 1.02   |
| 121891660                        | 72            | 16            | 56    | 8.4    | 0        | 1          | 100         | 1         | -56      | 0.22   |
| 121892947                        | 51            | 0             | 51    | 10.1   | 0        | 1          | 100         | 1         | -51      | 0.00   |
| 121894678                        | 62            | 40            | 22    | 3.1    | 1        | 1          | 100         | 1         | -22      | 0.65   |
| 121891598                        | 62            | 40            | 22    | 3.1    | 1        | 1          | 100         | 1         | -22      | 0.65   |
| 121891630                        | 67            | 0             | 67    | 11.6   | 0        | 1          | 100         | 1         | -67      | 0.00   |
| 121891630                        | 51            | 40            | 11    | 1.6    | 1        | 1          | 100         | 1         | -11      | 0.78   |
| 121893181                        | 31            | 25            | 6     | 1.1    | 1        | 1          | 100         | 1         | -6       | 0.81   |
| 121893181                        | 126           | 41            | 85    | 9.3    | 0        | 1          | 100         | 1         | -85      | 0.33   |
| 121894677                        | 67            | 0             | 67    | 11.6   | 0        | 1          | 100         | 1         | -67      | 0.00   |
| 121890684                        | 424           | 323           | 101   | 5.2    | 0        | 1          | 100         | 0         | -101     | 0.76   |
| 121890738                        | 511           | 508           | 3     | 0.1    | 1        | 1          | 100         | 1         | -3       | 0.99   |
| 121890738                        | 421           | 375           | 46    | 2.3    | 1        | 1          | 100         | 1         | -46      | 0.89   |
| 121890378                        | 417           | 513           | -96   | 4.5    | 1        | 1          | 100         | 1         | 96       | 1.23   |
| 121899789                        | 206           | 258           | -52   | 3.4    | 1        | 1          | 100         | 1         | 52       | 1.25   |
| 2000002261                       | 170           | 190           | -20   | 1.5    | 1        | 1          | 100         | 1         | 20       | 1.12   |
| 2000002282                       | 33            | 22            | 11    | 2.1    | 1        | 1          | 100         | 1         | -11      | 0.67   |
| 2000002297                       | 10            | 0             | 10    | 4.5    | 1        | 1          | 100         | 1         | -10      | 0.00   |
| 121894612                        | 11            | 11            | 0     | 0.0    | 1        | 1          | 100         | 1         | 0        | 1.00   |
| 121891751                        | 40            | 77            | -37   | 4.8    | 1        | 1          | 100         | 1         | 37       | 1.93   |
| 121891751                        | 36            | 84            | -48   | 6.2    | 0        | 1          | 100         | 1         | 48       | 2.33   |
| 121890064                        | 484           | 482           | 2     | 0.1    | 1        | 1          | 100         | 1         | -2       | 1.00   |
| 2000002521                       | 23            | 20            | 3     | 0.6    | 1        | 1          | 100         | 1         | -3       | 0.87   |
| 2000002521                       | 315           | 305           | 10    | 0.6    | 1        | 1          | 100         | 1         | -10      | 0.97   |
| 2000002524                       | 136           | 128           | 8     | 0.7    | 1        | 1          | 100         | 1         | -8       | 0.94   |
| 2000002531                       | 23            | 21            | 2     | 0.4    | 1        | 1          | 100         | 1         | -2       | 0.91   |
| 121892925                        | 7             | 24            | -17   | 4.3    | 1        | 1          | 100         | 1         | 17       | 3.43   |
| 2000002557                       | 401           | 350           | 51    | 2.6    | 1        | 1          | 100         | 1         | -51      | 0.87   |
| 2000002558                       | 83            | 89            | -6    | 0.6    | 1        | 1          | 100         | 1         | 6        | 1.07   |
| 2000002558                       | 55            | 56            | -1    | 0.1    | 1        | 1          | 100         | 1         | 1        | 1.02   |
| 2000002563                       | 33            | 10            | 23    | 5.0    | 1        | 1          | 100         | 1         | -23      | 0.30   |
| 2000002563                       | 21            | 36            | -15   | 2.8    | 1        | 1          | 100         | 1         | 15       | 1.71   |
| 2000002563                       | 19            | 14            | 5     | 1.2    | 1        | 1          | 100         | 1         | -5       | 0.74   |
| 2000002377                       | 115           | 126           | -11   | 1.0    | 1        | 1          | 100         | 1         | 11       | 1.10   |
| 2000002293                       | 18123         | 17548         | 575   | 4.3    | 1        | 2          | 2718        | 1         | -575     | 0.97   |
| 2000002573                       | 0             | 8             | -8    | 4.0    | 1        | 1          | 100         | 1         | 8        | #DV/0! |
|                                  | <b>36,236</b> | <b>34,905</b> | 1,331 | 7.1    | 65       |            |             | 75        | -1,331   | 0.96   |

### PM Peak Turn Validation

| PM Total Turning Flow Validation |               |               |           |            |           |            |             |           |            |             |     |
|----------------------------------|---------------|---------------|-----------|------------|-----------|------------|-------------|-----------|------------|-------------|-----|
| Counts :                         |               | 79            |           | RESULT =   |           |            | 85%         |           | RESULT =   |             | 97% |
| Total Traffic                    |               | REQD =        |           | 85%        |           |            | REQD =      |           | 85%        |             |     |
| Link Number                      | Obs           | Mod           | Diff      | GEH        | GEH TEST  | CLASS TEST | Target Diff | Flow Test | ACT DIFF   | FACTOR      |     |
| 2000002072                       | 214           | 284           | -70       | 4.4        | 1         | 1          | 100         | 1         | 70         | 1.33        |     |
| 2000002065                       | 822           | 780           | 42        | 1.5        | 1         | 2          | 123         | 1         | -42        | 0.95        |     |
| 2000002066                       | 329           | 300           | 29        | 1.6        | 1         | 1          | 100         | 1         | -29        | 0.91        |     |
| 2000002071                       | 329           | 300           | 29        | 1.6        | 1         | 1          | 100         | 1         | -29        | 0.91        |     |
| 2000002070                       | 534           | 456           | 78        | 3.5        | 1         | 1          | 100         | 1         | -78        | 0.85        |     |
| 2000002070                       | 105           | 127           | -22       | 2.0        | 1         | 1          | 100         | 1         | 22         | 1.21        |     |
| 2000002069                       | 308           | 373           | -65       | 3.5        | 1         | 1          | 100         | 1         | 65         | 1.21        |     |
| 2000002068                       | 308           | 373           | -65       | 3.5        | 1         | 1          | 100         | 1         | 65         | 1.21        |     |
| 121895468                        | 115           | 96            | 19        | 1.8        | 1         | 1          | 100         | 1         | -19        | 0.83        |     |
| 121891052                        | 9             | 0             | 9         | 4.2        | 1         | 1          | 100         | 1         | -9         | 0.00        |     |
| 121898092                        | 57            | 32            | 25        | 3.7        | 1         | 1          | 100         | 1         | -25        | 0.56        |     |
| 121892862                        | 70            | 0             | 70        | 11.8       | 0         | 1          | 100         | 1         | -70        | 0.00        |     |
| 121894501                        | 232           | 276           | -44       | 2.8        | 1         | 1          | 100         | 1         | 44         | 1.19        |     |
| 121890193                        | 396           | 381           | 15        | 0.8        | 1         | 1          | 100         | 1         | -15        | 0.96        |     |
| 121890193                        | 12            | 9             | 3         | 0.9        | 1         | 1          | 100         | 1         | -3         | 0.75        |     |
| 121890515                        | 454           | 551           | -97       | 4.3        | 1         | 1          | 100         | 1         | 97         | 1.21        |     |
| 121890383                        | 23            | 24            | -1        | 0.2        | 1         | 1          | 100         | 1         | 1          | 1.04        |     |
| 121896748                        | 405           | 442           | -37       | 1.8        | 1         | 1          | 100         | 1         | 37         | 1.09        |     |
| 121893478                        | 85            | 117           | -32       | 3.2        | 1         | 1          | 100         | 1         | 32         | 1.38        |     |
| 121892820                        | 239           | 281           | -42       | 2.6        | 1         | 1          | 100         | 1         | 42         | 1.18        |     |
| 121895471                        | 321           | 359           | -38       | 2.1        | 1         | 1          | 100         | 1         | 38         | 1.12        |     |
| 121893943                        | 279           | 316           | -37       | 2.1        | 1         | 1          | 100         | 1         | 37         | 1.13        |     |
| 121894400                        | 821           | 929           | -108      | 3.7        | 1         | 2          | 123         | 1         | 108        | 1.13        |     |
| 121891012                        | 847           | 910           | -63       | 2.1        | 1         | 2          | 127         | 1         | 63         | 1.07        |     |
| 121898508                        | 141           | 120           | 21        | 1.8        | 1         | 1          | 100         | 1         | -21        | 0.85        |     |
| 121605492                        | 537           | 535           | 2         | 0.1        | 1         | 1          | 100         | 1         | -2         | 1.00        |     |
| 121641080                        | 162           | 55            | 107       | 10.3       | 0         | 1          | 100         | 0         | -107       | 0.34        |     |
| 121891475                        | 186           | 208           | -22       | 1.6        | 1         | 1          | 100         | 1         | 22         | 1.12        |     |
| 121893878                        | 161           | 177           | -16       | 1.2        | 1         | 1          | 100         | 1         | 16         | 1.10        |     |
| 121893236                        | 403           | 381           | 22        | 1.1        | 1         | 1          | 100         | 1         | -22        | 0.95        |     |
| 121892073                        | 397           | 381           | 16        | 0.8        | 1         | 1          | 100         | 1         | -16        | 0.96        |     |
| 121894922                        | 627           | 605           | 22        | 0.9        | 1         | 1          | 100         | 1         | -22        | 0.96        |     |
| 121893526                        | 555           | 611           | -56       | 2.3        | 1         | 1          | 100         | 1         | 56         | 1.10        |     |
| 121890062                        | 483           | 582           | -99       | 4.3        | 1         | 1          | 100         | 1         | 99         | 1.20        |     |
| 121892991                        | 400           | 456           | -56       | 2.7        | 1         | 1          | 100         | 1         | 56         | 1.14        |     |
| 121639135                        | 173           | 152           | 21        | 1.6        | 1         | 1          | 100         | 1         | -21        | 0.88        |     |
| 121892291                        | 323           | 254           | 69        | 4.1        | 1         | 1          | 100         | 1         | -69        | 0.79        |     |
| 121897587                        | 346           | 262           | 84        | 4.8        | 1         | 1          | 100         | 1         | -84        | 0.76        |     |
| 121891499                        | 253           | 171           | 82        | 5.6        | 0         | 1          | 100         | 1         | -82        | 0.68        |     |
| 121894696                        | 251           | 181           | 70        | 4.8        | 1         | 1          | 100         | 1         | -70        | 0.72        |     |
| 121894696                        | 81            | 40            | 41        | 5.3        | 0         | 1          | 100         | 1         | -41        | 0.49        |     |
| 121891048                        | 233           | 278           | -45       | 2.8        | 1         | 1          | 100         | 1         | 45         | 1.19        |     |
| 121891072                        | 9             | 54            | -45       | 8.0        | 0         | 1          | 100         | 1         | 45         | 6.00        |     |
| 121893802                        | 95            | 59            | 36        | 4.1        | 1         | 1          | 100         | 1         | -36        | 0.62        |     |
| 121891660                        | 162           | 112           | 50        | 4.3        | 1         | 1          | 100         | 1         | -50        | 0.69        |     |
| 121892947                        | 92            | 72            | 20        | 2.2        | 1         | 1          | 100         | 1         | -20        | 0.78        |     |
| 121894678                        | 101           | 83            | 18        | 1.9        | 1         | 1          | 100         | 1         | -18        | 0.82        |     |
| 121891598                        | 101           | 83            | 18        | 1.9        | 1         | 1          | 100         | 1         | -18        | 0.82        |     |
| 121891630                        | 112           | 72            | 40        | 4.2        | 1         | 1          | 100         | 1         | -40        | 0.64        |     |
| 121891630                        | 94            | 83            | 11        | 1.2        | 1         | 1          | 100         | 1         | -11        | 0.88        |     |
| 121893181                        | 25            | 24            | 1         | 0.2        | 1         | 1          | 100         | 1         | -1         | 0.96        |     |
| 121893181                        | 142           | 80            | 62        | 5.9        | 0         | 1          | 100         | 1         | -62        | 0.56        |     |
| 121894677                        | 112           | 72            | 40        | 4.2        | 1         | 1          | 100         | 1         | -40        | 0.64        |     |
| 121890684                        | 308           | 312           | -4        | 0.2        | 1         | 1          | 100         | 1         | 4          | 1.01        |     |
| 121890738                        | 546           | 467           | 79        | 3.5        | 1         | 1          | 100         | 1         | -79        | 0.86        |     |
| 121890738                        | 592           | 520           | 72        | 3.1        | 1         | 1          | 100         | 1         | -72        | 0.88        |     |
| 121890378                        | 474           | 481           | -7        | 0.3        | 1         | 1          | 100         | 1         | 7          | 1.01        |     |
| 121899789                        | 222           | 276           | -54       | 3.4        | 1         | 1          | 100         | 1         | 54         | 1.24        |     |
| 2000002261                       | 131           | 54            | 77        | 8.0        | 0         | 1          | 100         | 1         | -77        | 0.41        |     |
| 2000002282                       | 62            | 43            | 19        | 2.6        | 1         | 1          | 100         | 1         | -19        | 0.69        |     |
| 2000002297                       | 11            | 0             | 11        | 4.7        | 1         | 1          | 100         | 1         | -11        | 0.00        |     |
| 121894612                        | 20            | 0             | 20        | 6.3        | 0         | 1          | 100         | 1         | -20        | 0.00        |     |
| 121891751                        | 71            | 141           | -70       | 6.8        | 0         | 1          | 100         | 1         | 70         | 1.99        |     |
| 121891751                        | 58            | 30            | 28        | 4.2        | 1         | 1          | 100         | 1         | -28        | 0.52        |     |
| 121890064                        | 308           | 350           | -42       | 2.3        | 1         | 1          | 100         | 1         | 42         | 1.14        |     |
| 2000002521                       | 58            | 10            | 48        | 8.2        | 0         | 1          | 100         | 1         | -48        | 0.17        |     |
| 2000002521                       | 178           | 99            | 79        | 6.7        | 0         | 1          | 100         | 1         | -79        | 0.56        |     |
| 2000002524                       | 126           | 109           | 17        | 1.6        | 1         | 1          | 100         | 1         | -17        | 0.87        |     |
| 2000002531                       | 51            | 91            | -40       | 4.7        | 1         | 1          | 100         | 1         | 40         | 1.78        |     |
| 121892925                        | 17            | 10            | 7         | 1.9        | 1         | 1          | 100         | 1         | -7         | 0.59        |     |
| 2000002557                       | 400           | 456           | -56       | 2.7        | 1         | 1          | 100         | 1         | 56         | 1.14        |     |
| 2000002558                       | 244           | 298           | -54       | 3.3        | 1         | 1          | 100         | 1         | 54         | 1.22        |     |
| 2000002558                       | 91            | 59            | 32        | 3.7        | 1         | 1          | 100         | 1         | -32        | 0.65        |     |
| 2000002563                       | 51            | 26            | 25        | 4.0        | 1         | 1          | 100         | 1         | -25        | 0.51        |     |
| 2000002563                       | 35            | 48            | -13       | 2.0        | 1         | 1          | 100         | 1         | 13         | 1.37        |     |
| 2000002563                       | 3             | 7             | -4        | 1.8        | 1         | 1          | 100         | 1         | 4          | 2.33        |     |
| 2000002377                       | 171           | 329           | -158      | 10.0       | 0         | 1          | 100         | 0         | 158        | 1.92        |     |
| 2000002293                       | 18515         | 18565         | -50       | 0.4        | 1         | 2          | 2777        | 1         | 50         | 1.00        |     |
| 2000002573                       | 0             | 4             | -4        | 2.8        | 1         | 1          | 100         | 1         | 4          | #DN/0!      |     |
|                                  | <b>36,814</b> | <b>36,744</b> | <b>70</b> | <b>0.4</b> | <b>67</b> |            |             | <b>77</b> | <b>-70</b> | <b>1.00</b> |     |



# **Appendix B**

## **Practical Capacity**

### *M11/N11 Practical Capacity*

In order to refine the practical capacity for the sections of the M11/N11 under consideration an assessment of the two TII TMU counters on the M11/N11 was undertaken; the first on the M11 between Junction 5 (Bray North) and Junction 6 (Bray South), and the second on the N11 between Junction 8 (Kilmacanogue) and Junction 9 (Glen of the Downs).

The flow of traffic during the AM and PM peak periods (06:00 – 09:00 & 16:00 – 17:00) was plotted against speed in order to identify the point when flow breakdown occurs, which, for this study is assumed to be when average speeds reduce to below 80kph (Level of Service D).

Data for each traffic lane for each working day in May 2015 was used as part of the assessment and the flow/speed relationship based on 5 mins time intervals during the peak periods was utilised. Traffic flows within the 85<sup>th</sup> percentile speed during the peak periods was isolated.

#### *M11 Junction 5 (Bray Central) – Junction 6 (Bray South)*

The practical capacity of the section of the M11 between Junction 5 (Bray Central) and Junction 6 (Bray South) was estimated using data from the TII TMU counter (Site No. 20111). Table B.1 provides a summary of the assessment and Figures B1 to B4 illustrate the TMU flow/speed data used as part of the assessment.

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*Table B.1: Practical Capacity (M11 Junction 5 – Junction 6)*

| Lane                    | Northbound                            | Southbound                            |
|-------------------------|---------------------------------------|---------------------------------------|
|                         | AM Practical Capacity (vehicles/hour) | PM Practical Capacity (vehicles/hour) |
| <b>Outside</b>          | 2,688                                 | 2,136                                 |
| <b>Nearside</b>         | 2,004                                 | 1,716                                 |
| <b>Combined</b>         | <b>4,692</b>                          | <b>3,852</b>                          |
| <b>Average per Lane</b> | <b>2,346</b>                          | <b>1,926</b>                          |

It should be noted that the southbound average practical capacity of 1,926 vehicles/hour reconfirms the value quoted in the GDA lane capacity study for this location of 1,900 vehicles/hour.

The capacity of the southbound lanes south of this location is impacted by the combination of several issues between Junction 6 and Junction 8 such as the uphill gradient of the N11, the change to dual carriageway standard with 100km/hr speed limit, a number of direct accesses, and weaving/merging associated with two left on / left off junctions. Therefore the southbound carriageway between Junctions 6 and 8 will have a lower practical capacity.

#### *N11 Junction 8 (Kilmacanogue) – Junction 9 (Glen of the Downs)*

The practical capacity of the section of the N11 between Junction 8 (Kilmacanogue) and Junction 9 (Glen of the Downs) in the northbound direction was estimated using data from the TII TMU counter (Site No. 20111). Table B.2 provides a summary of the assessment which is based on the TMU flow/speed data provided (Figures B5 & B6).

*Table B.2: Practical Capacity (N11 Junction 8 – Junction 9)*

| Lane                    | Northbound                           |
|-------------------------|--------------------------------------|
|                         | AM Practical Capacity(vehicles/hour) |
| <b>Outside</b>          | 2,004                                |
| <b>Nearside</b>         | 1,533                                |
| <b>Combined</b>         | <b>3,537</b>                         |
| <b>Average per Lane</b> | <b>1,769</b>                         |

In the southbound direction, south of Junction 8 (Kilmacanogue) peak hour traffic volumes reduce and there are currently no flow breakdown issues in the PM peak hour. Therefore the assessment of the practical capacity in the southbound direction at this location did not yield a practical capacity threshold. However, it is considered reasonable to assume that the southbound practical capacity here is similar to the combined northbound figure of 3,550 vehicles/hour.

#### *Estimation of Practical Capacity of the Various Links in the Study Area*

Using the observed data provided above, and our understanding of the existing geometry and operation of the M11/N11 corridor, an estimation of the practical capacity of the outstanding sections along the M11/N11 corridor is provide below and is summarised in Table B.3.

- 2 lane motorways (M50 and M11) – 4,600 (each direction) – based on M11 northbound data;

- 2 lane links (M11 Junction 3 to Junction 4) – 3,400 – based on GDA average in light of lower speed limit and geometry
- 2 lane + 1 auxiliary motorway - 6,300 (each direction), capacity of auxiliary lane assumed to be 1700 in line with GDA average;
- 2 lane dual carriageway:
  - 3,550 (northbound) between Junction 6 and Junction 8 – based on N11 northbound data.
  - 3,200 (southbound) between Junction 6 and Junction 8 based on reduction below 3,550 in light of the local conditions highlighted.
  - 3,550 (both directions) between Junction 8 and Junction 14 – based on N11 northbound data.

Table B.3: Practical Capacity

| Road | Junction No. | Junction Name                           | No. of Lanes | Practical Capacity (vehicles/lane/hour) |              |
|------|--------------|---|--------------|---|--------------|
|      |              |   |              | Northbound                              | Southbound   |
| M50  | 16 – 17      | Cherrywood – M11                        | 2            | 4,600                                   | 4,600        |
| M11  | 3 – 4        | Loughlinstown – M50                     | 2            | 3,400                                   | 3,400        |
|      | 4 – 5        | M50/M11 – Bray North                    | 2+1          | 6,300                                   | 6,300        |
|      | <b>5 – 6</b> | <b>Bray North – Bray Central</b>        | <b>2</b>     | <b>4,600</b>                            | <b>3,850</b> |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117        | 2            | 3,550                                   | 3,200        |
|      | 6a – 7       | Herbert Rd/R117 – Bray South            | 2            | 3,550                                   | 3,200        |
|      | 7 – 8        | Bray South - Kilmacanogue               | 2            | 3,550                                   | 3,200        |
|      | <b>8 – 9</b> | <b>Kilmacanogue – Glen of the Downs</b> | <b>2</b>     | <b>3,550</b>                            | <b>3,550</b> |
|      | 9 – 10       | Glen of the Downs - Delgany             | 2            | 3,550                                   | 3,550        |
|      | 10 – 11      | Delgany – Greystones (Kilpedder)        | 2            | 3,550                                   | 3,550        |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown          | 2            | 3,550                                   | 3,550        |
|      | 12 – 13      | Newtown MK - Newcastle                  | 2            | 3,550                                   | 3,550        |
|      | 13 – 14      | Newcastle – Coyne's Cross               | 2            | 3,550                                   | 3,550        |
| M11  | 14 – 15      | Coyne's Cross - Ashford                 | 2            | 4,600                                   | 4,600        |

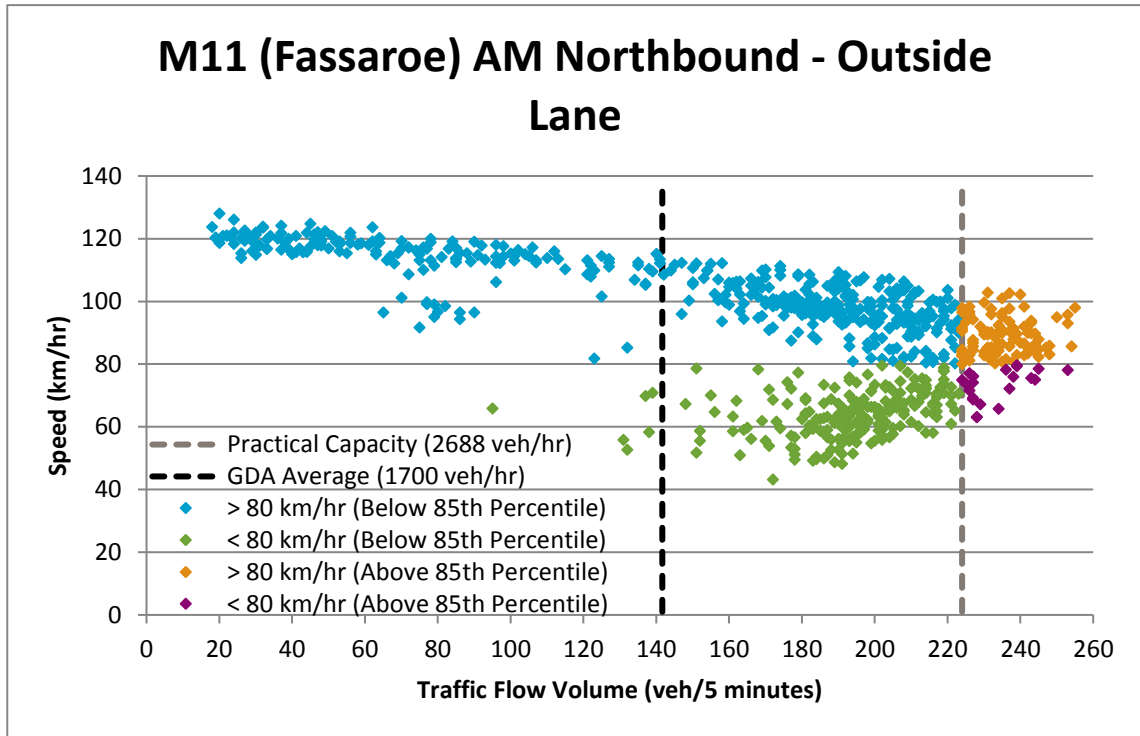


Figure B.1: M11 North of Fassaroe (AM Northbound – Outside Lane)

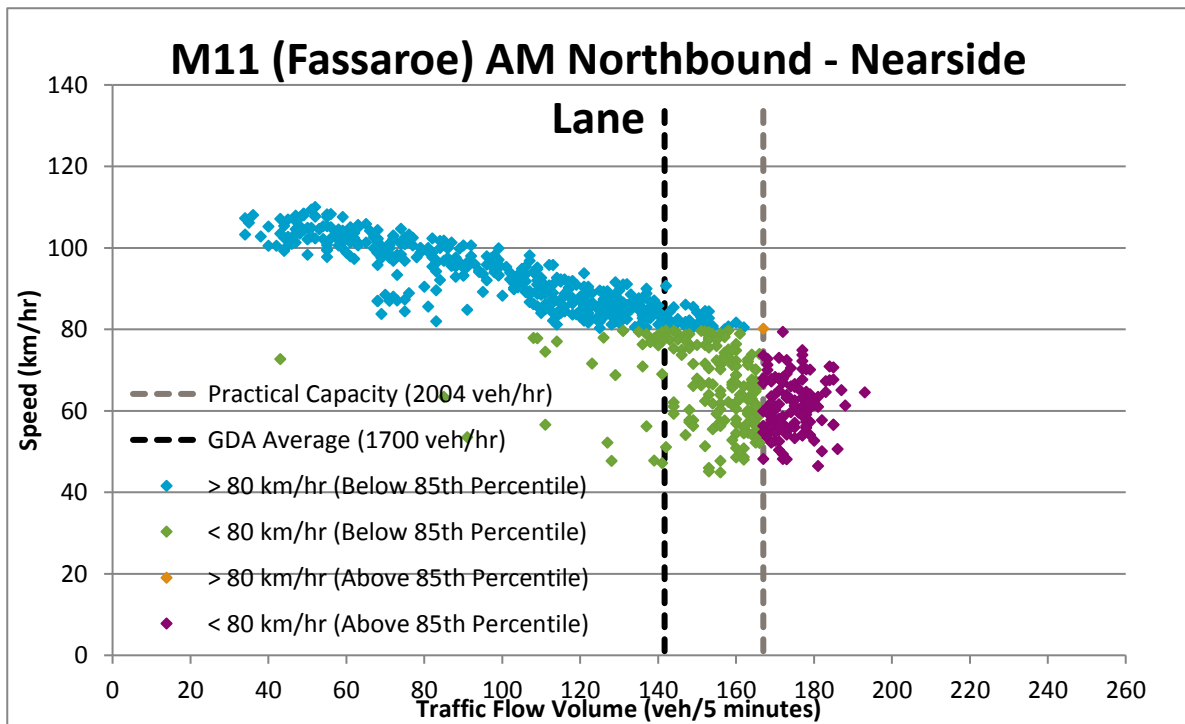


Figure B.2: M11 North of Fassaroe (AM Northbound – Nearside Lane)

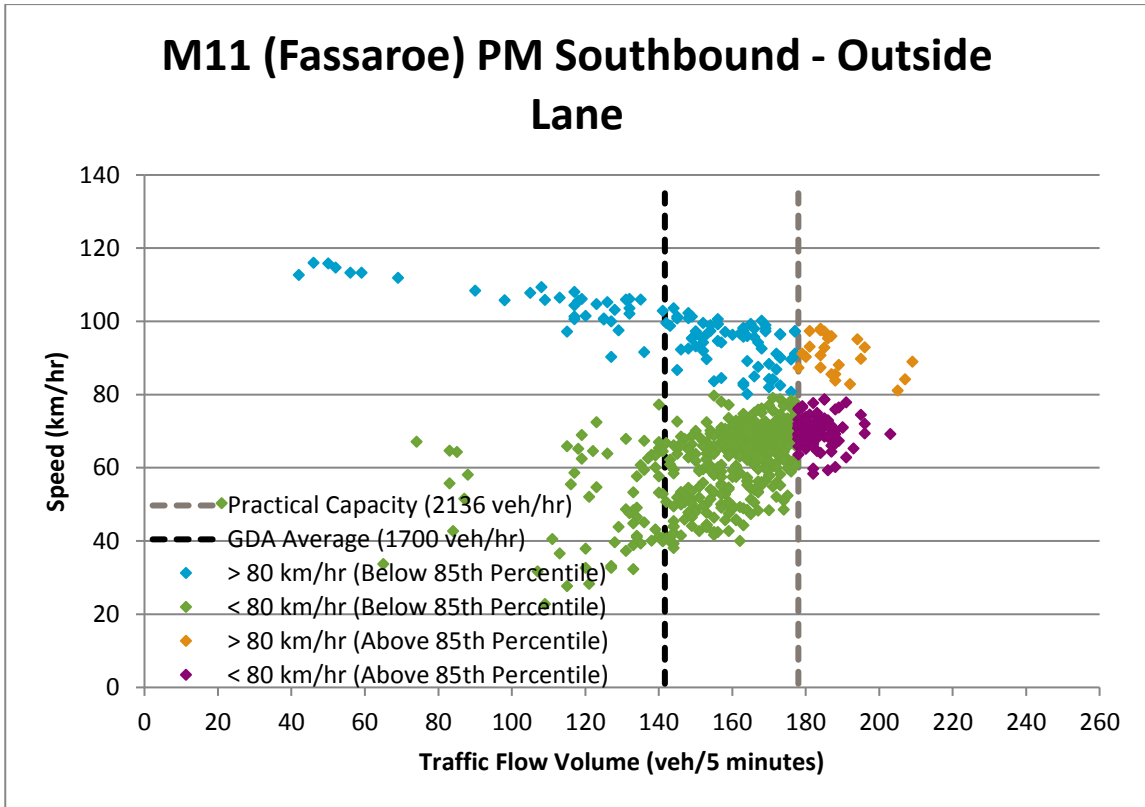


Figure B.3: M11 North of Fassaroe (PM Southbound – Outside Lane)

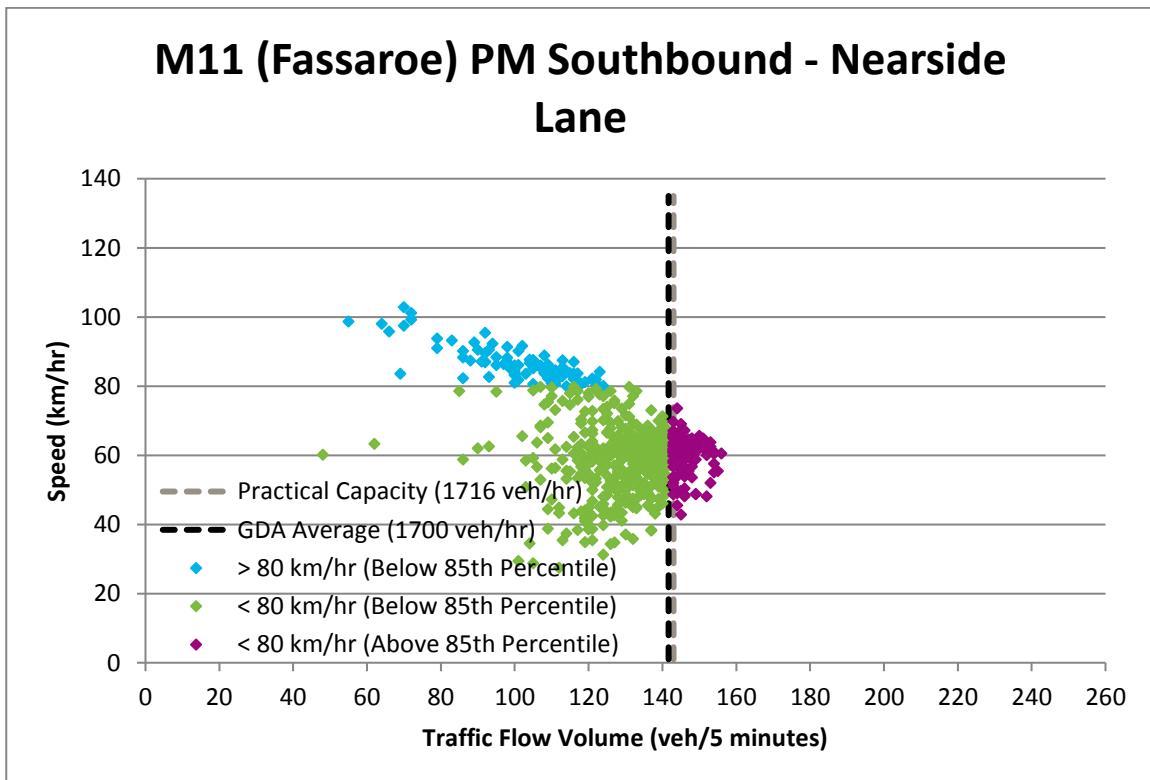


Figure B.4: M11 North of Fassaroe (PM Southbound – Nearside Lane)

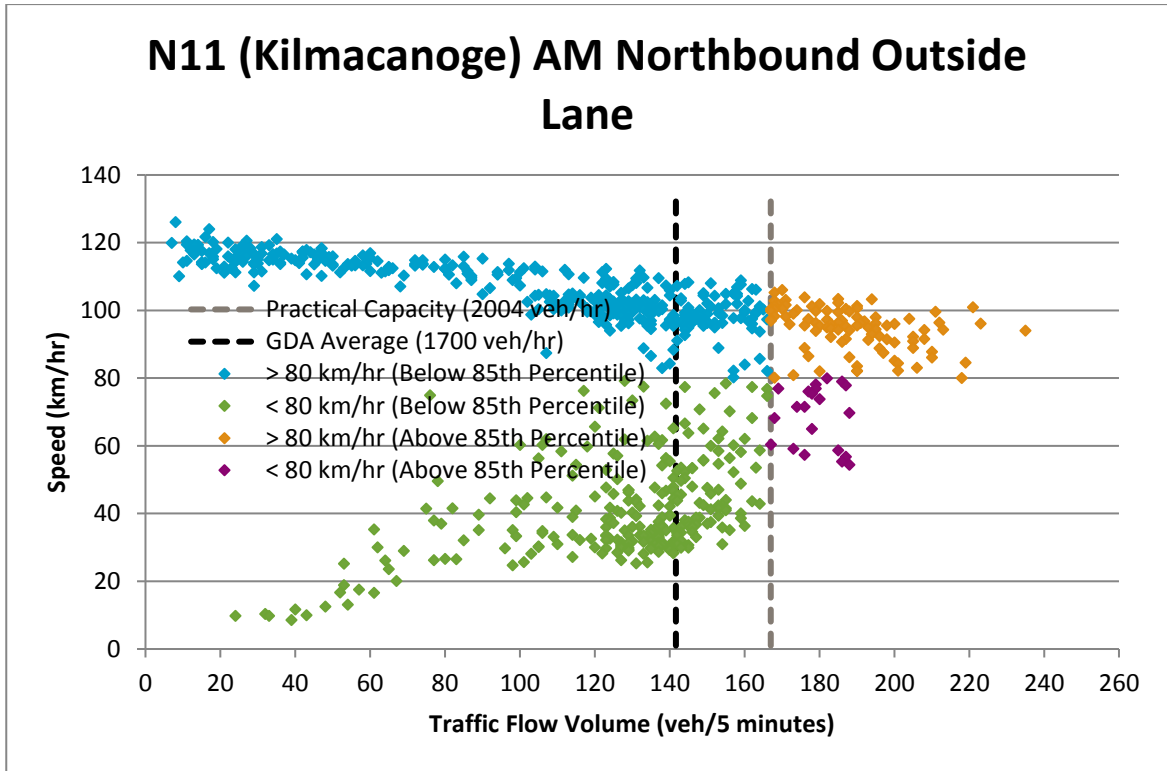


Figure B.5: N11 South of Kilmacanogue (AM Northbound – Outside Lane)

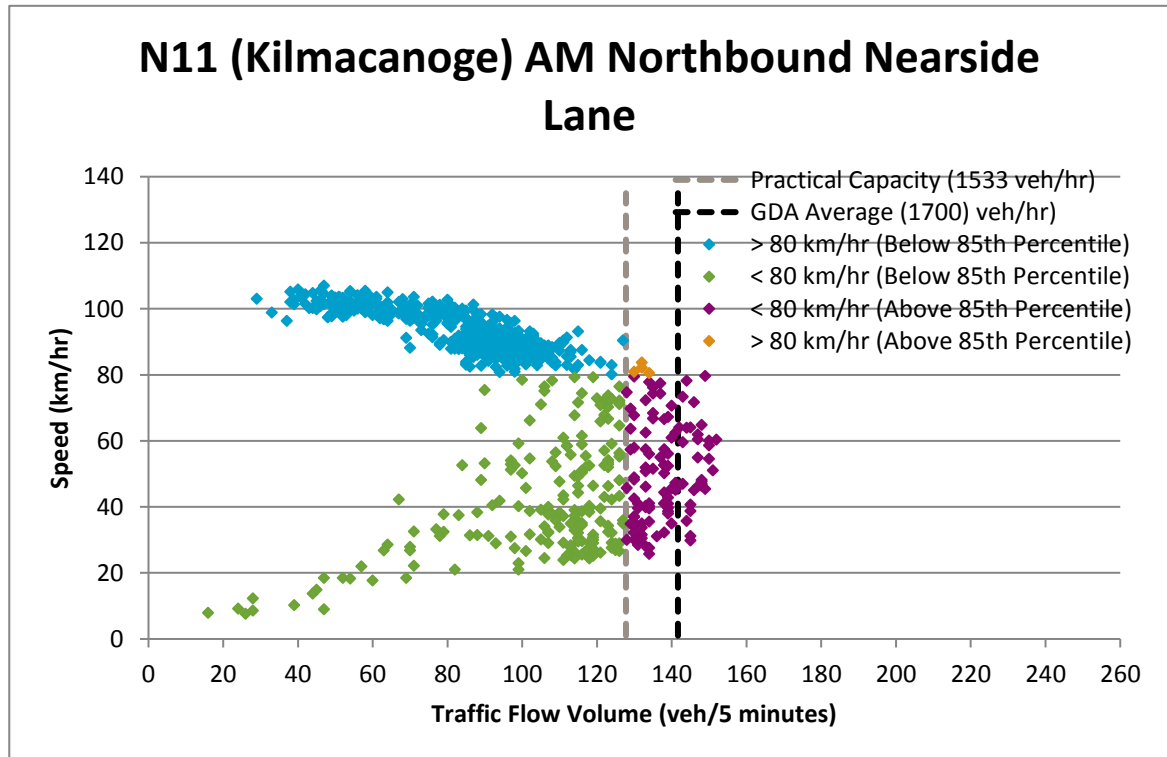


Figure B.6: N11 South of Kilmacanogue (AM Northbound – Nearside Lane)

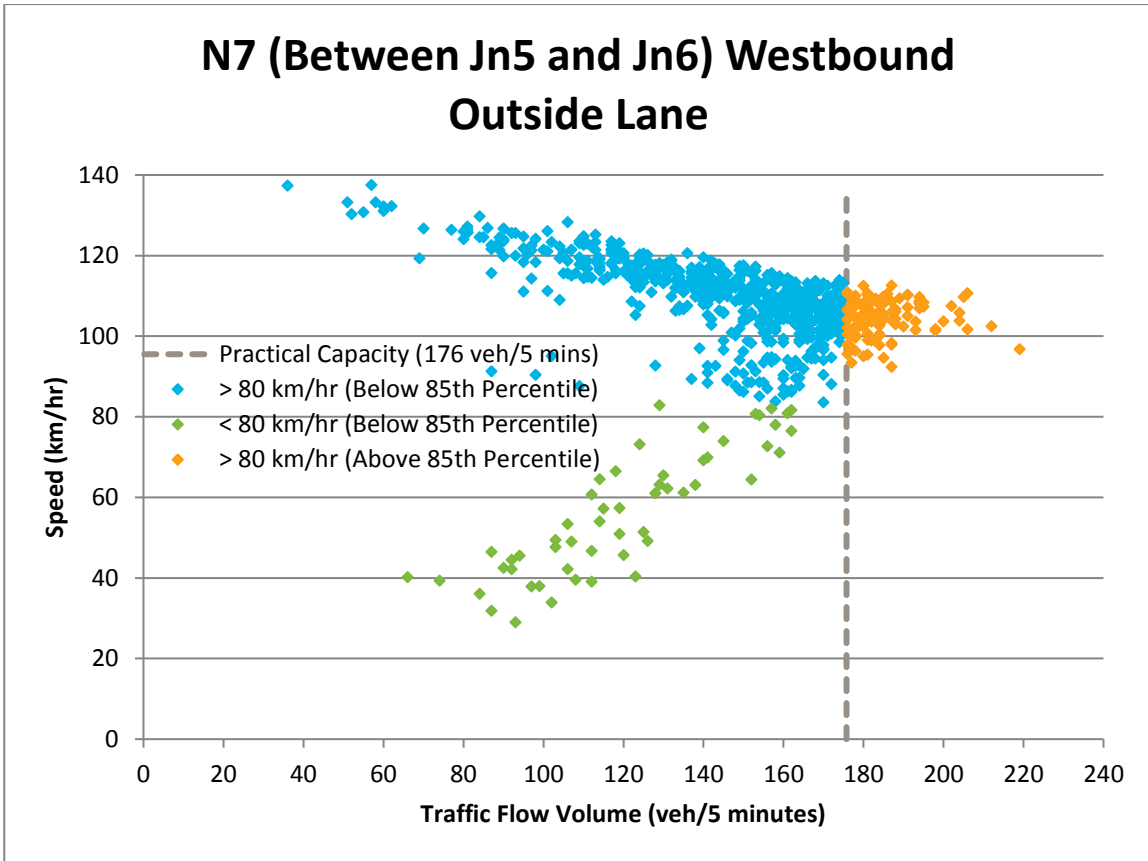


Figure B.7: N7 between Junctions 5 & 6 (PM Westbound – Nearside Lane)

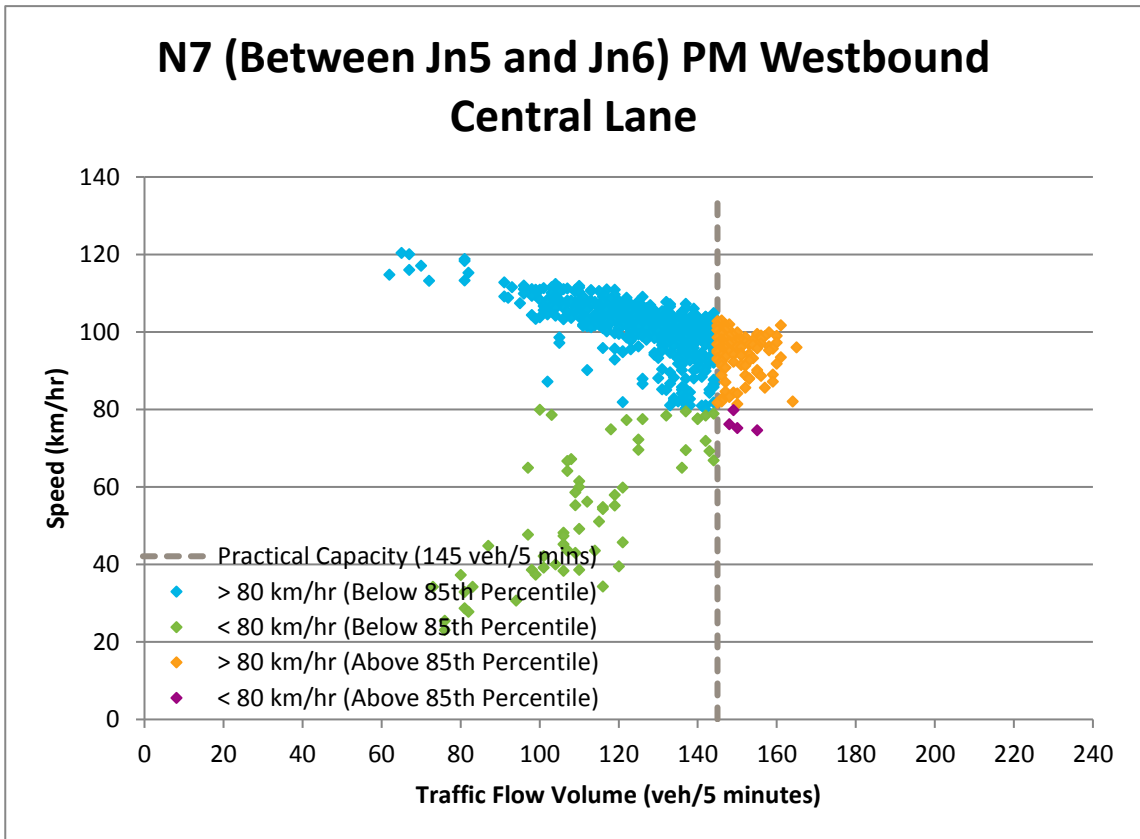


Figure B.8: N7 between Junctions 5 & 6 (PM Westbound – Centre Lane)



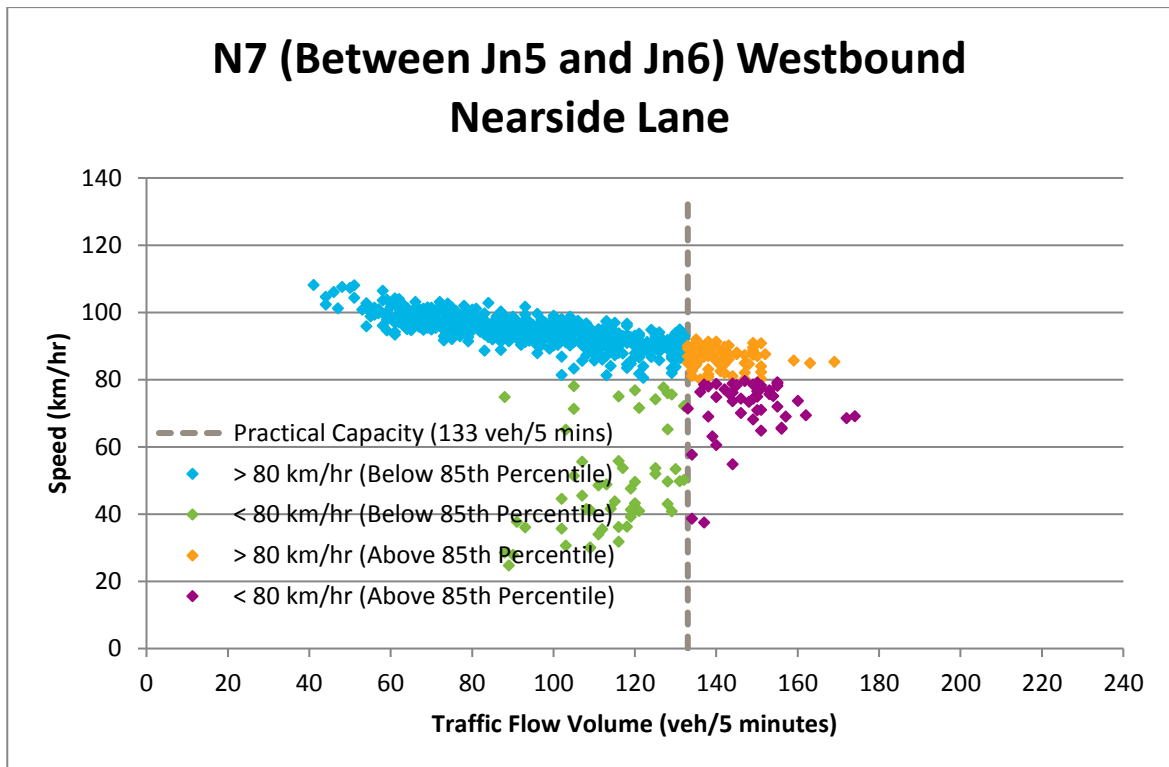


Figure B.9: N7 between Junctions 5 & 6 (PM Westbound – Nearside Lane)

# **Appendix C**

## **Modelled Flows**

Table C.1: 2015 M11/N11 Northbound Peak Hour Flows (Source: 2015 M11/N11 Local Area Model)

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00)<br>(vehicles/hour) |                                  | PM Peak (17:00 – 18:00)<br>(vehicles/hour) |                                  |
|------|--------------|----------------------------------|--------------|--|----------------------------------|--|----------------------------------|
|      |              |                                  |              | Demand Flow                                | Practical Link Specific Capacity | Demand Flow                                | Practical Link Specific Capacity |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 2,811                                      | 4,600                            | 1,551                                      | 4,600                            |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 1,829                                      | 3,400                            | 890  | 3,400                            |
|      | 4 – 5        | M50/M11 – Bray North             | 2+1          | 4,640                                      | 6,300                            | 2,441                                      | 6,300                            |
|      | 5 – 6        | Bray North – Bray Central        | 2            | 3,902                                      | 4,600                            | 2,023                                      | 4,600                            |
| N11  | 6 – 6a       | Bray Central – Herbert           | 2            | 3,985                                      | 3,550                            | 2,210                                      | 3,550                            |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 2            | 3,979                                      | 3,550                            | 2,060                                      | 3,550                            |
|      | 7 – 8        | Bray South - Kilmacanogue        | 2            | 2,905                                      | 3,550                            | 1,543                                      | 3,550                            |
|      | 8 – 9        | Kilmacanogue – Glen of the       | 2            | 2,425                                      | 3,550                            | 1,348                                      | 3,550                            |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 2,392                                      | 3,550                            | 1,307                                      | 3,550                            |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 2,092                                      | 3,550                            | 1,126                                      | 3,550                            |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 2,013                                      | 3,550                            | 1,253                                      | 3,550                            |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 1,613                                      | 3,550                            | 1,012                                      | 3,550                            |
|      | 13 – 14      | Newcastle – Coyne's Cross        | 2            | 1,710                                      | 3,550                            | 1,031                                      | 3,550                            |
| M11  | 14 – 15      | Coyne's Cross - Ashford          | 2            | 1,698                                      | 4,600                            | 1,024                                      | 4,600                            |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

Table C.2: 2015 M11/N11 Southbound Peak Hour Flows (Source: 2015 M11/N11 Local Area Model)

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00)<br>(vehicles/hour) |                                  | PM Peak (17:00 – 18:00)<br>(vehicles/hour) |                                  |
|------|--------------|----------------------------------|--------------|--|----------------------------------|--|----------------------------------|
|      |              |                                  |              | Demand Flow                                | Practical Link Specific Capacity | Demand Flow                                | Practical Link Specific Capacity |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 1,364                                      | 4,600                            | 2,339                                      | 4,600                            |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 790  | 3,400                            | 1,362                                      | 3,400                            |
|      | 4 – 5        | M50/M11 – Bray North             | 2+1          | 2,153                                      | 6,300                            | 3,701                                      | 6,300                            |
|      | 5 – 6        | Bray North – Bray Central        | 2            | 1,657                                      | 3,850                            | 3,273                                      | 3,850                            |
| N11  | 6 – 6a       | Bray Central – Herbert           | 2            | 1,987                                      | 3,200                            | 3,497                                      | 3,200                            |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 2            | 1,904                                      | 3,200                            | 3,159                                      | 3,200                            |
|      | 7 – 8        | Bray South - Kilmacanogue        | 2            | 1,379                                      | 3,200                            | 2,855                                      | 3,200                            |
|      | 8 – 9        | Kilmacanogue – Glen of the       | 2            | 1,210                                      | 3,550                            | 2,496                                      | 3,550                            |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 1,173                                      | 3,550                            | 2,464                                      | 3,550                            |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 1,041                                      | 3,550                            | 2,294                                      | 3,550                            |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 1,110                                      | 3,550                            | 2,118                                      | 3,550                            |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 903  | 3,550                            | 1,703                                      | 3,550                            |
|      | 13 – 14      | Newcastle – Coyne's Cross        | 2            | 932  | 3,550                            | 1,831                                      | 3,550                            |
| M11  | 14 – 15      | Coyne's Cross - Ashford          | 2            | 972  | 4,600                            | 1,920                                      | 4,600                            |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

Table C.3: 2030 Do-Minimum M11/N11 Northbound Peak Hour Flows (Source: 2030 Do-Minimum M11/N11 LAM)

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00)<br>(vehicles/hour) |                                  | PM Peak (17:00 – 18:00)<br>(vehicles/hour) |                                  |
|------|--------------|----------------------------------|--------------|--|----------------------------------|--|----------------------------------|
|      |              |                                  |              | Demand Flow                                | Practical Link Specific Capacity | Demand Flow                                | Practical Link Specific Capacity |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 3,390                                      | 4,600                            | 2014                                       | 4,600                            |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 2,021                                      | 3,400                            | 992  | 3,400                            |
|      | 4 – 5        | M50/M11 – Bray North             | 2+1          | 5,411                                      | 6,300                            | 3006                                       | 6,300                            |
|      | 5 – 6        | Bray North – Bray Central        | 2            | 4,714                                      | 4,600                            | 2444                                       | 4,600                            |
| N11  | 6 – 6a       | Bray Central – Herbert           | 2            | 4,855                                      | 3,550                            | 2546                                       | 3,550                            |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 2            | 4,866                                      | 3,550                            | 2314                                       | 3,550                            |
|      | 7 – 8        | Bray South - Kilmacanogue        | 2            | 3,978                                      | 3,550                            | 1875                                       | 3,550                            |
|      | 8 – 9        | Kilmacanogue – Glen of the       | 2            | 3,270                                      | 3,550                            | 1665                                       | 3,550                            |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 3,232                                      | 3,550                            | 1624                                       | 3,550                            |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 2,796                                      | 3,550                            | 1436                                       | 3,550                            |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 2,653                                      | 3,550                            | 1633                                       | 3,550                            |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 2,040                                      | 3,550                            | 1214                                       | 3,550                            |
|      | 13 – 14      | Newcastle – Coyne’s Cross        | 2            | 2,125                                      | 3,550                            | 1232                                       | 3,550                            |
| M11  | 14 – 15      | Coyne’s Cross - Ashford          | 2            | 2,227                                      | 4,600                            | 1234                                       | 4,600                            |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

Table C.4: 2030 Do-Minimum M11/N11 Southbound Peak Hour Flows (Source: 2030 Do-Minimum M11/N11 LAM)

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00)<br>(vehicles/hour) |                                  | PM Peak (17:00 – 18:00)<br>(vehicles/hour) |                                  |
|------|--------------|----------------------------------|--------------|--|----------------------------------|--|----------------------------------|
|      |              |                                  |              | Demand Flow                                | Practical Link Specific Capacity | Demand Flow                                | Practical Link Specific Capacity |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 1,813                                      | 4,600                            | 2,968                                      | 4,600                            |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 890  | 3,400                            | 1,617                                      | 3,400                            |
|      | 4 – 5        | M50/M11 – Bray North             | 2+1          | 2,704                                      | 6,300                            | 4,584                                      | 6,300                            |
|      | 5 – 6        | Bray North – Bray Central        | 2            | 2,150                                      | 3,850                            | 4,085                                      | 3,850                            |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117 | 2            | 2,337                                      | 3,200                            | 4,143                                      | 3,200                            |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 2            | 2,269                                      | 3,200                            | 4,054                                      | 3,200                            |
|      | 7 – 8        | Bray South - Kilmacanogue        | 2            | 1,850                                      | 3,200                            | 3,564                                      | 3,200                            |
|      | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 1,546                                      | 3,550                            | 3,103                                      | 3,550                            |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 1,510                                      | 3,550                            | 3,068                                      | 3,550                            |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 1,323                                      | 3,550                            | 2,888                                      | 3,550                            |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 1,402                                      | 3,550                            | 2,679                                      | 3,550                            |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 1,078                                      | 3,550                            | 2,160                                      | 3,550                            |
|      | 13 – 14      | Newcastle – Coyne’s Cross        | 2            | 1,095                                      | 3,550                            | 2,366                                      | 3,550                            |
| M11  | 14 – 15      | Coyne’s Cross - Ashford          | 2            | 1,140                                      | 4,600                            | 2,465                                      | 4,600                            |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

Table C.5: 2050 Do-Minimum M11/N11 Northbound Peak Hour Flows (Source: 2050 Do-Minimum M11/N11 LAM)

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00)<br>(vehicles/hour) |                                  | PM Peak (17:00 – 18:00)<br>(vehicles/hour) |                                  |
|------|--------------|----------------------------------|--------------|--|----------------------------------|--|----------------------------------|
|      |              |                                  |              | Demand Flow                                | Practical Link Specific Capacity | Demand Flow                                | Practical Link Specific Capacity |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 3,678                                      | 4,600                            | 2,206                                      | 4,600                            |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 2,168                                      | 3,400                            | 1,080                                      | 3,400                            |
|      | 4 – 5        | M50/M11 – Bray North             | 2+1          | 5,846                                      | 6,300                            | 3,286                                      | 6,300                            |
|      | 5 – 6        | Bray North – Bray Central        | 2            | 5,013                                      | 4,600                            | 2,627                                      | 4,600                            |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117 | 2            | 5,038                                      | 3,550                            | 2,671                                      | 3,550                            |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 2            | 5,077                                      | 3,550                            | 2,331                                      | 3,550                            |
|      | 7 – 8        | Bray South - Kilmacanogue        | 2            | 3,959                                      | 3,550                            | 1,773                                      | 3,550                            |
|      | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 3,326                                      | 3,550                            | 1,539                                      | 3,550                            |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 3,273                                      | 3,550                            | 1,497                                      | 3,550                            |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 2,915                                      | 3,550                            | 1,269                                      | 3,550                            |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 2,785                                      | 3,550                            | 1,417                                      | 3,550                            |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 2,084                                      | 3,550                            | 879  | 3,550                            |
|      | 13 – 14      | Newcastle – Coyne's Cross        | 2            | 2,209                                      | 3,550                            | 866  | 3,550                            |
| M11  | 14 – 15      | Coyne's Cross - Ashford          | 2            | 2,319                                      | 4,600                            | 862  | 4,600                            |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

Table C.6: 2050 Do-Minimum M11/N11 Southbound Peak Hour Flows (Source: 2050 Do-Minimum M11/N11 LAM)

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00)<br>(vehicles/hour) |                                  | PM Peak (17:00 – 18:00)<br>(vehicles/hour) |                                  |
|------|--------------|----------------------------------|--------------|--|----------------------------------|--|----------------------------------|
|      |              |                                  |              | Demand Flow                                | Practical Link Specific Capacity | Demand Flow                                | Practical Link Specific Capacity |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 2,197                                      | 4,600                            | 3,218                                      | 4,600                            |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 1,036                                      | 3,400                            | 1,693                                      | 3,400                            |
|      | 4 – 5        | M50/M11 – Bray North             | 2+1          | 3,233                                      | 6,300                            | 4,910                                      | 6,300                            |
|      | 5 – 6        | Bray North – Bray Central        | 2            | 2,424                                      | 3,850                            | 4,300                                      | 3,850                            |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117 | 2            | 2,510                                      | 3,200                            | 4,468                                      | 3,200                            |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 2            | 2,316                                      | 3,200                            | 4,379                                      | 3,200                            |
|      | 7 – 8        | Bray South - Kilmacanogue        | 2            | 1,862                                      | 3,200                            | 3,811                                      | 3,200                            |
|      | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 1,702                                      | 3,550                            | 3,292                                      | 3,550                            |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 1,647                                      | 3,550                            | 3,255                                      | 3,550                            |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 1,523                                      | 3,550                            | 3,089                                      | 3,550                            |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 1,612                                      | 3,550                            | 2,845                                      | 3,550                            |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 1,229                                      | 3,550                            | 2,261                                      | 3,550                            |
|      | 13 – 14      | Newcastle – Coyne's Cross        | 2            | 1,250                                      | 3,550                            | 2,488                                      | 3,550                            |
| M11  | 14 – 15      | Coyne's Cross - Ashford          | 2            | 1,301                                      | 4,600                            | 2,585                                      | 4,600                            |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

Table C.7: 2030 Do-Something Scenario 1 - M11/N11 Northbound Peak Hour Flows

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00) (vehicles/hour) |       | PM Peak (17:00 – 18:00) (vehicles/hour) |       | Do-Something Practical Capacity (vehicles/hour) |
|------|--------------|----------------------------------|--------------|---|-------|---|-------|---|
|      |              |                                  |              | Demand Flow                             |       | Demand Flow                             |       |   |
|      |              |                                  |              | DM                                      | DS 1  | DM                                      | DS 1  | Link Specific                                   |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 3,390                                   | 3,394 | 2,035                                   | 1,916 | 4,600   |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 2,021                                   | 2,017 | 1,012                                   | 936   | 3,400   |
|      | 4 – 5        | M50/M11 – Bray North             | 3+1          | 5,411                                   | 5,411 | 3,047                                   | 2,852 | 8,600   |
|      | 5 – 6        | Bray North – Bray Central        | 3            | 4,714                                   | 4,729 | 2,513                                   | 2,299 | 6,900   |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117 | 3            | 4,855                                   | 4,856 | 2,608                                   | 2,397 | 5,450   |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 3            | 4,866                                   | 4,867 | 2,380                                   | 2,147 | 5,450   |
|      | 7 – 8        | Bray South - Kilmacanogue        | 3            | 3,978                                   | 3,984 | 1,853                                   | 1,876 | 5,450   |
|      | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 3,270                                   | 3,274 | 1,636                                   | 1,666 | 3,550   |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 3,232                                   | 3,237 | 1,595                                   | 1,624 | 3,550   |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 2,796                                   | 2,797 | 1,411                                   | 1,436 | 3,550   |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 2,653                                   | 2,653 | 1,623                                   | 1,633 | 3,550   |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 2,040                                   | 2,040 | 1,205                                   | 1,214 | 3,550   |
| M11  | 14 – 15      | Coyne's Cross - Ashford          | 2            | 2,227                                   | 2,227 | 1,229                                   | 1,234 | 4,600   |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

Table C.8: 2030 Do-Something Scenario 1 - M11/N11 Southbound Peak Hour Flows

| Road | Junction No. | Junction Name                    | No. of Lanes | AM Peak (08:00 – 09:00) (vehicles/hour) |       | PM Peak (17:00 – 18:00) (vehicles/hour) |       | Do-Something Practical Capacity (vehicles/hour) |
|------|--------------|----------------------------------|--------------|---|-------|---|-------|---|
|      |              |                                  |              | Demand Flow                             |       | Demand Flow                             |       |   |
|      |              |                                  |              | DM                                      | DS 1  | DM                                      | DS 1  | Link Specific                                   |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 1,806                                   | 1,833 | 2,968                                   | 2,970 | 4,600   |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 903                                     | 870   | 1,617                                   | 1,617 | 3,400   |
|      | 4 – 5        | M50/M11 – Bray North             | 3+1          | 2,709                                   | 2,703 | 4,584                                   | 4,587 | 8,600   |
|      | 5 – 6        | Bray North – Bray Central        | 3            | 2,066                                   | 2,159 | 4,085                                   | 4,085 | 5,750   |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117 | 3            | 2,190                                   | 2,346 | 4,143                                   | 4,141 | 5,000   |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 3            | 2,081                                   | 2,277 | 4,054                                   | 4,057 | 5,000   |
|      | 7 – 8        | Bray South - Kilmacanogue        | 3            | 1,650                                   | 1,851 | 3,564                                   | 3,556 | 5,000   |
|      | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 1,479                                   | 1,546 | 3,103                                   | 3,094 | 3,550   |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 1,441                                   | 1,510 | 3,068                                   | 3,059 | 3,550   |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 1,331                                   | 1,322 | 2,888                                   | 2,888 | 3,550   |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 1,425                                   | 1,402 | 2,679                                   | 2,679 | 3,550   |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 1,086                                   | 1,078 | 2,160                                   | 2,159 | 3,550   |
| M11  | 14 – 15      | Coyne's Cross - Ashford          | 2            | 1,157                                   | 1,140 | 2,465                                   | 2,464 | 4,600   |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

# **Appendix D**

## **Option Assessment**

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|                     |  |                |                 |
|---------------------|--|----------------|-----------------|
| <b>Project:</b>     | TII TP4 Transport Modelling (M11/N11 Models)                                     | <b>Job No:</b> | 60266721 – 4.15 |
| <b>Subject:</b>     | M11/N11 Corridor Study – Need Assessment Report (Traffic Modelling & Assessment) |                |                 |
| <b>Prepared by:</b> | C. De Courcy/Liam O'Brien  | <b>Date:</b>   | 31.03.2017      |
| <b>Checked by:</b>  | Philip Shiels  | <b>Date:</b>   | 31.03.2017      |
| <b>Approved by:</b> | Colin Acton  | <b>Date:</b>   | 31.03.2017      |

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## 1.0 Introduction

This Technical Note forms an Appendix to the Needs Assessment Report developed as part of the M11/N11 Corridor Study by AECOM-Roughan & O'Donovan on behalf of Transport Infrastructure Ireland (TII). The M11/N11 Corridor Study considers the section of the M11/N11 between Junction 4 (M50/M11) and Junction 14 (Coyne's Cross) only. The objectives of the M11/N11 Corridor Study are to:

1. Identify the improvements required to:
  - Bring the section of the corridor (M11/N11 mainline and junctions) up to the appropriate standard;
  - Develop the regional and local road network to support local access and complement the corridor strategy, including the closure of all direct accesses; and
  - Ensure the safe daily operation of the M11/N11 mainline and junctions in the event of the occurrence of incidents.
2. Identify a phased implementation of the improvements such that operational benefits on the corridor can be realised at an early stage without compromising the long term strategy.

This Technical Note relates only to the improvements required and outlines the various measures which were considered in relation to increasing the capacity of the M11/N11 corridor and regional/local road network in order to meet the future needs. The phased implementation of the recommended measures is dealt with in the main body of the report.

## 2.0 Objective of Technical Note

The objective of this Technical Note is to identify, test and assess a number of proposed measures to M11/N11 mainline, mainline junctions and regional/local road network which may improve the operation and increase the capacity of the M11/N11 corridor. The findings of this assessment are then used to inform the identification of an Emerging Preferred Strategy for the M11/N11 corridor.

## 3.0 Proposed Infrastructure Measures

This section describes the proposed infrastructure measures which were considered and assessed using the M11/N11 Local Area Models (LAM) <sup>1</sup> developed as part of the M11/N11 Corridor Study. The proposed measures are grouped into four sub-areas based on the objectives of the study:

- 1) M11/N11 mainline measures;
- 2) M11/N11 junction measures;
- 3) Regional/Local road network measures; and
- 4) Alternative route measures (i.e. network resilience).

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<sup>1</sup> For full detail of the M11/N11 Local Area Models refer to the Traffic Modelling Report.



### 3.1 M11/N11 Mainline Measures

The 2030 & 2050 Do-Minimum AM and PM Peak hour LAM's identified the need to consider an increase in the capacity of the M11/N11 corridor between Junction 4 (M50/M11) and Junction 8 (Kilmacanogue). Based on this need the Do-Something (DS) scenario presented in Table 3.1 was tested in the LAM's.

Table 3.1: Do-Something Scenario 1 (Mainline)

| Scenario Name | Description   |
|---------------|---|
| DS 1          | 3 lanes plus an auxiliary lane on the M11 between Junction 4 (M50/M11) and Junction 5 (Bray North) and 3 lanes in each direction on the M11/N11 between Junction 5 and Junction 8 (Kilmacanogue). |

It should be noted that while future year modelled flows indicate a need for 3 mainline lanes between Junctions 7 and 8, the merge and diverge flows are such that this is best achieved by the provision of lane gains and lane drops northbound and southbound at Junction 7 such that the third lane between Junctions 7 and 8 is a continuous auxiliary lane.

Considerations should be given at preliminary design stage to ensure that the possibility of maintaining three mainline lanes through Junction 7 is not precluded.

An assessment of the 2030 and 2050 flows on the M11/N11 corridor in DS 1 is provided in Annex A (Tables A1 and A2) for the AM Peak (northbound) and PM Peak (southbound) directions. The tables demonstrate that the increase in capacity of the M11/N11 corridor to Junction 8 (Kilmacanogue) can cater for the projected flows in both 2030 and 2050.

### 3.2 M11/N11 Mainline Junction Measures

Table 3.2 outlines the various M11/N11 mainline junction measures considered and tested using the M11/N11 LAMs. The geographic location of these measures is provided in Figure 3.15.

Table 3.2: Do-Something Scenarios (Junction Proposals)

| Junction                             | Scenario Name | Description  |
|--------------------------------------|---------------|--|
| J5 - Bray North (Wilford)            | DS J5a        | Increased capacity (Gyratory layout)   |
|                                      | DS J5b        | Increased capacity (Dumbbell layout)   |
| J6 - Bray Central (Fassaroe)         | DS J6         | Increased capacity (roundabouts and merges/diverges)   |
| J6a – Herbert Road / Enniskerry Road | DS J6a        | Closure of direct access between N11 and Herbert Road/Enniskerry Road. This proposal forms part of Do—Something L7. Refer to Do-Something L7 in Section 3.3.7 for full details |
| J7 - Bray South (Kilcronee)          | DS J7         | Increased capacity (Dumbbell layout), with potential southbound lane drop and lane gain south of J7, and northbound lane drop and lane gain north of J7.                       |

| Junction          | Scenario Name | Description   |
|-------------------|---------------|---|
| J8 – Kilmacanogue | DS J8         | Introduction of single southbound lane drop/service road and single northbound lane gain/service road with associated increase in speed limit of 100km/hr |

3.2.1 Do-Something J5a (Junction 5 – Bray North)

Do-Something Junction 5a (DS J5a) which is illustrated in Figure 3.1 is one of two upgrade options considered for Junction 5. This gyratory design was proposed by Atkins in the ‘Assessment of the N11 Corridor’ report (2013) for Bray Town Council.

The proposal includes for the provision of a new northbound off-ramp, northbound on-ramp, gyratory roundabout and a new link road which provides a connection to Ferndale Road. The existing northbound off ramp, which currently provides a connection to Old Connaught Avenue, is closed as part of this proposal.

The link road between the upgraded junction and Ferndale road will now replace the connection previously provided by the northbound off-ramp (this link road will also provide future network resilience in the case of incidents on the M11 mainline or its closure).

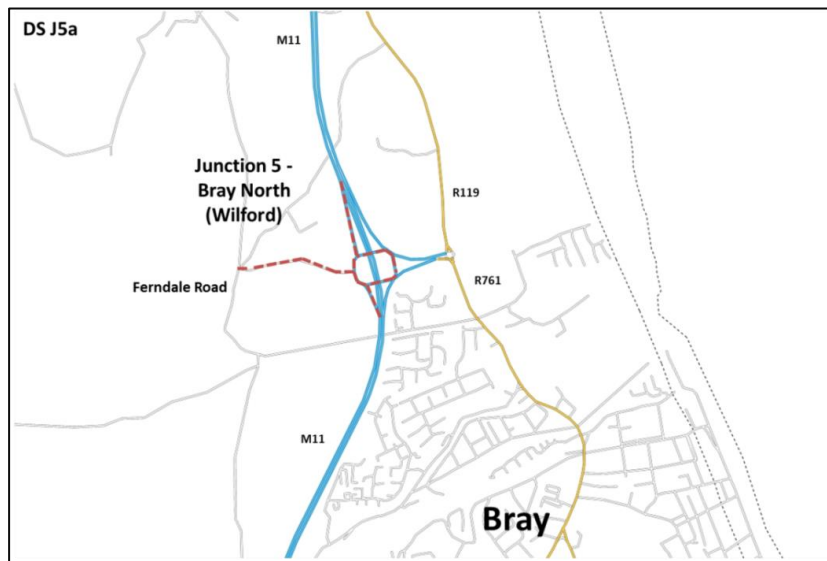


Figure 3.1: Do-Something Scenario J5a

3.2.2 Do-Something J5b (Junction 5 – Bray North)

Do-Something Junction 5b (DS J5b) which is illustrated in Figure 3.2 is the second of the two upgrade options considered for Junction 5. This option allows for a dumbbell arrangement which includes the removal of the existing northbound off-ramp to Old Connaught Avenue, and the provision of a new roundabout on the west side of the junction which will connect the new northbound off-ramp and on-ramp, a new link road to Ferndale Road (seen previously in DS J5a) and a new link to the existing roundabout on the east side of the junction.

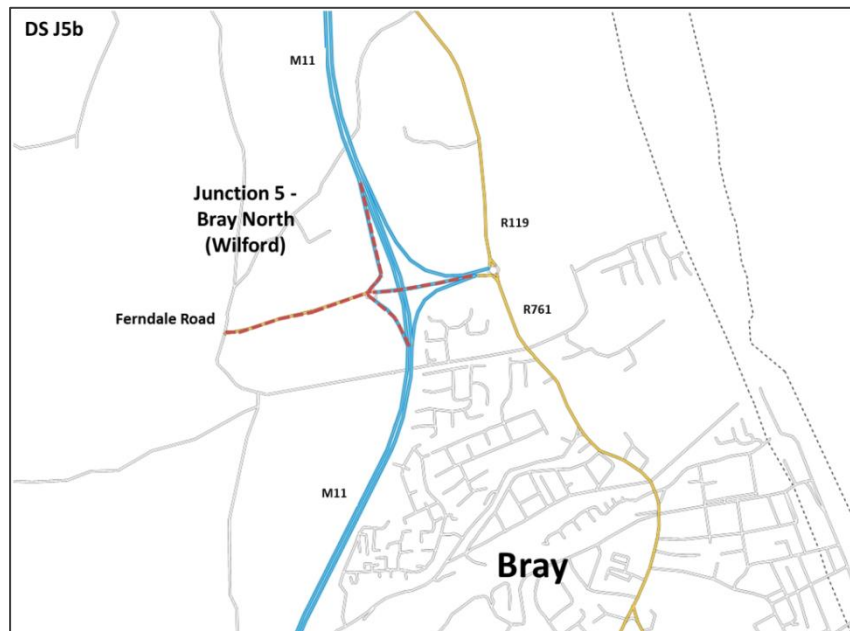


Figure 3.2: Do-Something Scenario J5b

3.2.3 Do-Something J6 (Junction 6 – Bray Central)

Do-Something Junction 6 (DS J6) which is illustrated in Figure 3.3, includes for an upgrade of the existing merges/diverges to the appropriate design standard and an increase in the capacity of the two existing roundabouts of Junction 6.

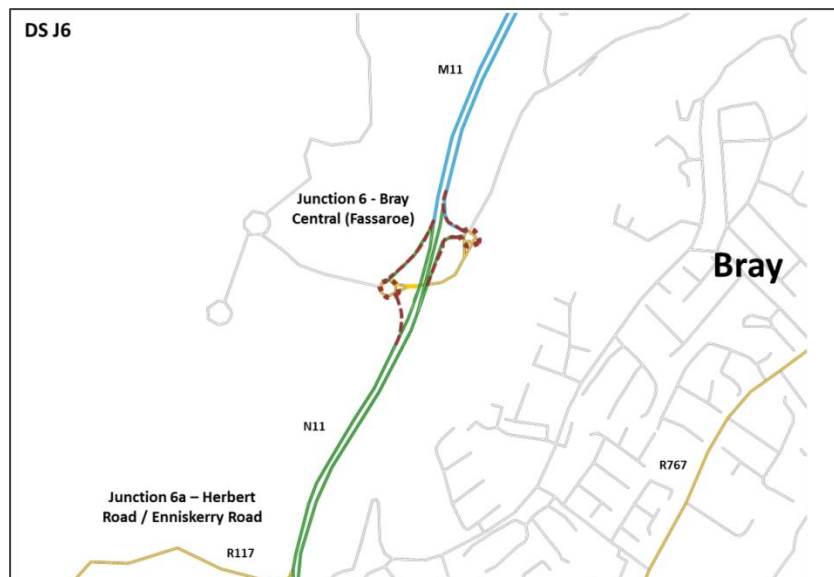


Figure 3.3: Do-Something Scenario J6

3.2.4 Do-Something J6a (Junction 6a Herbert Road/Enniskerry Road)

The existing left on / left off junctions at Herbert Road (southbound) and Enniskerry Road (northbound) are substandard and have a direct impact upon the capacity and operation of the N11 mainline. As the interventions proposed at Junction 6a mainly deals with regional and local roads and do not include a junction test, this proposal forms part of Do-Something L7. Full details of which are provided in Section 3.3.7.

3.2.5 Do-Something J7 (Junction 7 – Bray South)

Do-Something Junction 7 (DS J7) is illustrated in Figure 3.4. This option includes the provision of a new dumbbell arrangement with a longer off ramp and on ramp, and a new roundabout on the west side of the junction which is linked by a new bridge to the existing roundabout, and a new off-ramp and on-ramp for the northbound direction. This option includes the closure of the current northbound on and off-ramps. As part of this proposal, the existing bridge (R768) across the N11 is closed to vehicular traffic.

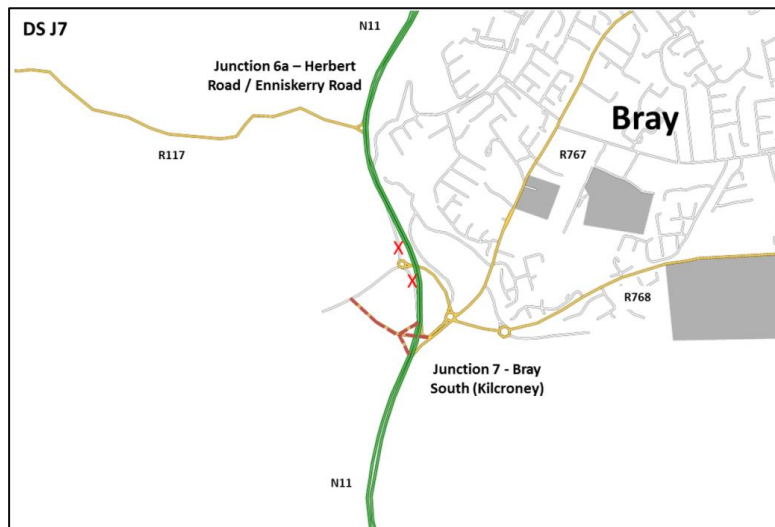


Figure 3.4: Do-Something Scenario J7

3.2.6 Do-Something J8 (Junction 8 – Kilmacanogue)

Do-Something Junction 8 (DS J8) is illustrated in Figure 3.5, this measure includes a new southbound diverge designed to appropriate standard which will incorporate a service road and all accesses. This option also includes a single northbound merge to appropriate standard to incorporate a service road, local junctions and all accesses. This proposal will facilitate the increase of speed limit to 100km/hr in both directions.

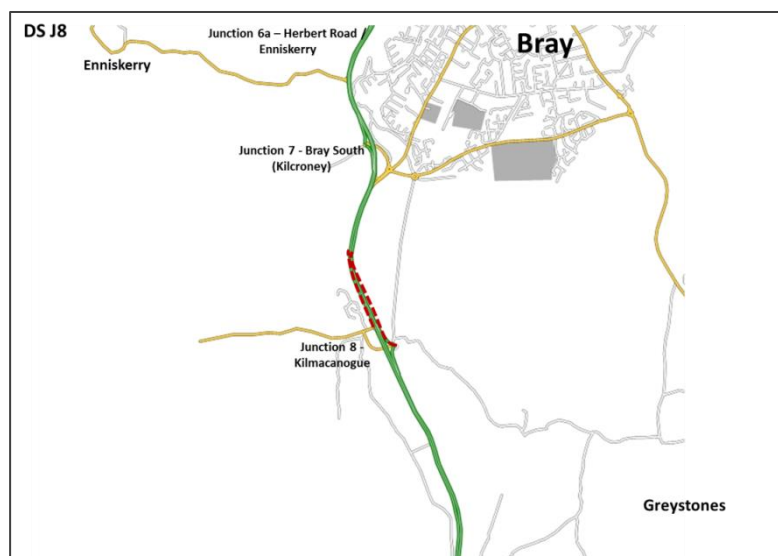


Figure 3.5: Do-Something Scenario J8

### 3.3 Regional/Local Road Measures

The following sections discuss a number of proposals to improve access between the M11/N11 mainline corridor and the regional/local road network. Many of these proposals were originally identified in the M50/M11/N11 Corridor Strategy<sup>2</sup>. Table 3.3 provides a summary of the measures considered. The geographic location of these measures is provided in Figure 3.15.

Table 3.3: Do-Something Scenarios (Regional/local Road Options)

| Scenario Name | Description  |
|---------------|--|
| DS L1         | Link road between Herbert Road and Upper Dargle Road. Provides an additional crossing of the River Dargle allowing more direct access between Junction 6 (Bray Central) and the area of Bray south of the River Dargle |
| DS L2         | Bridge over the N11 (at Junction 6a) between Herbert Road and Enniskerry Road (R117)   |
| DS L3         | Link road between Junction 6 (Bray Central/Fassaroe) and Enniskerry  |
| DS L4         | Link road between Bray Southern Cross Road (R738) and Junction 8 (Kilmacanogue)  |
| DS L5         | North Greystones Link Road   |
| DS L6         | Closure of Herbert Road Access to N11 and resulting impact on nearby junctions   |
| DS L7         | Provide services roads between Junction 6a and Junctions 6 and 7. Remove direct access onto the N11 at Junction 6a   |
| DS L8         | Link road from Rathmichael/Ballycorus Road to M50 Junction 16 (Cherrywood)   |

#### 3.3.1 Do-Something L1 – Herbert/Dargle Road Link

Do-Something L1 (DS L1) which is illustrated indicatively in Figure 3.6 aims to improve access between the M11/N11 corridor and Bray by providing an additional crossing of the River Dargle in the vicinity of Junction 6. This proposal would reduce traffic on the N11 corridor between Junctions 6 and 7 as vehicles would be able to access the southern areas of Bray via Junction 6.

The provision of this additional crossing of the River Dargle would also have added advantages to traffic movement within Bray, as well as improving the connectivity between Bray and development proposals at Fassaroe.

<sup>2</sup> M50/M11/N11 Corridor Study Final Report, Transport Infrastructure Ireland, January 2012.

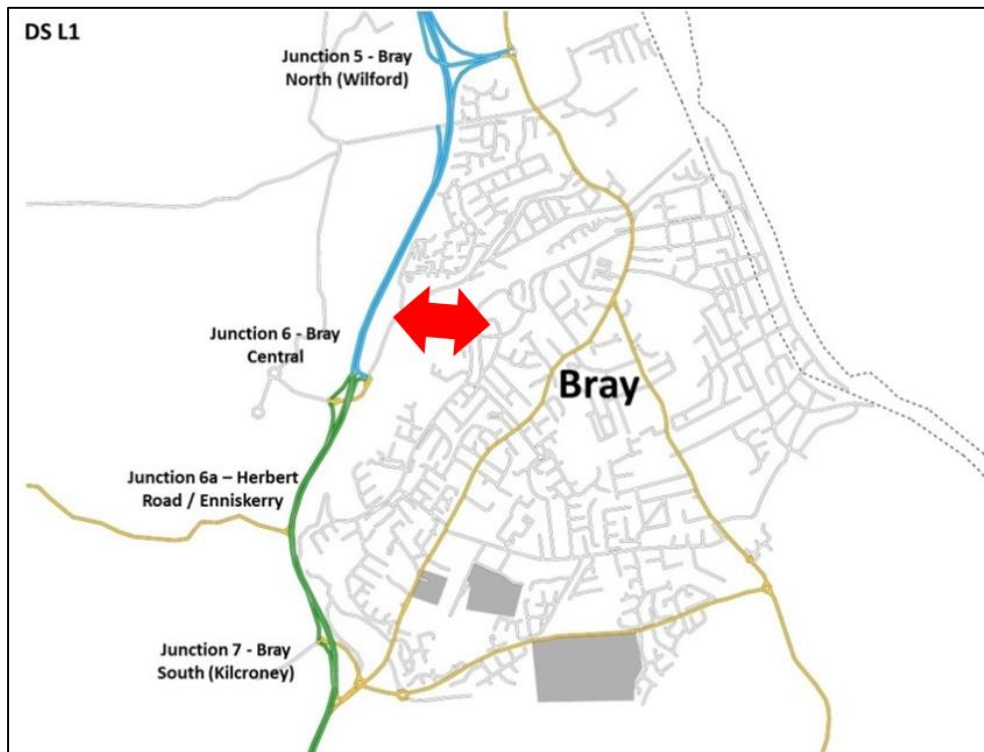


Figure 3.6: Do-Something L1

3.3.2 Do-Something L2 – Bridge Over N11 at Junction 6a

Do-Something L2 (DS L2) which is illustrated in Figure 3.7 provides for a crossing of the N11 at Junction 6a (Herbert Road/Enniskerry Road). The intention of this proposal is to provide direct east-west access between Bray and Enniskerry (the junction currently operates as a left in/left out only junction east and west of the N11). This proposal would remove the need for traffic to utilise Junctions 6 & 7 in order to make a U-turn to access the N11 or Bray/Enniskerry. Direct access to the N11 via Junction 6a is maintained as part of the proposal.



Figure 3.7: Do-Something L2

3.3.3 Do-Something L3 – Enniskerry Link Road

Do-Something L3 (DS L3) which is illustrated in Figure 3.8 aims to improve access between Enniskerry and the M11/N11 corridor/Bray by upgrading the existing local road (Berryfield Lane). Berryfield Lane currently provides a connection between Junction 6 and the R117 north of Enniskerry, however the route is of poor cross section and alignment at present. The intention of this proposal is to provide an alternative route between Enniskerry and the M11/N11 via Junction 6.

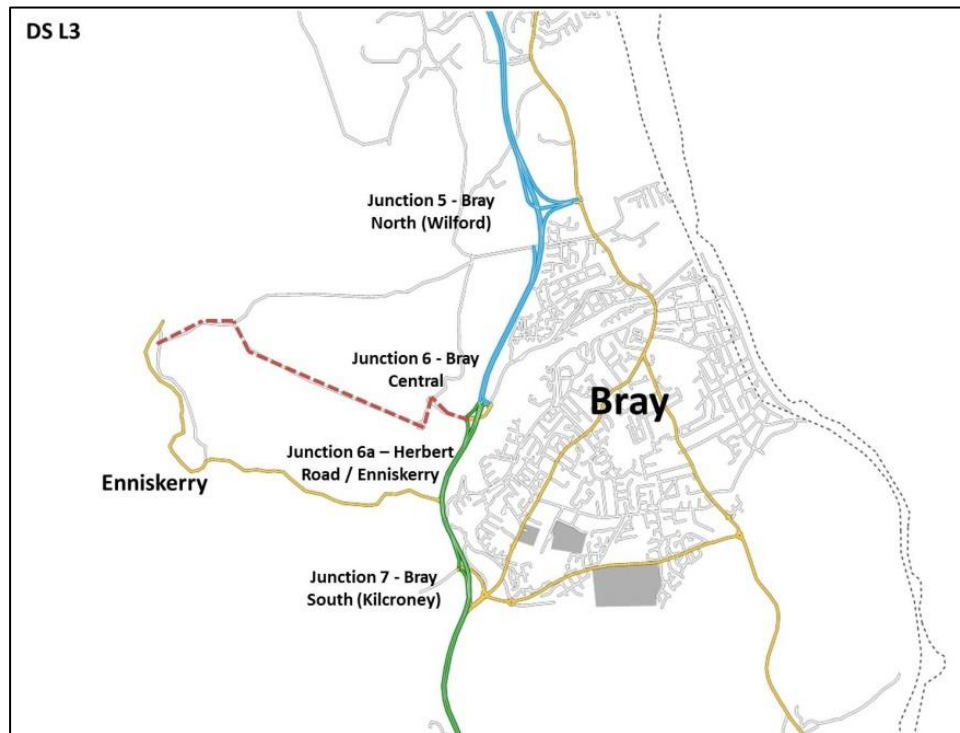


Figure 3.8: Do-Something L3

3.3.4 Do-Something L4 – Kilmacanogue to Bray Southern Cross Link Road

Do-Something L4 (DS L4) which is illustrated in Figure 3.9 provides for a connection between Junction 8 (Kilmacanogue) and Bray Southern Cross Road (R768). The intention of this proposal is to reduce the level of traffic through Junction 7 (Bray South/Kilcronee) and on the N11 between Junction 7 (Bray South/Kilcronee) and Junction 8 (Kilmacanogue). This proposal would also include the Do-Something J8 services road proposals at Junction 8 (Kilmacanogue) as discussed in Section 3.2.6.

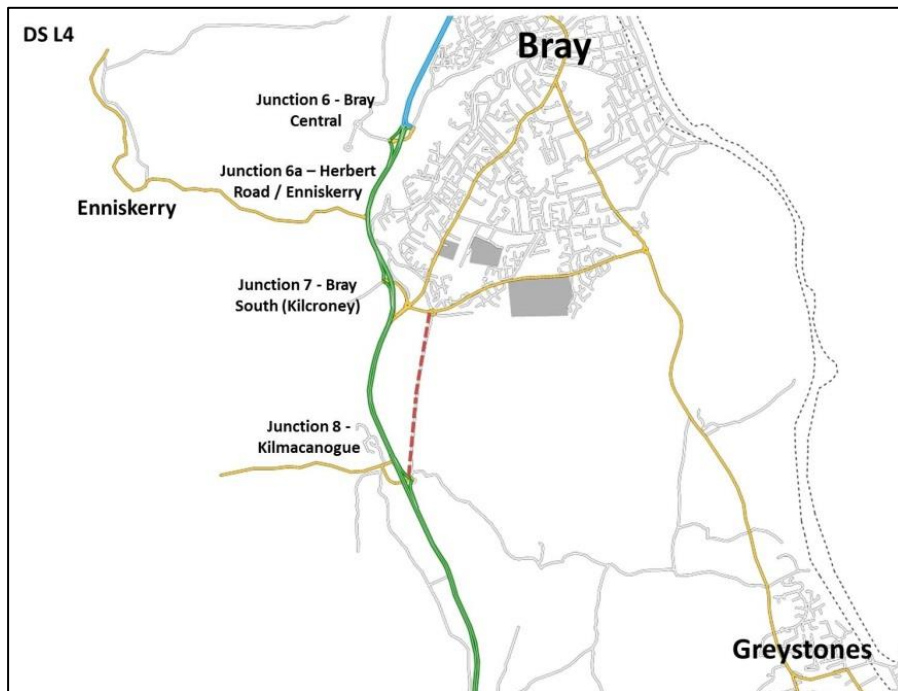


Figure 3.9: Do-Something L4

3.3.5 Do-Something L5 – North Greystones Link Road

Do-Something L5 (DS L5) which is illustrated in Figure 3.10 provides for a new link road from the R761 at Greystones to Ballydonagh Road (as identified in the 'Greystones-Delgany and Kilcoole Local Area Plan 2013-2019' improving access onwards to the N11 at Junction 9 (Glen of the Downs)).

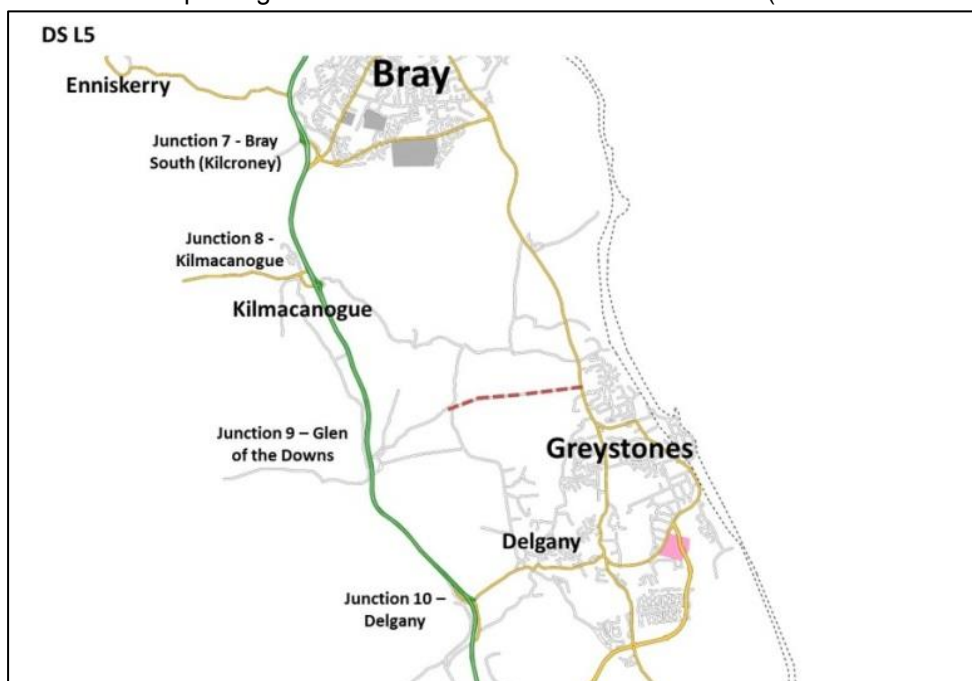


Figure 3.10: Do-Something L5



### 3.3.6 Do-Something L6 – Closure of Direct Access at Junction 6a between N11 and Herbert Road

Do-Something L6 (DS L6) which is illustrated in Figure 3.11 aims to close access to and from Junction 6a at Herbert Road on the N11 southbound carriageway. The diverge at this location is a tight radius bend and the intention of this proposal is to improve the operation of the southbound section of the N11 between Junctions 6 and 7.

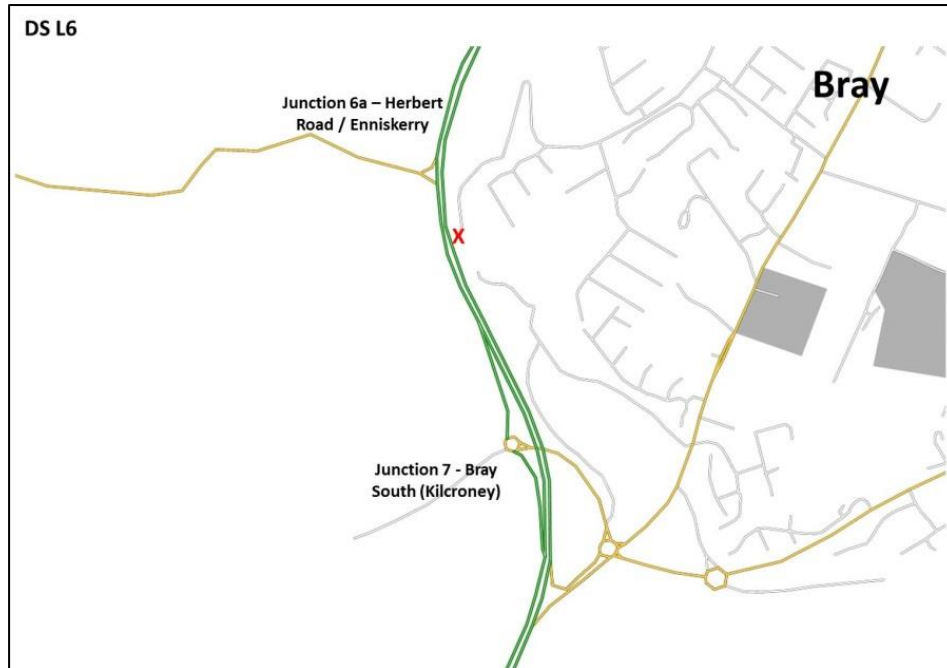


Figure 3.11: Do-Something L6

### 3.3.7 Do-Something L7 – Closure of Direct Access to N11 at Junction 6a plus Services Roads

Do-Something L7 (DS L7) which is illustrated in Figure 3.12 provides for new service roads adjacent to the N11 connecting Junction 6a to both Junction 6 and Junction 7. On the western side of the N11, Junction 6a (R117 - Enniskerry Road) will be connected to both Junction 6 and 7 via segregated one-way services road and direct access to the N11 will be closed. On the eastern side of the N11, a one-way segregated service road will commence north of Dargle Lane and connect Junction 6a (Herbert Road) to Junction 7. Direct access between the N11 and Junction 6a (Herbert Road) will be closed (as outlined in DS 6a).

The intention of this proposal is to effectively remove direct access onto the N11 at Junction 6a from both Herbert Road and the R117, to allow traffic to join the N11 at junctions of a higher standard that are in line with TEN-T requirements. This will also have the effect of raising the southbound mainline capacity by removing the weaving movements and slower moving vehicles at this location.

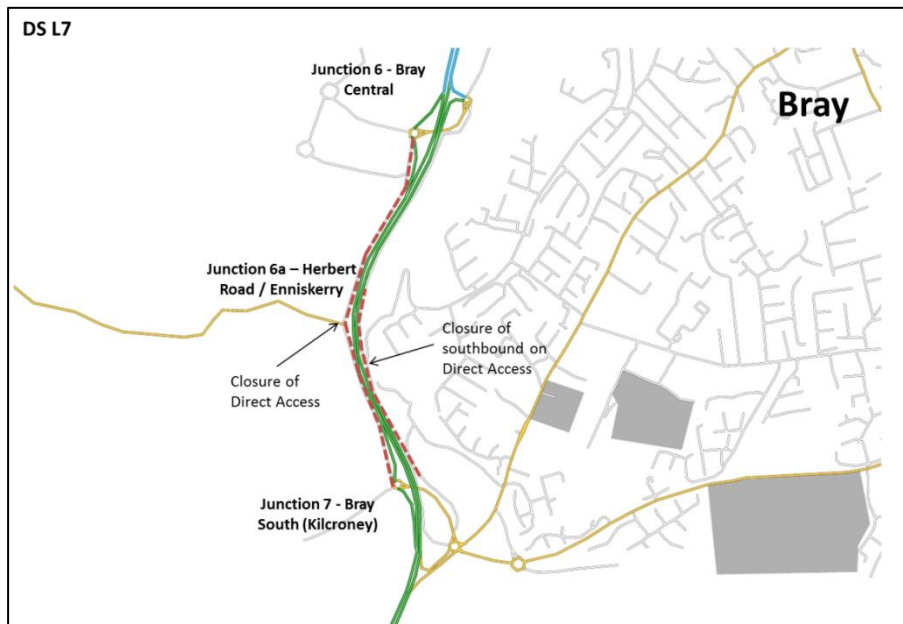


Figure 3.12: Do-Something L7

3.3.8 Do-Something L8 – M50 Cherrywood Junction to Ballycorus Road Link

Do-Something L8 (DS L8) which is illustrated in Figure 3.13 provides for a link road from Rathmichael/Ballycorus Road to M50 Junction 16 (Cherrywood). This proposal provides an alternative route for users travelling from the Shankill area to the M50 by allowing them a more direct route thereby potentially avoiding travelling to this destination via Junction 5 (Bray North/Wilford). It also provides for network resilience in the case of incidents on the M50 or M11.

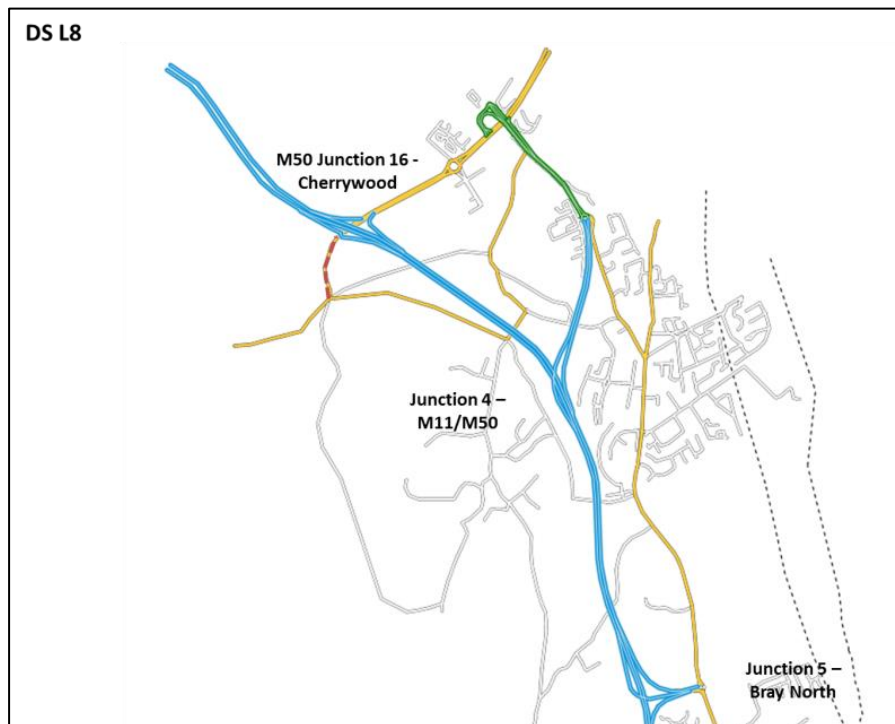


Figure 3.13: Do-Something L8

### 3.4 Alternative Routes for Incident Management

One of the objectives of the needs assessment is to ensure the safe daily operation of the M11/N11 mainline and junctions in the event of the occurrence of incidents. The unexpected closure of a section of the National Road network particularly one which carries a high volume of traffic can lead to significant delays and wider network impacts. In the event of an unexpected closure an alternative route which provides a safe route to the next junction should be available.

The proposals outlined in Table 3.4, if delivered, would provide an alternative route for traffic if an incident on the M11/M11 required the road to be closed.

*Table 3.4: Do-Something Scenarios (Alternative Routes)*

| Scenario | Description  |
|----------|--|
| AR1      | Improved local roads to the west of M11 between J4 and J6 (Ferndale Road, part of Thornhill Road plus a new link from Thornhill Road to Fassaroe as per Fassaroe masterplan) |
|          | New link from M50 J16 (Cherrywood) to Rathmichael/Ballycorus Road - (DS L8)  |
|          | New local road between Junction 7 & 8 on the east side (Kilmacanogue Link Road) – (DS L4)  |

### 3.5 Location of the Do-Something Scenarios

Figure 3.14 depicts the location of each of the proposed measures in the M11/N11 Needs Assessment study area.

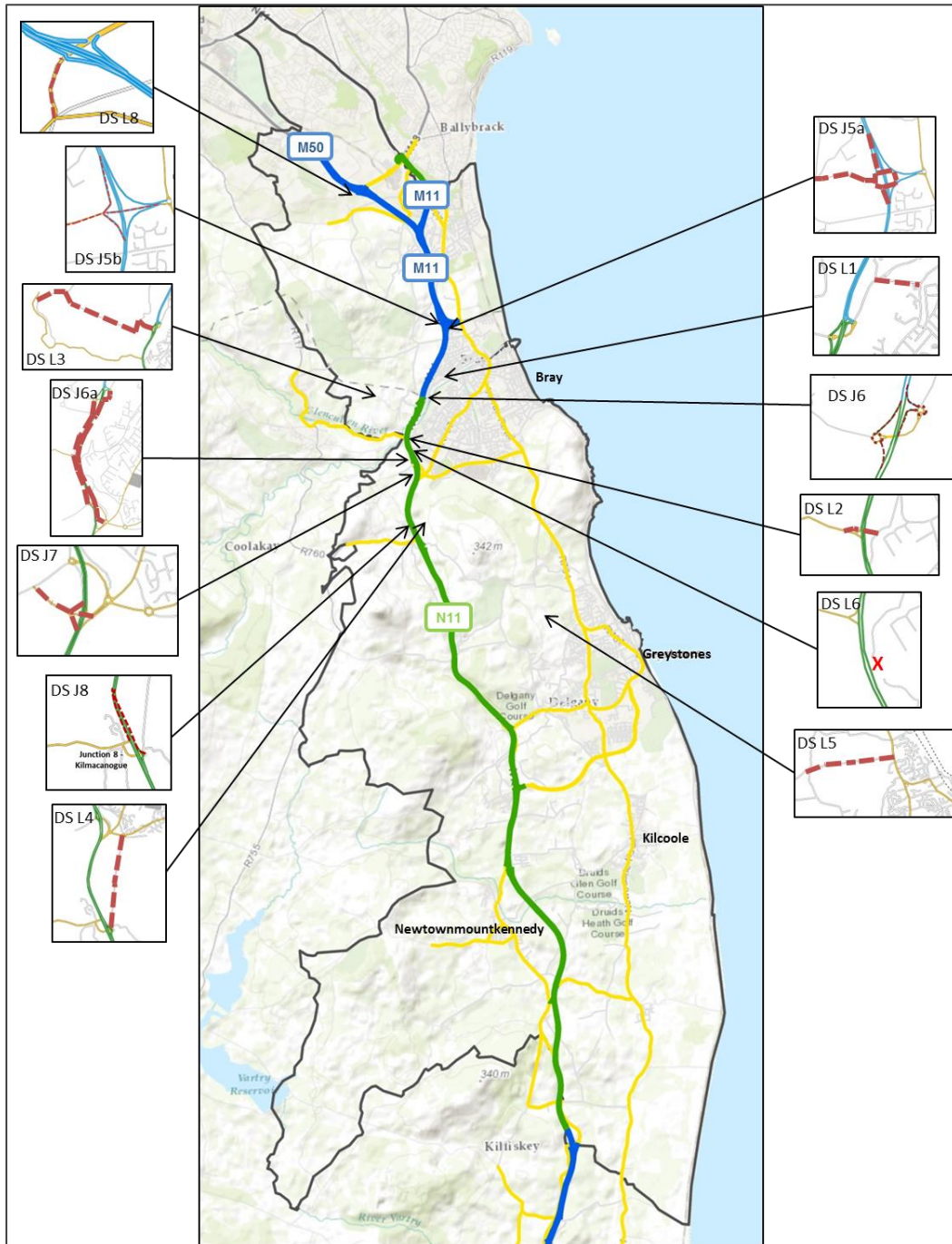


Figure 3.14: Study Area with the Location of Proposed Measures

## 4.0 Assessment of Proposed Measures

This section presents the impacts of each of the proposed measures. The performance of the various measures is discussed with reference to changes in traffic routing (difference plots), overall network performance (key network statistics) and the impact upon the M11/N11 mainline flows.

Each proposed measure was initially tested using the 2015 LAM's to assess its direct impact in the short term. The results of the 2015 assessment were then used to determine whether the proposed measure provides a notable benefit and is appropriate for further testing in the 2030 LAM's. Finally, the impact of the proposed measure in 2030 was used to inform the overall Emerging Preferred Strategy for the M11/N11 corridor.

### 4.1 Difference Plots

The difference plots presented in the following sections compare the modelled AM and PM peak static flow volumes for each of the individual 2015 or 2030 Do-Something scenario to their corresponding Do-Minimum volumes. The following points should be noted in the presentation of difference plots:

- The difference plots show the re-assignment (transfer) of traffic from one section of the network to another as a direct result of the proposed measure;
- A red bar indicates a change in flow above the Do-Minimum volume, whilst a green bar indicates a change in flow below the Do-Minimum volumes;
- The thickness of the red or green bar relates to the magnitude of change. The thicker the bar the greater the volume change;
- Do-Something measures J6a and L7 have been combined into one measure for testing (i.e. L7); and
- The impacts of the J8 measures cannot be modelled in the LAMs, as the existing direct accesses that would be served by the proposed services roads are not included in the LAM network.

### 4.2 Key Network Statistics

The impact of a proposed measure is assessed in relation to its impact upon the performance of the overall network (i.e. all roads included in the modelled network). A proposal may benefit on section on the road network but have a dis-benefit to another section. The network statistics combine both the benefits and dis-benefits (if applicable) of a proposed measure to give an overall indication of the performance of the proposal. The following key network statistics are provided in relation to each of the proposed measures:

- **Total Trips (vehicles per hour)** – Total number of trips assigned to the modelled road network;
- **Total Travel Time (hours)** – Total travel time of each individual trip in the overall network combined;
- **Travel Time per Vehicle (mins)** – Average travel time per vehicle;
- **Total Distance (kilometres)** – Total distance travelled on the modelled road network: and
- **Total Delay (hours)** – Total number of hours of congestion on the modelled road network (total travel time minus free flow travel time).

### 4.3 Impact Upon M11/N11 Mainline Flows

The impact of a proposed measure in terms of increase or decreasing the flow of traffic on the M11/N11 mainline corridor is provided as part of the assessment.

5.0 2015 Assessment – M11/N11 Mainline Junction Measures

5.1 Junction 5 – Bray North

The AM and PM peak hour modelled flow volumes in DS J5a and DS J5b are compared to the corresponding modelled flow volumes in the Do-Nothing (DN) scenario in the difference plots in Figures 5.1 and 5.2.

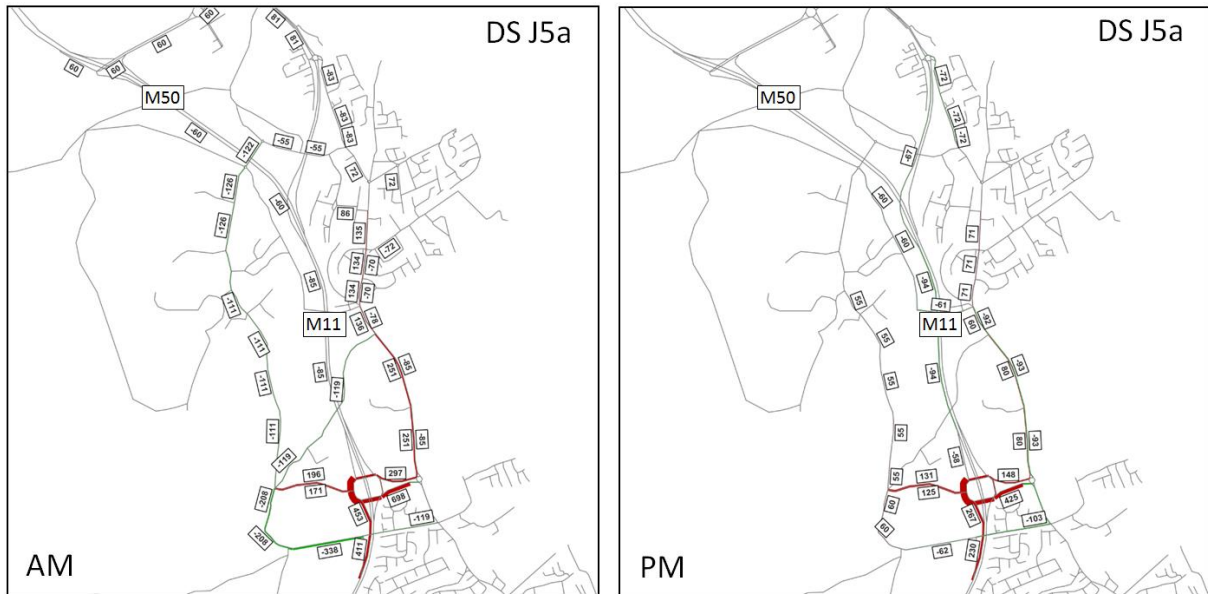


Figure 5.1: DS J5a AM and PM Peak Difference Plots

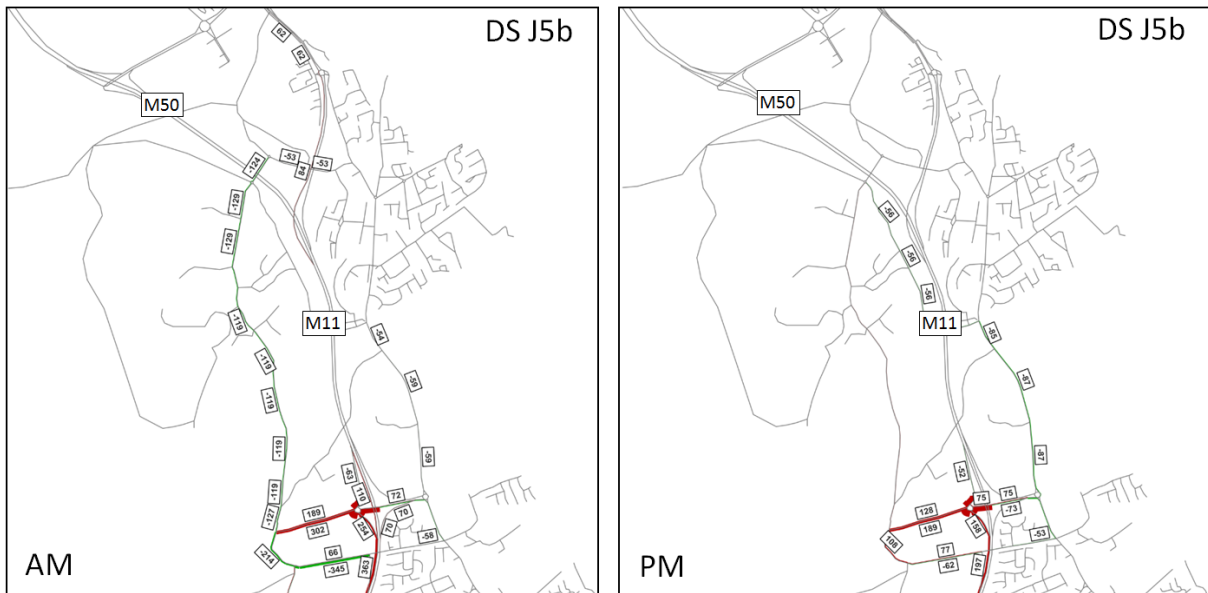


Figure 5.2: DS J5b AM and PM Peak Difference Plots

The closure and relocation of the existing northbound off-ramp and inclusion of the link road between the proposed junction and Ferndale road in both proposals lead to:

- A reduction in traffic on Old Connaught Avenue as traffic now uses the new northbound off ramp and link road to Ferndale Road in both peaks; and

- Changes in flow on both Ferndale Road and the R119 between Bray and Shankill.

### 5.1.1 Network Statistics

Table 5.1 provides a summary of the key network statistics for both DS J5a and DS J5b scenarios in the AM and PM alongside the Do-Nothing scenario.

Table 5.1: AM & PM Peak Hour Modelled Network Statistics: DS J5a

| Scenario       | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|----------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN     | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DS J5a | 17,721                | 4,655                   | 15.76                          | 201,565             | 1,001             |
| 2015 AM DS J5b | 17,721                | 4,655                   | 15.76                          | 201,816             | 1,001             |
|                |                       |                         |                                |                     |                   |
| 2015 PM DN     | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DS J5a | 17,706                | 4,447                   | 15.07                          | 200,571             | 806               |
| 2015 PM DS J5b | 17,706                | 4,449                   | 15.08                          | 200,754             | 808               |

The statistics indicates that neither proposal will have a significant impact upon the overall performance of the network based on 2015 traffic levels. The existing congestion issues on both the M11 mainline and on the regional road network (R761) will not be alleviated by increasing the capacity of this junction.

### 5.1.2 Impact on M11/N11 Mainline Flows

Referring to Tables C.1 – C.2 (Annex C), both proposals have a negligible impact on the mainline flows of the M11/N11 corridor.

### 5.1.3 Summary

At present there are no significant congestion/operational issues associated with Junction 5 Bray North (Wilford). Congestion issues in this area are caused not by the limited capacity of the Bray North junction but by the limited capacity of the regional/local road network and by the M11 mainline corridor.

The difference plots and network statistics demonstrated that neither proposal will have a significant impact. Therefore a proposal to upgrade the Bray North junction is not recommended for consideration as part of an Emerging Preferred Strategy. However, future public transport proposals (i.e. Luas extension to Bray) may require the upgrading of the junction and either of the two proposals considered could cater for this, also the link to Ferndale road would provide network resilience in the case on incidents on the M11 mainline corridor.

5.2 Junction 6 – Bray Central

Figure 5.3 depicts the difference plots for the AM and PM peak modelled flow volumes in the DS J6 scenario compared to the corresponding modelled flow volumes in the Do-Nothing scenario. The difference plots indicate that the increase in capacity associated with this proposal only leads to the reassignment of a small number of vehicles on the road network in both peaks.

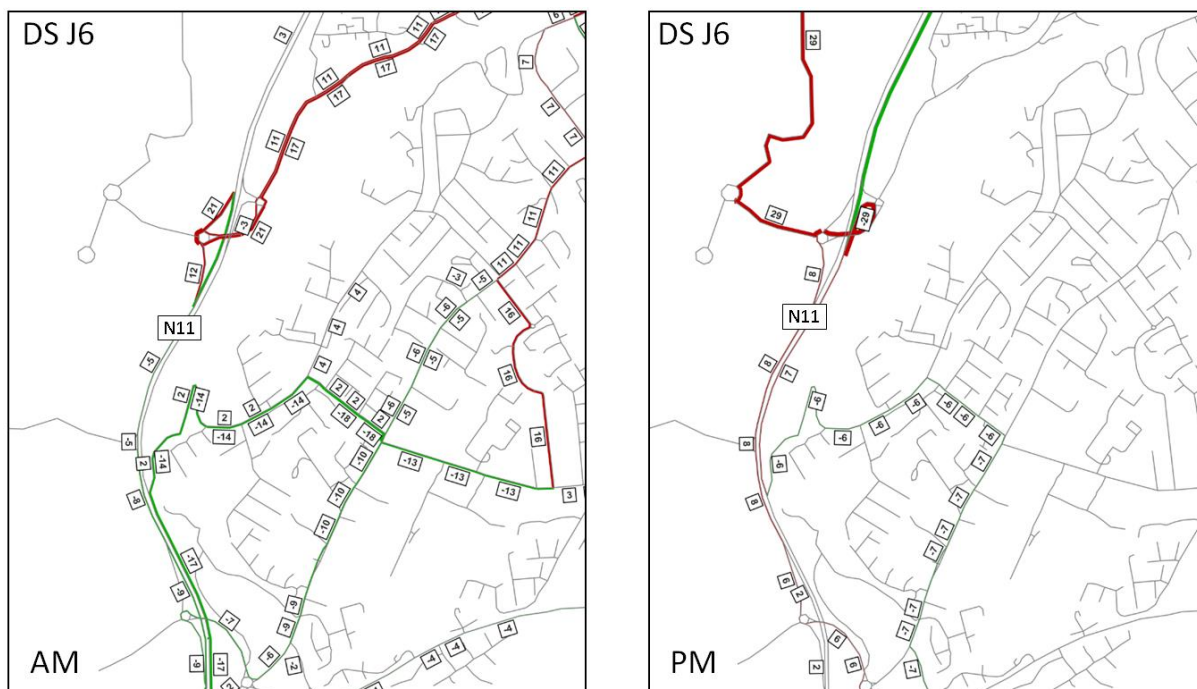


Figure 5.3: DS J6 AM and PM Peak Difference Plots

5.2.1 Network Statistics

Table 5.2 provides a summary of the key network statistics for the DS J6 scenario in the AM and PM alongside the DN scenario. The network statistics show a marginal positive benefit in both peaks.

Table 5.2: AM & PM Peak Hour Modelled Network Statistics: DS J6

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN    | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DS J6 | 17,721                | 4,643                   | 15.72                          | 201,581             | 992               |
| 2015 PM DN    | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DS J6 | 17,706                | 4,442                   | 15.05                          | 200,469             | 805               |



## 5.2.2 *Impact on M11/N11 Mainline Flows*

Referring to Tables C.1 – C.2 (Annex C) DS J6 has a negligible impact on the mainline flows of the M11/N11 corridor.

## 5.2.3 *Summary*

Do-Something J6 provides for an upgrade of the existing merges/diverges at Junction 6 (Bray Central) to the appropriate design standard and an increase in the capacity of the two existing roundabouts. The difference plots and networks statistics show limited impacts, however the need to bring the merges/diverges up to standard as part of the upgrading on the mainline corridor is the key driver for this proposal. Therefore this proposal is brought forward as part of the Emerging Preferred Strategy.

## **5.3 Junction 6a – Herbert Road/Enniskerry Road**

The proposal forms part of Do-Something L7. Full details of which are provided in Section 6.7.

5.4 Junction 7 – Bray South

Figure 5.4 depicts the difference plots for the AM and PM peak modelled flow volumes in the DS J7 scenario to the corresponding modelled flow volumes in the DN scenario.

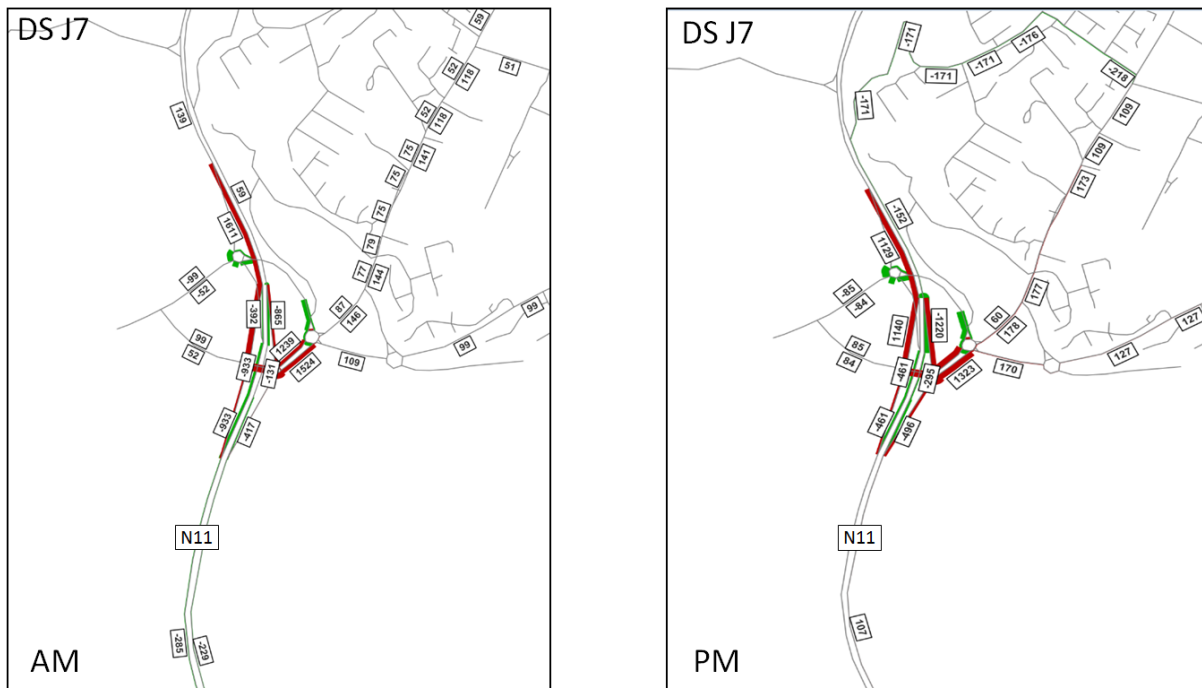


Figure 5.4: DS J7 AM and PM Peak Difference Plots

5.4.1 Network Statistics

Table 5.3 provides a summary of the key network statistics for the proposal in the AM and PM alongside the DN scenario. The statistics show a highly positive impact in both peaks, with both total delay and distance travelled reducing substantially.

Table 5.3: AM & PM Peak Hour Modelled Network Statistics

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN    | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DS J7 | 17,721                | 4,566                   | 15.46                          | 200,234             | 921               |
| 2015 PM DN    | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DS J7 | 17,706                | 4,388                   | 14.87                          | 200,008             | 762               |

5.4.2 Impact on M11/N11 Mainline Flows

Referring to Table C.1 - C.2 (Annex C) DS J7 leads to an increase in flow (approx. 100 vehicles) on the N11 mainline northbound between Junction 6 and Junction 7 in the AM Peak . This is caused by traffic now access the N11 at Junction 7 via Killarney Road instead of Herbert Road. A reduction in traffic (approx. 150 vehicles) on the N11 southbound between Junction 6a and 7 in the PM Peak is

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also noted, this is also due to traffic reassigning from Herbert Road to Killarney Road.

### 5.4.3 *Summary*

At present there are significant congestion issues at Junction 7 – Bray South and this proposal will alleviate this congestion as illustrated by the network statistics. Therefore it is recommended that this proposal be brought forward for further testing in the 2030 LAM's.

### **5.5 Junction 8 – Kilmacanogue**

The local accesses that would be served by the proposed parallel services roads are not included in the LAM network. Therefore no assessment is undertaken based on model outputs. The need for services roads at these locations is both to improve safety on this section of the N11 and to improve the efficiency of the corridor. This will bring this section of the N11 up to the appropriate standard for a TEN-T road and will also allow the current speed limit to be increase to 100kph in both directions. Therefore this proposal is proposed as part of the Emerging Preferred Strategy for the corridor.

6.0 2015 Assessment - M11/N11 Mainline Junction Measures

6.1 Do-Something L1 – Herbert Road/Dargle Road Link

Figure 6.1 depicts the difference plots for the AM and PM peak modelled flows volumes in the Do-Something L1 (DS L1) scenario to the corresponding modelled flow volumes in the DN scenario. The plots shows a reduction in traffic flows on the M11 mainline between Junctions 6 and 7 as traffic is now able to access the areas of Bray south of the River Dargle via Junction 6.

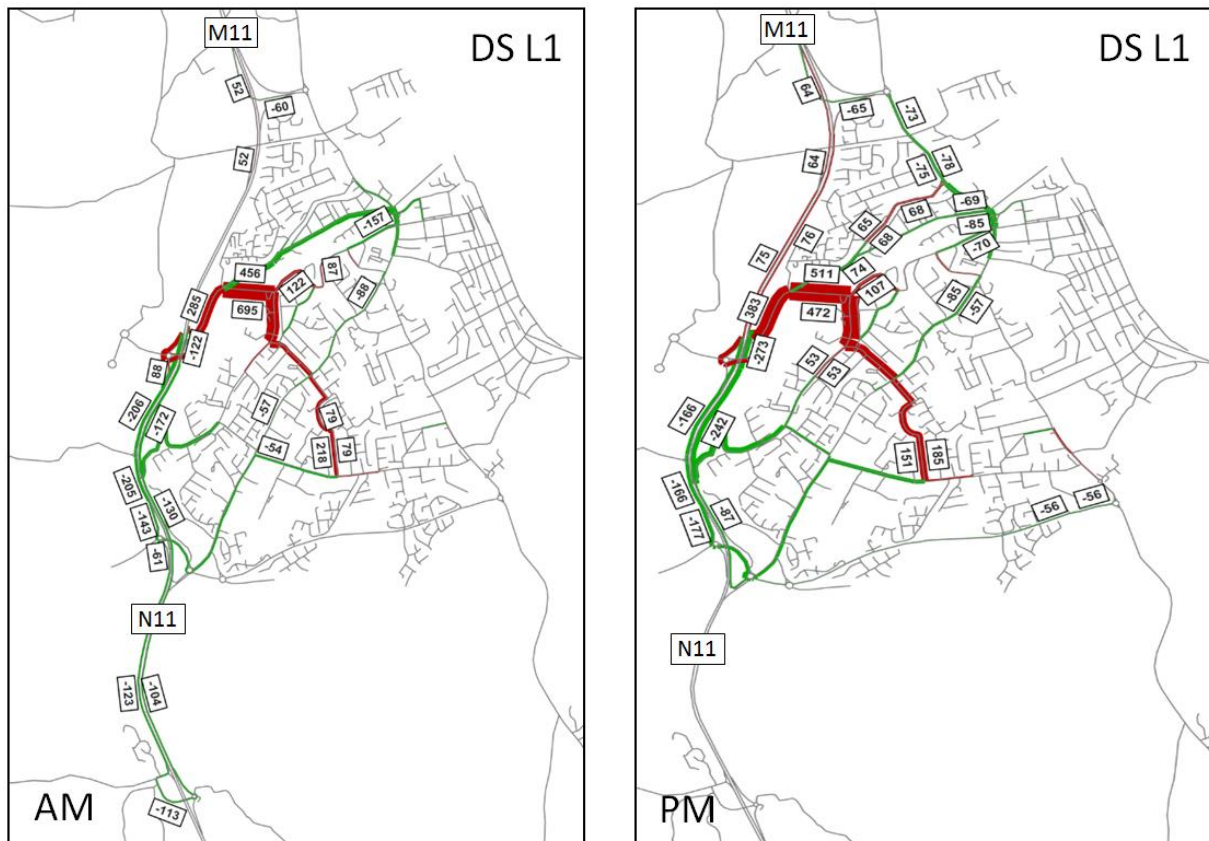


Figure 6.1: DS L1 AM and PM Peak Difference Plots

6.1.1 Network Statistics

Table 6.1 provides a summary of the key network statistics for DS L1 in the AM and PM alongside the Do-Nothing scenario. The statistics show that there are significant reductions in both the total network delay and total distance travelled in the network.

Table 6.1: AM & PM Peak Hour Modelled Network Statistics DS L1

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN    | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DS L1 | 17,721                | 4,502                   | 15.24                          | 200,092             | 877               |
| 2015 PM DN    | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DS L1 | 17,706                | 4,391                   | 14.88                          | 199,969             | 762               |

6.1.2 Impact on M11/N11 Mainline Flows

Referring to Tables C.3 and C.4 of Annex C, DS L1 leads to a reduction in traffic on the N11 mainline between Junctions 6 and 7.

6.1.3 Summary

DS L1 provides for a link road between Herbert and Upper Dargle Road. It provides an additional crossing of the River Dargle and allows access to Junction 6 (Bray Central/Fassaroe). This scenario results in positive improvements to travel time and reduction delay in both the AM and PM peak periods.

The difference plots demonstrate that this scenario is effective in increasing the number of vehicles accessing the N11 via Junction 6 (Fassaroe) rather than continuing down Herbert Road and accessing the N11 via Junction 6a (thereby resulting in less disruption to mainline flow).

However, the precise location for a bridge crossing of the River Dargle will require further consideration. In addition to any benefit to the M11/N11 corridor, the location of the crossing will be influenced by the requirements of public transport, walking and cycling and local trips and the technical feasibility of crossing the river.

6.2 Do-Something L2 - Bridge Over N11 at Junction 6a

Figure 6.2 depicts the difference plots for the AM and PM peak modelled flow volumes in the Do-Something L2 (DS L2) scenario to the corresponding modelled flow volumes in the DN scenario. The proposed bridge over the N11 would carry approximately 1000 vehicles in the AM peak.

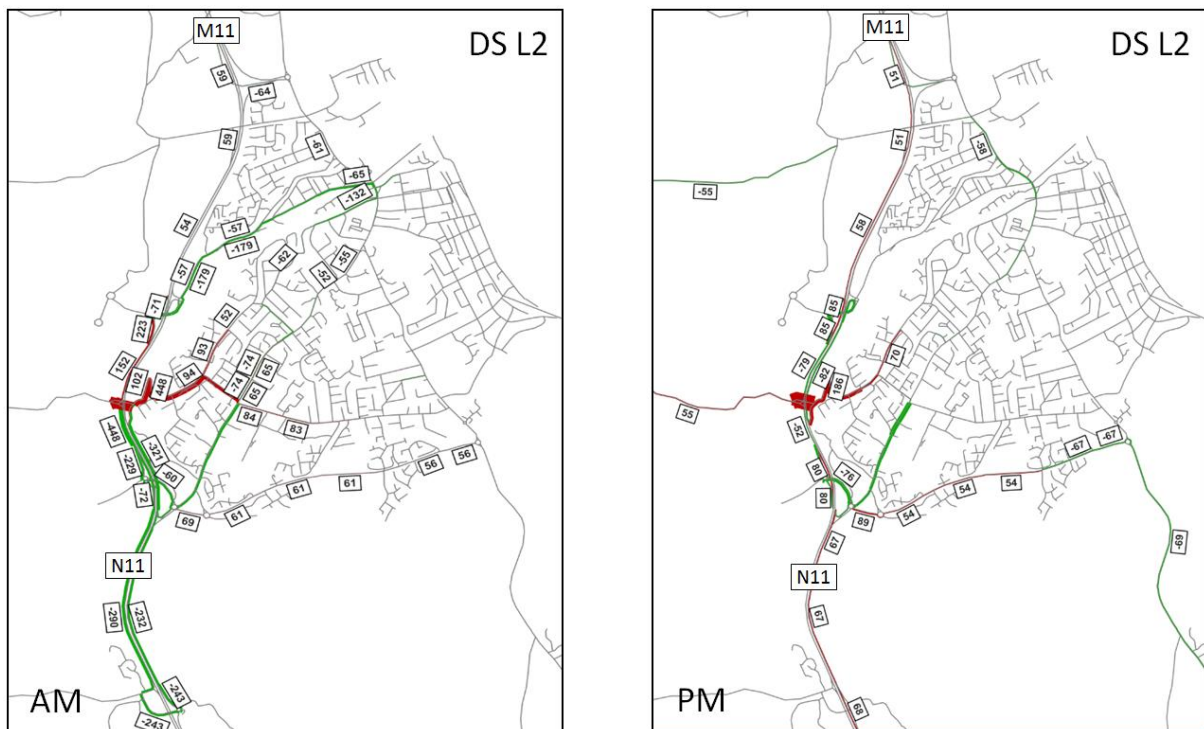


Figure 6.2: DS L2 AM and PM Peak Difference Plots

## 6.2.1 Network Statistics

Table 6.2 provides a summary of the key network statistics for DS L2 in the AM and PM alongside the DN scenario. The tables show that the proposal would provide benefits most notably in the AM Peak.

Table 6.2: AM & PM Peak Hour Modelled Network Statistics DS L2

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN    | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DS L2 | 17,721                | 4,494                   | 15.22                          | 199,093             | 884               |
| 2015 PM DN    | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DS L2 | 17,706                | 4,412                   | 14.95                          | 200,068             | 791               |

## 6.2.2 Impact on M11/N11 Mainline Flows

Referring to Table C.3 and C.4 (Annex C) DS L2 reduces the number of vehicles on the N11 mainline between Junction 6 and 7 , most notably in the AM Peak.

## 6.2.3 Summary

DS L2 provides for a bridge over the N11 (Junction 6a) between Herbert Road and Enniskerry Road (R117). The network statistics revealed that this scenario results in improvements to travel time and delay for the overall network particularly in the AM Peak. However, providing three junctions in close proximity (<2km) with full turning movements would not be recommend from a safety, operational or efficiency perspective. Therefore it is not recommended to include this proposal in the Emerging Preferred Strategy.

## 6.3 Do-Something L3 - Enniskerry Link Road

Figure 6.3 depicts the difference plots for the AM and PM peak modelled flows volumes in the Do-Something L3 (DS L3) scenario to the corresponding modelled flow volumes in the DN scenario.

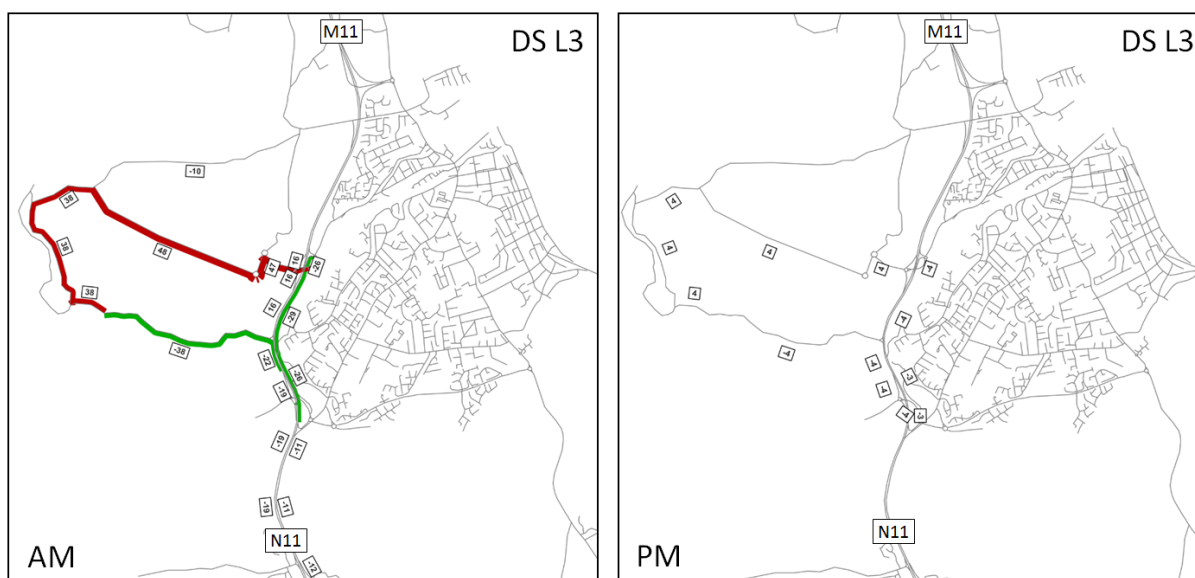


Figure 6.3: DS L3 AM and PM Peak Difference Plots

### 6.3.1 Network Statistics

Table 6.3 provides a summary of the key network statistics DS L3 in the AM and PM alongside the DN scenario. The statistics indicated that the impact of the proposal is negligible.

Table 6.3: AM & PM Peak Hour Modelled Network Statistics: DS L3

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN    | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DS L3 | 17,721                | 4,636                   | 15.70                          | 201,548             | 985               |
| 2015 PM DN    | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DS L3 | 17,706                | 4,444                   | 15.06                          | 200,450             | 806               |

### 6.3.2 Impact on M11/N11 Mainline Flows

Referring to Table C.3 and C.4 (Annex C) the impact of DS L3 on the mainline flows is negligible.

### 6.3.3 Summary

DS L3 provides for a link road between Junction 6 (Bray Central/Fassaroe) and Enniskerry. This scenario provides only marginal improvements in travel time and delay in the AM and PM peaks. Closer inspection of the difference plots shows that the traffic volumes using this link are relatively low and furthermore there are no improvements to the mainline flow when compared to the Do-Nothing scenarios.

Finally, from a financial feasibility perspective, this option is dependent on private sector funding and therefore not guaranteed to progress. Therefore, for the above reasons it is not considered a viable option to be included as part of an Emerging Preferred Strategy for the M11/N11 corridor.

## 6.4 Do-Something L4 – Kilmacanogue to Bray Southern Cross Link

Figure 6.4 depicts the difference plots for the AM and PM peak modelled flow volumes in the Do-Something L4 (DS L4) scenario to the corresponding modelled flow volumes in the DN scenario.

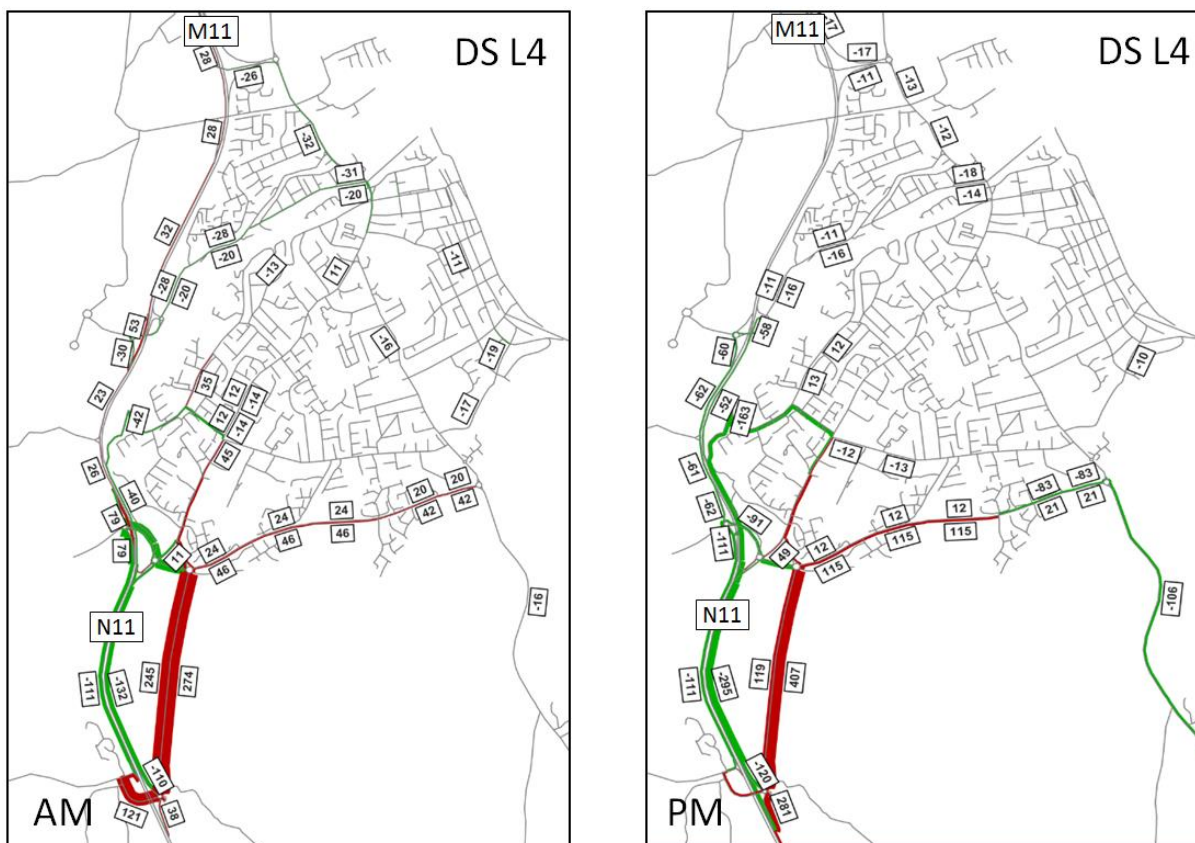


Figure 6.4: DS L4 AM and PM Peak Difference Plots

6.4.1 Key Network Statistics

Table 6.4 provides a summary of the key network statistics for DS L4 in the AM and PM alongside the Do-Nothing scenario. The statistics show that benefits are provided in both peaks as a result of the proposal.

Table 6.4: AM & PM Peak Hour Modelled Network Statistics: DS L4

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN    | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DS L4 | 17,721                | 4,578                   | 15.50                          | 201,808             | 924               |
| 2015 PM DN    | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DS L4 | 17,706                | 4,394                   | 14.89                          | 199,752             | 772               |

6.4.2 Impact on M11/N11 Mainline Flows

Referring to Table C.3 and C.4 (Annex C) DS L4 reduces the volume of traffic on the N11 mainline though Junction 7 and on the mainline between Junction 7 and 8 by approximately 100 vehicles northbound in the AM and approximately 300 vehicles southbound in the PM.



6.4.3 Summary

This scenario provides for a link road between Bray Southern Cross Road and Junction 8 (Kilmacanogue). This proposal shows positive improvements in travel time and delay in the in both peaks. The difference plots demonstrate that the new link is successful in attracting traffic away from the mainline between Junction 7 and Junction 8 thereby proving beneficial to the corridor along this section (in addition to being beneficial to the study area as a whole as demonstrated by the network statistics). It is recommended that this option is brought forward to the 2030 assessment.

6.5 Do-Something L5 – Greystones Link Road

Figure 6.5 depicts the difference plots for the AM and PM peak modelled flow volumes in the Do-Something L5 (DS L5) scenario to the corresponding modelled flow volumes in the DN scenario. The plots show that the proposal leads to an increase in traffic volumes on the N11 mainline between Junction 7 and Junction 9 and reduction in traffic on the R761 Bray-Greystones Road.

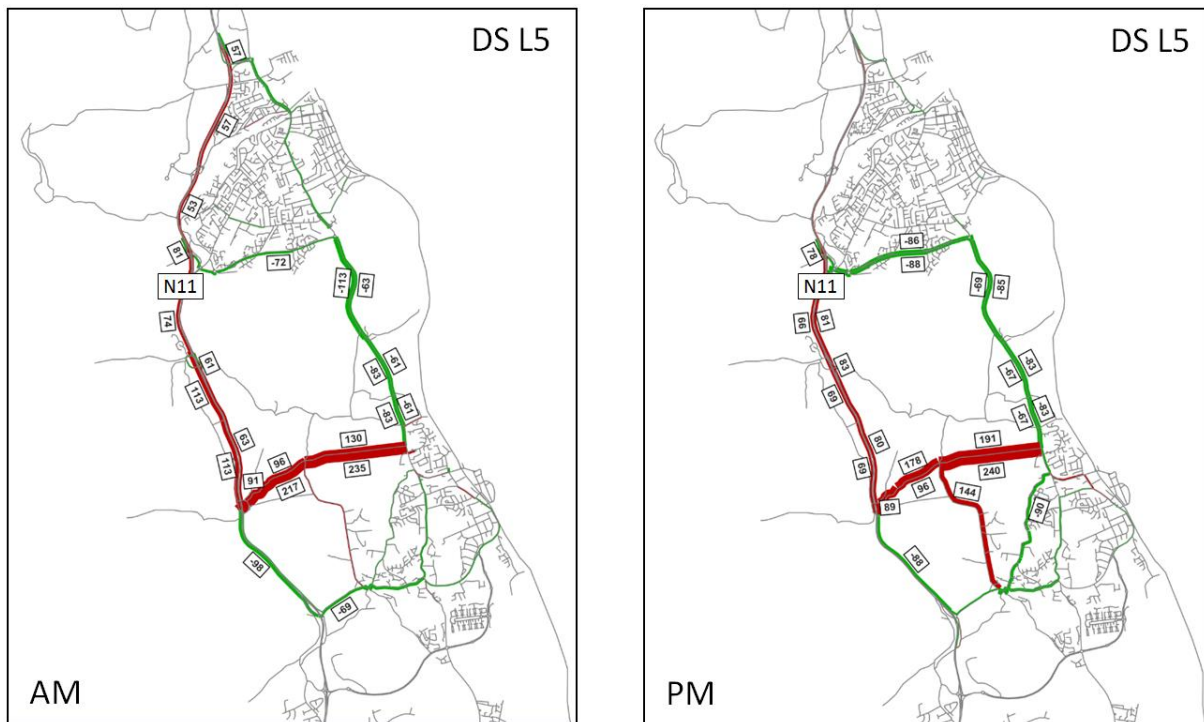


Figure 6.5: DS L5 AM and PM Peak Difference Plots

6.5.1 Network Statistics

Table 6.5 provides a summary of the key network statistics for DS L5 in the AM and PM alongside the DN scenario. The statistics indicate that the proposal provide overall benefits to the network in both peaks.

Table 6.5: AM & PM Peak Hour Modelled Network Statistics: DS L5

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN    | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DS L5 | 17,721                | 4,563                   | 15.45                          | 201,772             | 907               |
| 2015 PM DN    | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DS L5 | 17,706                | 4,411                   | 14.95                          | 200,741             | 769               |

### 6.5.2 Impact on M11/N11 Mainline Flows

Referring to Table C.3 and C.4 (Annex C), DS L5 leads to a small increase in traffic volumes on the N11 mainline between Junctions 7 and 9 during both peak hours. Traffic volumes between Junction 9 and 10 reduce by approximately 100 vehicles.

### 6.5.3 Summary

DS L5 provides for a new link road from the R761 at Greystones to Ballydonagh Road (Greystones Link Road) improving access onwards to the N11 at Junction 9 (Glen of the Downs). When considered in isolation there is a small increase in traffic volumes between Junctions 8 and 9 with a subsequent reduction along the Bray Southern Cross Road. This equates to a 4% increase in flows on the N11 between Junctions 8 and 9.

However when considered with the Junction 7 upgrade in place traffic continues to use the R761/R768 Bray Southern Cross. This road is of a good standard and the link flow is comfortably below the capacity. Therefore this proposal is not recommended for inclusion in the Emerging Preferred Strategy.

## 6.6 Do-Something L6 - Closure of Direct Access at Junction 6a between N11 and Herbert Road

Figure 6.6 depicts the difference plots for the AM and PM peak modelled flow volumes in the Do-Something L6 (DS L6) scenario to the corresponding modelled flow volumes in the DN scenario. The lots shows that the closure of access to Herbert Road from the N11 leads to an increase in traffic between Junction 6a and 7 and also a transfer of the traffic from the N11 to the regional/local road network through Bray.

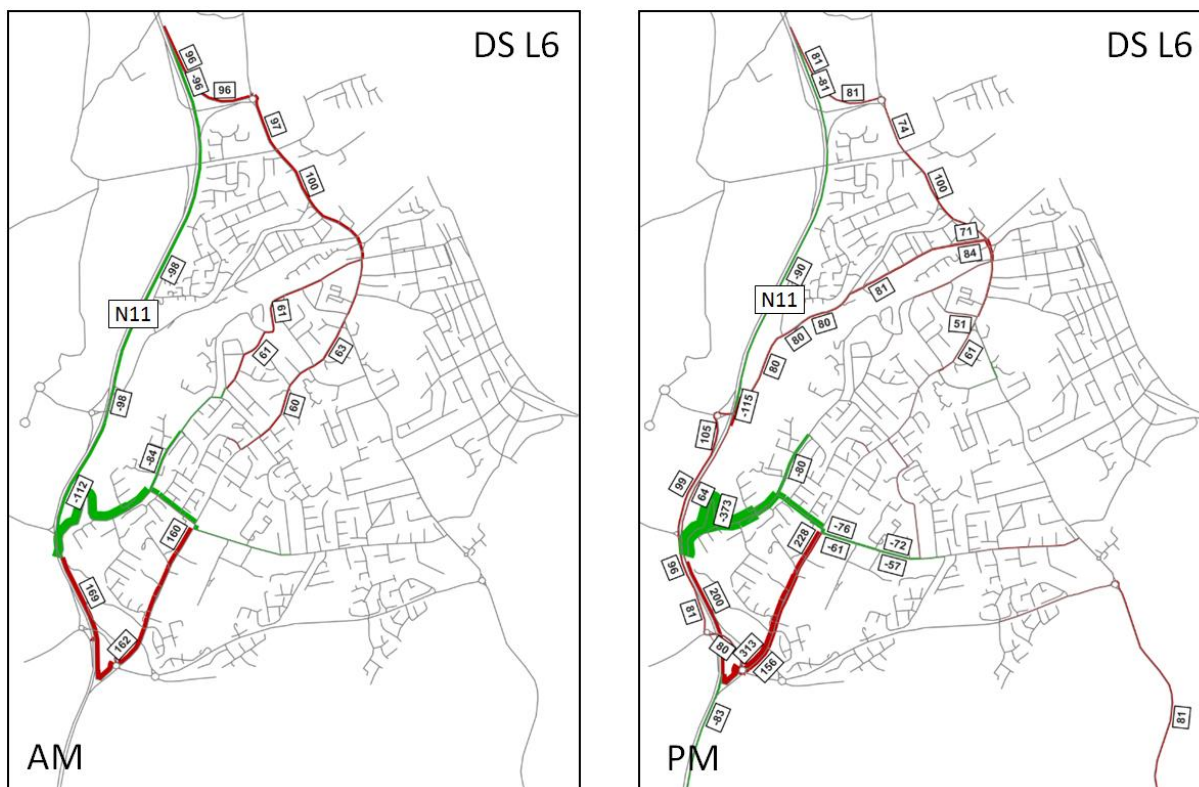


Figure 6.6: DS L6 AM and PM Peak Difference Plots

6.6.1 Key Network Statistics

Table 6.6 provides a summary of the key network statistics for DS L6 in the AM and PM alongside the DN scenario. The statistics show that this proposal has a negative impact upon the performance of the overall network particularly during the PM Peak as vehicles must now continue southbound along the N11 to use Junction 7 in order to access Bray.

Table 6.6: AM & PM Peak Hour Modelled Network Statistics: DS L6

| Scenario     | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|--------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN   | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DSL6 | 17,721                | 4,667                   | 15.80                          | 201,558             | 1,014             |
| 2015 PM DN   | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DSL6 | 17,706                | 4,528                   | 15.35                          | 200,953             | 875               |

6.6.2 Impact on M11/N11 Mainline Flows

Referring to Table C.3 and C.4 (Annex C) DS L6 leads to an increase in traffic volumes on the N11 mainline between Junction 6a and 7 in the AM Peak and Junction 6 and 7 in the PM Peak.

6.6.3 Summary

DS L6 provides for the closure of direct access between Herbert Road and the N11 on the eastern side of the N11. The intention of the scenario is to reduce the level of traffic weaving and remove

direct access in order to improve the efficiency and safety of this section of the N11. The network statistics clearly demonstrated the negative impacts of this proposal in terms of travel time and delay while the difference plots highlighted the increased pressure on the local and regional network. In its current form (i.e. as presented in this note) the closure of Herbert Road as an isolated proposal is not considered viable.

A modified form of this scenario allowing traffic from Herbert Road to access Junction 7 via a local service road is considered viable and is included as part of the Do-Something L7 proposal.

**6.7 Do-Something L7 – Closure of Direct Access to N11 at Junction 6a plus Services Roads**

Figure 6.7 below depicts the difference plots for the AM and PM peak modelled flows volumes in the Do-Something L7 (DS L7) scenario to the corresponding modelled flow volumes in the DN scenario.



Figure 6.7: DS L7 AM and PM Peak Difference Plots

**6.7.1 Network Statistics**

Table 6.7 provides a summary of the key network statistics for DS L7 with the DN scenario included for comparison purposes. The statistics indicate that this proposal when considered in isolation has a slightly negative impact in the AM Peak and slighty positive impact in the PM Peak.

Table 6.7: AM & PM Peak Hour Modelled Network Statistics: DS L7

| Scenario     | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|--------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN   | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DSL7 | 17,721                | 4,665                   | 15.80                          | 201,411             | 1,005             |
| 2015 PM DN   | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DSL7 | 17,706                | 4,451                   | 15.08                          | 200,909             | 797               |

6.7.2 Impact on M11/N11 Mainline Flows

Referring to Table C.3 and C.4 (Annex C) DS L7 would significantly reduce traffic volumes on the N11 mainline between Junction 6 and 7 as traffic between the N11 and Herbert Road/Enniskerry Road uses the proposed service roads.

6.7.3 Summary

Do-Something L7 provides for one-way parallel service roads connecting Junction 6a to Junctions 6 and 7 on the western side of the N11 and to Junction 7 on the eastern side of the N11. This option resulted in marginal changes to the overall performance of the overall network. However, the assessment does not take into account the safety benefits and improved efficiency associated with the proposal. Therefore, it is recommended that this proposal is brought forward for consideration as part of the 2030 assessment.

6.8 Do-Something L8 – M50 Cherrywood Junction to Ballycorus Road Link

Figure 6.8 below illustrates the difference plots for the AM and PM peak modelled flows volumes in the Do-Something L8 (DS L8) scenario to the corresponding modelled flow volumes in the DN scenario. The plots show the reassignment of traffic from the Shankill area and limited impact upon the M11/N11 corridor.

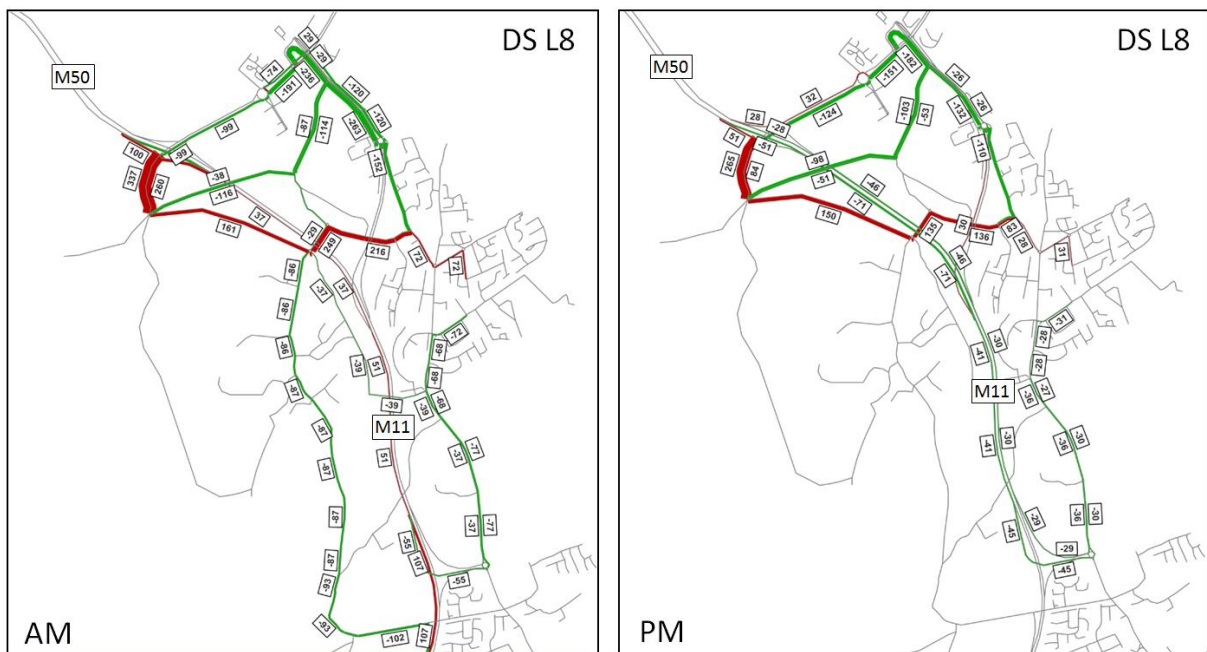


Figure 6.8: DS L8 AM and PM Peak Difference Plots

6.8.1 Network Statistics

Table 6.8 provides a summary of the key network statistics for DS L8 and the DN scenario. The statistics shows a slightly positive benefit in both peak hours, with a reduction in delay and travel distance noted.

Table 6.8: AM & PM Peak Hour Modelled Network Statistics: DS L8

| Scenario     | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|--------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2015 AM DN   | 17,721                | 4,648                   | 15.74                          | 201,602             | 997               |
| 2015 AM DSL8 | 17,721                | 4,619                   | 15.64                          | 200,879             | 984               |
| 2015 PM DN   | 17,706                | 4,445                   | 15.06                          | 200,448             | 807               |
| 2015 PM DSL8 | 17,706                | 4,420                   | 14.98                          | 199,803             | 794               |

### 6.8.2 Impact on M11/N11 Mainline Flows

Referring to Table C.3 and C.4 (Annex C), DS L8 as a negligible impact on the N11 mainline flows.

### 6.8.3 Summary

DS L8 provides for a link road from Rathmichael/Ballycorus Road to M50 Junction 16 (Cherrywood). This proposal provides an alternative route for users travelling from the Shankill area to the M50 by allowing them a more direct route thereby potentially avoiding travelling to this destination via M11 Junction 5 (Bray North/Wilford).

As the network statistics have demonstrated, this scenario results in only minor benefits in travel time and reduction in delay. The difference plots have shown that the introduction of the link provides a shorter route to the M50 for traffic in Shankill.

In the PM peak the reduction of the U-turn movement down to Wilford Junction is also apparent. This scenario is unlikely to show benefits for the current situation although is likely to be very beneficial should an incident occur on the M11/N11 corridor. The relatively low benefits of this scenario (in terms of the travel time and delay improvement) are outweighed by the new link's contribution to network resilience in providing an alternative route to the M50. For these reasons it is recommended that this scenario be included for consideration in an Emerging Preferred Strategy.

## 6.9 2015 Assessment Summary

The results of the 2015 analysis indicated that some options should be excluded from further assessment due to a limited or negative impact. The remaining options which had a positive influence were tested in the 2030 model. A summary of the proposal considered is provided in Table 6.9.

Table 6.9: Measure Brought Forward to 2030 Assessment

| Scenario | Included in 2030 Assessment | Assessment Summary                                      |
|----------|-----------------------------|---|
| J5       | x                           | No further assessment                                   |
| J6       | ✓                           | Included in Emerging Preferred Strategy                 |
| J7       | ✓                           | Further assessment in 2030 LAM                          |
| J8       | ✓                           | Included in Emerging Preferred Strategy                 |
| L1       | ✓                           | Further assessment in 2030 LAM                          |
| L2       | x                           | No further assessment (minimal benefit to N11 corridor) |

| Scenario | Included in 2030 Assessment | Assessment Summary   |
|----------|-----------------------------|--|
| L3       | x                           | No further assessment (minimal benefit to N11 corridor)      |
| L4       | ✓                           | Further assessment in 2030 LAM                               |
| L5       | x                           | No further assessment (minimal benefit to Glen of the Downs) |
| L6       | x                           | Negative impact on N11 corridor – No further assessment      |
| L7       | ✓                           | Further assessment in 2030 LAM                               |
| L8       | ✓                           | Included in Emerging Preferred Strategy (network resilience) |

## 7.0 2030 Assessment

The proposals assessed against the 2015 Do-Nothing LAM's which were considered beneficial to M11/N11 corridor were then tested against the 2030 Do-Minimum (DM) LAM's in order to assess their suitability for inclusion in the Emerging Preferred Strategy. The 2030 Do-Minimum scenario assumes that the widening of the M11/N11 corridor is in place based on the assessment of M11/N11 mainline capacity discussed in Section 3.1. The following proposals are assessed against the 2030 Do-Minimum scenario:

- Do-Something J7 - Junction 7 Bray South;
- Do-Something L1 - Herbert Road/Dargle Road Link;
- Do-Something L4 - Kilmacanogue to Bray Southern Cross Link; and
- Do-Something L7 - Closure of Direct Access to N11 at Junction 6a plus Services Roads.

It is assumed that both DSJ6 (Junction 6 – Bray Central), DS J8 (Kilmacanogue Service Roads) and DS L8 (M50 Cherrywood Junction to Ballycorus Road Link) will form part of the Emerging Preferred Strategy and therefore do not require further assessment.

### 7.1 Do-Something J7 - Bray South

Figure 7.1 depicts the difference plots for the AM and PM peak modelled flow volumes in the DS J7 scenario to the corresponding Do-Minimum modelled flow volumes in 2030.

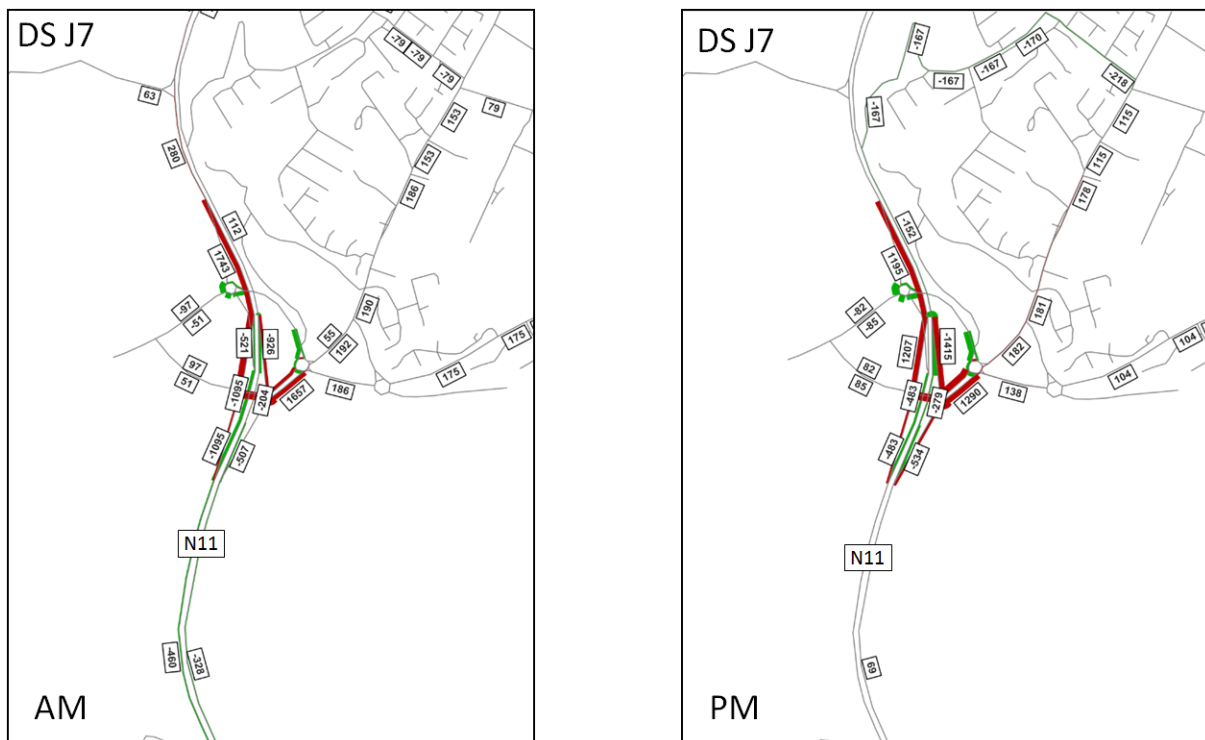


Figure 7.1: DS J7 AM and PM Peak Difference Plots

#### 7.1.1 Network Statistics

Table 7.1 provides a summary of the key network statistics for DS J7 in the AM and PM alongside the 2030 DM scenario. The statistics indicate the the proposal provides positive benefits in both the AM and PM peaks.



Table 7.1: AM & PM Peak Hour Modelled Network Statistics: DS J7

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2030 AM DM    | 21,284                | 5,740                   | 16.18                          | 248,432             | 1,333             |
| 2030 AM DS J7 | 21,284                | 5,548                   | 15.64                          | 246,480             | 1,180             |
| 2030 PM DM    | 21,223                | 5,451                   | 15.41                          | 244,970             | 1,102             |
| 2030 PM DS J7 | 21,223                | 5,380                   | 15.21                          | 244,591             | 1,049             |

### 7.1.2 Impact on M11/N11 Mainline Flows

Referring to Table C.5 - C.6 (Annex C) DS J7 leads to an increase in flow (approx. 200 vehicles) on the N11 mainline northbound between Junction 6 and Junction 7 in the AM Peak . This is caused by traffic now access the N11 at Junction 7 via Killarney Road instead of Herbert Road. A reduction in traffic (approx. 150 vehicles) on the N11 southbound between Junction 6a and 7 in the PM Peak is also noted, this is also due to traffic reassigning from Herbert Road to Killarney Road.

### 7.1.3 Summary

The network statistics indicate that the upgrading of Junction 7 is required regardless of the upgrading of the M11/N11 mainline. It is therefore recommend that this proposal form part of the Emerging Preferred Strategy.

## 7.2 Do-Something L1 – Herbert Road/Dargle Road Link

Figure 7.2 depicts the difference plots for the AM and PM peak modelled flow volumes in the DS L1 scenario to the corresponding DM modelled flow volumes in 2030. The plots show that volumes on the N11 between Junction 6 and 7 reduce as a result of this proposal. The plots also show an increase in traffic on the M11 between Junction 5 and 6 in the PM peak and a reduction in flow on the R761.

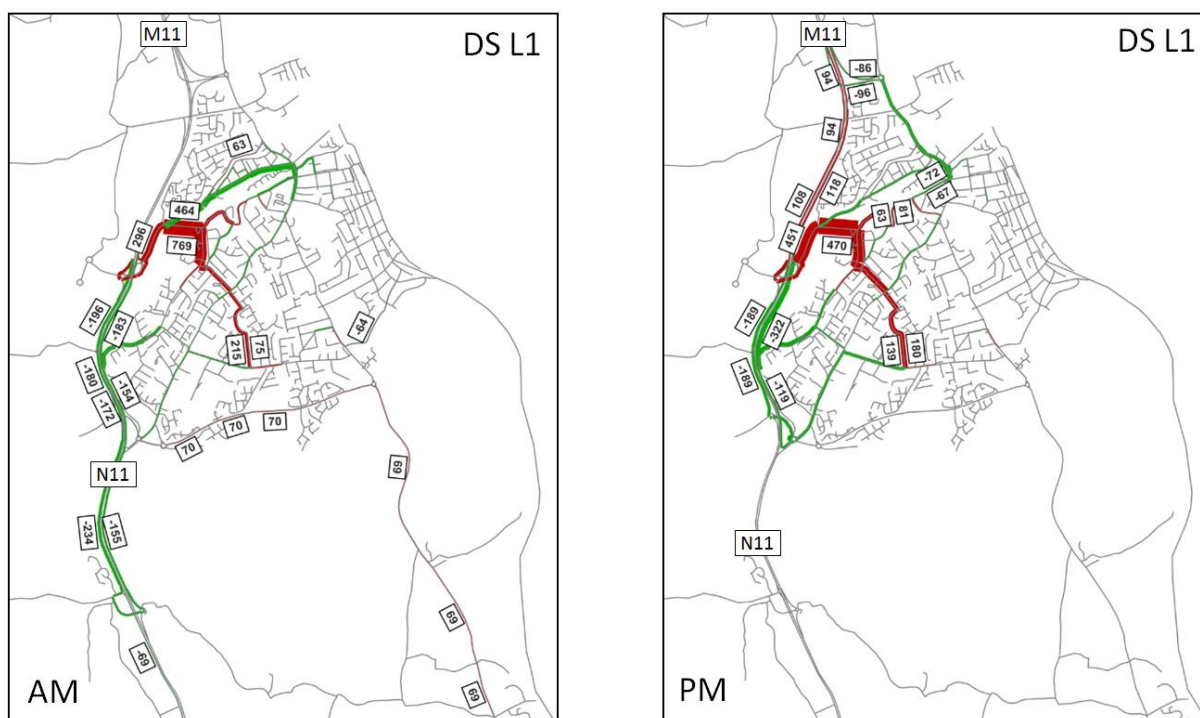


Figure 7.2: 2030 DS L1 AM and PM Peak Difference Plots

### 7.2.1 Network Statistics

Table 7.2 provides a summary of the key network statistics for DS L1 in the AM and PM alongside the DM scenario. The statistics indicate the proposal provide benefits in both the AM and PM Peaks, with a reduction in total delay and distance travelled noted.

Table 7.2: AM & PM Peak Hour Modelled Network Statistics: DS L1

| Scenario     | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|--------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2030 AM DM   | 21,284                | 5,740                   | 16.18                          | 248,432             | 1,333             |
| 2030 AM DSL1 | 21,284                | 5,603                   | 15.79                          | 246,172             | 1,233             |
| 2030 PM DM   | 21,223                | 5,451                   | 15.41                          | 244,970             | 1,102             |
| 2030 PM DSL1 | 21,223                | 5,389                   | 15.23                          | 244,495             | 1,051             |

### 7.2.2 Impact on M11/N11 Mainline Flows

As illustrated in the difference plots and referenced in Tables C.5 and C6 (Annex C), this proposal will reduce traffic volumes on the N11 between Junction 6 and 7 in both the AM and PM peaks.

### 7.2.3 Summary

The difference plots and network statistics indicate that the proposed Herbert Road/Dargle Road link is beneficial to both the M11/N11 corridor and to the wider network. It is therefore recommended that this proposal form part of the Emerging Preferred Strategy.

However, the precise location for a bridge crossing of the River Dargle will require further consideration. In addition to any benefit to the M11/N11 corridor, the location of the crossing will be influenced by the requirements of public transport, walking and cycling and local trips and the technical feasibility of crossing the river.

### 7.3 Do-Something L4 - Kilmacanogue to Bray Southern Cross Link

Figure 7.3 depicts the difference plots for the AM and PM peak modelled flow volumes in DS L4 to the corresponding Do-Minimum modelled flow volumes in 2030.

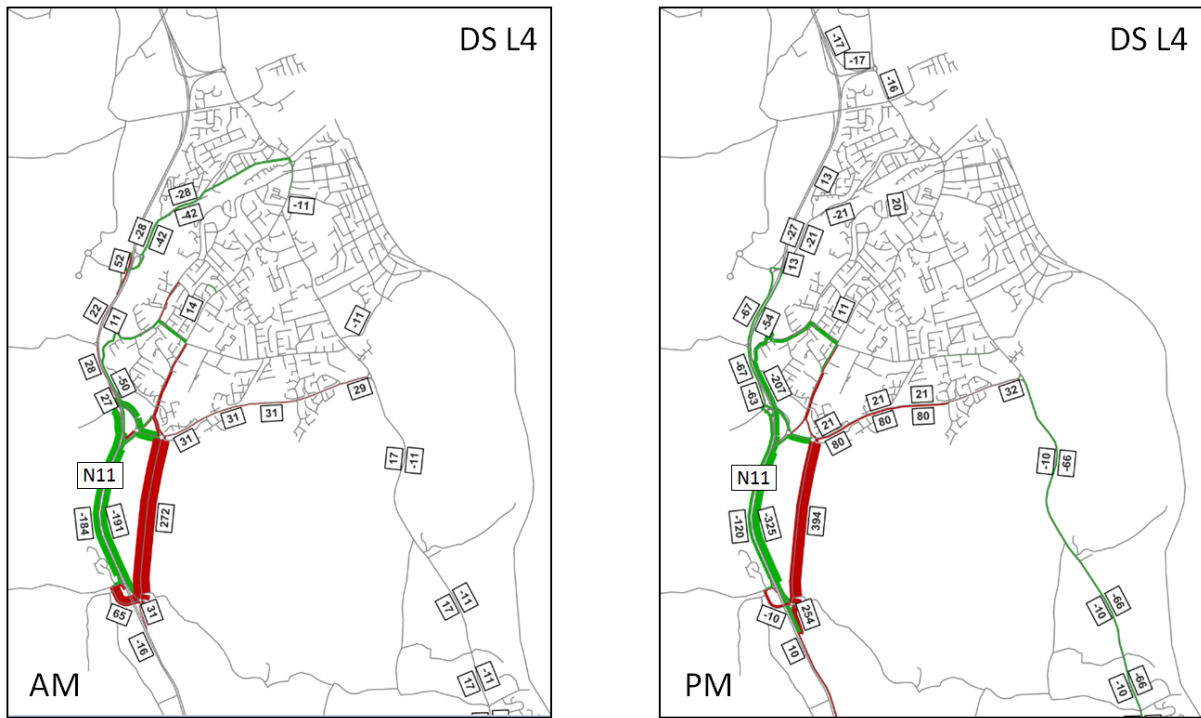


Figure 7.3: DS L4 AM and PM Peak Difference Plots

#### 7.3.1 Network Statistics

Table 7.3 provides a summary of the key network statistics for DS L4 in the AM and PM alongside the Do-Minimum scenario. The statistics indicate the the proposal provides benefits in both the AM and PM Peaks.

Table 7.3: AM & PM Peak Hour Modelled Network Statistics: DS L4

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2030 AM DN    | 21,284                | 5,740                   | 16.18                          | 248,432             | 1,333             |
| 2030 AM DS L4 | 21,284                | 5,709                   | 16.09                          | 248,250             | 1,303             |
| 2030 PM DN    | 21,223                | 5,451                   | 15.41                          | 244,970             | 1,102             |
| 2030 PM DS L4 | 21,223                | 5,404                   | 15.28                          | 244,327             | 1,067             |

### 7.3.2 Impact on M11/N11 Mainline Flows

With reference to Tables C.5 and C6 (Annex C), this proposal will reduce traffic volumes on the N11 between Junction 7 and 8 in both the AM and PM peaks.

### 7.3.3 Summary

The benefits of the scheme are limited when combined with the increased capacity on the N11 mainline. The increase in capacity of the mainline corridor, improvements to Junction 7 (DS J7) as outlined previously and the services road proposed at Kilmacanogue (DS J8) will have a significant impact on the level of service experienced by drivers between Junction 7 and Junction 8 during both peaks. Therefore it is not recommended that this option is included in the Emerging Preferred Strategy. However it is recognised there is still some merit in this option from the point of view of local accessibility.

### 7.4 Do-Something L7 - Closure of Direct Access to N11 at Junction 6a plus Services Roads

Figure 7.4 depicts the difference plots for the AM and PM peak modelled flow volumes in the DS L7 scenario to the corresponding DM modelled flow volumes in 2030. The plots show a significant reduction in traffic on the N11 between Junction 6 and 7 as traffic reassigns to the proposed service roads.

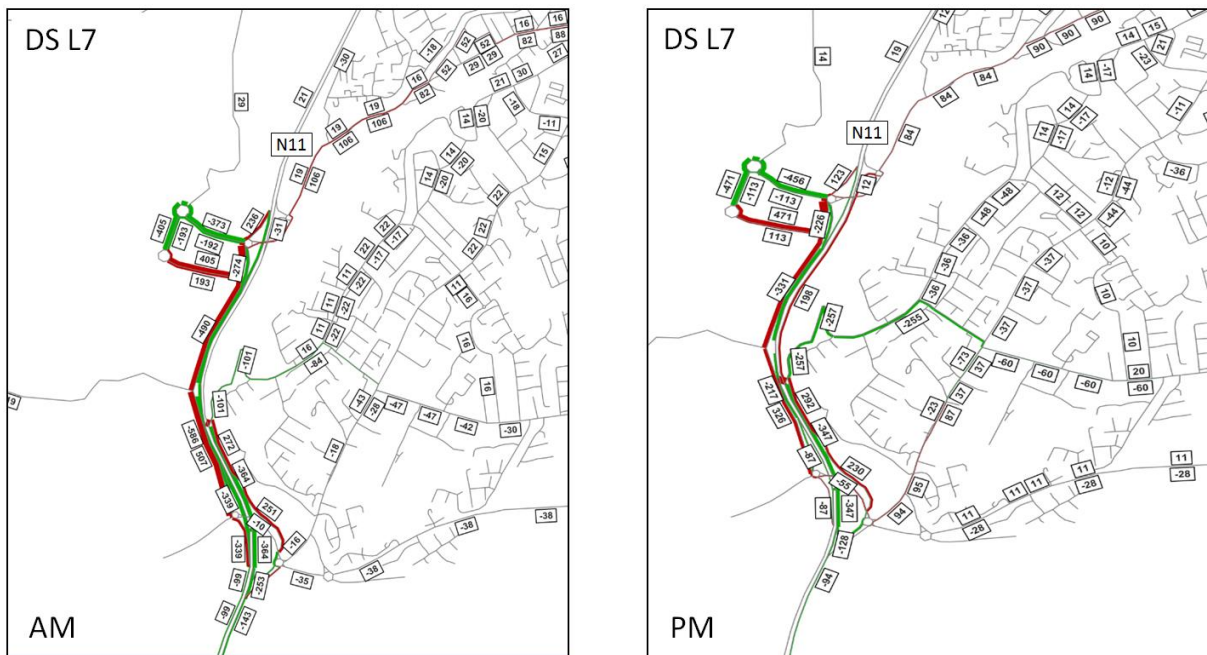


Figure 7.4: DS L7 AM and PM Peak Difference Plots

#### 7.4.1 Network Statistics

Table 7.4 provides a summary of the key network statistics for DS L7 in the AM and PM alongside the 2030 Do-Minimum scenario. The statistics shows that the proposed measures have a slightly negative impact on the performance on the overall network.

Table 7.4: AM & PM Peak Hour Modelled Network Statistics: DS L7

| Scenario      | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|---------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2030 AM DM    | 21,284                | 5,740                   | 16.18                          | 248,432             | 1,333             |
| 2030 AM DS L7 | 21,284                | 5,760                   | 16.24                          | 247,965             | 1,349             |
|               |                       |                         |                                |                     |                   |
| 2030 PM DM    | 21,223                | 5,451                   | 15.41                          | 244,970             | 1,102             |
| 2030 PM DS L7 | 21,223                | 5,462                   | 15.44                          | 245,133             | 1,103             |

7.4.2 Impact on M11/N11 Mainline Flows

Referring to Table C.5 and C.6 (Annex C) DS L7 would significantly reduce traffic volumes on the N11 mainline between Junction 6 and 7 as traffic between the N11 and Herbert Road/Enniskerry Road uses the proposed service roads.

7.4.3 Summary

This proposal resulted in marginal dis-benefits to the overall performance of the network. However, the assessment does not take into account the safety benefits and improved efficiency associated with the proposal. Therefore, it is recommended that this proposal is included as part of the Emerging Preferred Strategy.

**8.0 Conclusions and Recommendations**

This Technical Note considered and examined the performance of a number of proposed measures in isolation against the 2015 Do-Nothing LAMs. The measures which were considered beneficial were then tested against the 2030 Do-Minimum LAMs. Each proposal was assessed by reference to difference plots, network statistics and impact on the M11/N11 mainline corridor. The viability of the options was discussed and recommendations were made regarding the suitability of each option for inclusion in an Emerging Preferred Strategy for the study area.

In Table 8.1 a summary is provided of the measures suitable for inclusion as part of the Emerging Preferred Strategy for the corridor.

Table 8.1: Measures for the Emerging Preferred Strategy

| Scenario | Description   |
|----------|---|
| 1        | 3 lanes plus an auxiliary lane on the M11 between Junction 4 (M50/M11) and Junction 5 (Bray North) and 3 lanes in each direction on the M11/N11 between Junction 5 and Junction 8 (Kilmacanogue).   |
| J6       | Increased capacity (roundabouts and merges/diverges)  |
| J7       | Increased capacity (Dumbbell layout), with southbound lane drop and lane gain south of J7, and northbound lane drop and lane gain north of J7.  |
| L1       | Link road between Herbert Road and Upper Dargle Road. Provides another crossing of the Dargle and allows access to Junction 6 (Bray Central/Fassaroe).  |
| L7       | Junction 6a (West) – Closure of direct access between Enniskerry Road and the N11. Access maintained through one-way northbound service roads between Junction 7 and 6 connecting to Enniskerry Road.<br>Junction 6a (East) - Closure of direct access between Herbert Road and the N11. New additional diverge between J6 and J7 to a southbound segregated one-way service road accessing Halting site, Dargle Lane, Herbert Road and private accesses, which then connects to Ballywaltrim Lane and then to J7 via local road network. |
| J8       | Introduction of single southbound lane drop/service road and single northbound lane gain/service road with associated increase in speed limit of 100km/hr.  |
| AR1      | 1. Improved local roads to the west of M11 between J4 and J6 (Ferndale Road, part of Thornhill Road plus a new link from Thornhill Road as per Fassaroe masterplan).<br>2. New link from M50 J16 (Cherrywood) to Rathmichael/Ballycorus Road (DS L8)  |

## 8.1 Emerging Preferred Strategy

Figure 8.5 depicts the difference plots for the AM and PM peak modelled flow volumes in Emerging Preferred Strategy to the corresponding Do-Minimum modelled flow volumes in 2030.

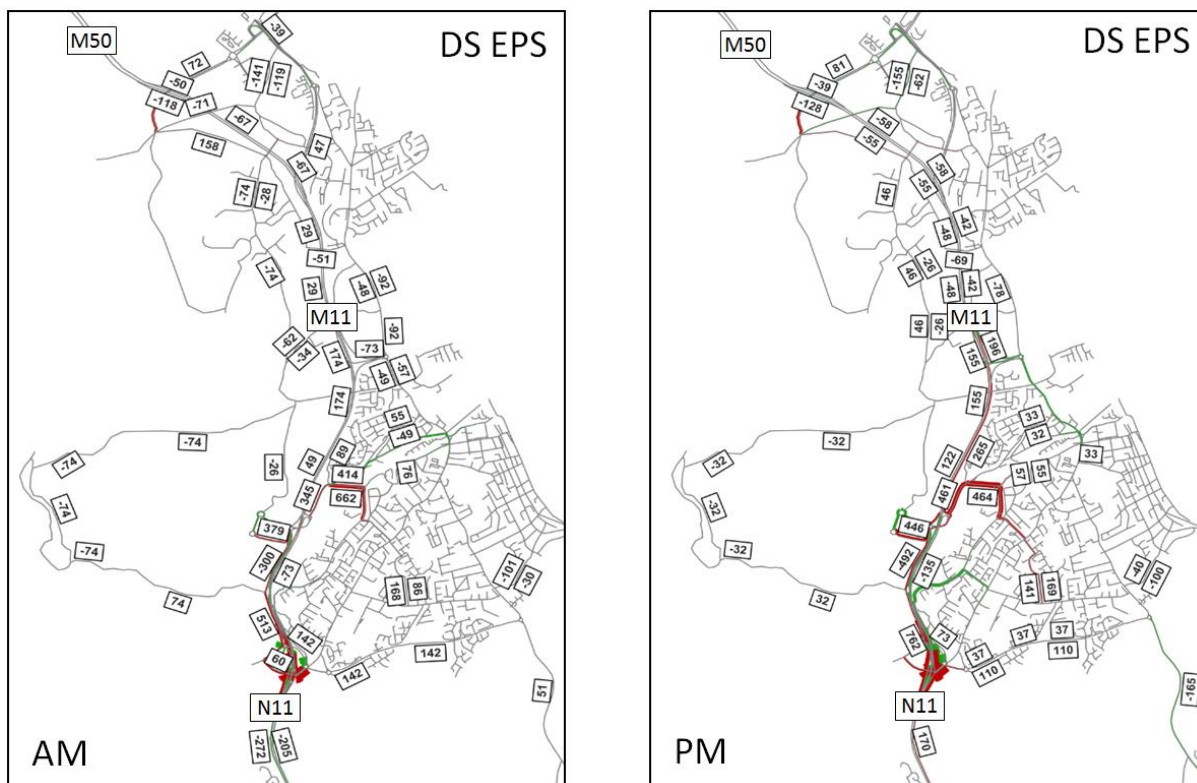


Figure 8.1: Emerging Preferred Strategy AM and PM Peak Difference Plots

8.1.1 Network Statistics

Table 8.2 provides a summary of the key network statistics for the Emerging Preferred Strategy in the AM and PM alongside the 2030 Do-Nothing scenario. The statistics show that the combined elements of the Emerging Preferred Strategy have a significant positive benefits to the overall performance of the network.

Table 8.1: AM & PM Peak Hour Modelled Network Statistics: Emerging Preferred Strategy

| Scenario    | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|-------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| 2030 AM DN  | 21,284                | 6,080                   | 17.14                          | 247,835             | 1,667             |
| 2030 AM EPS | 21,284                | 5,442                   | 15.34                          | 244,156             | 1,107             |
| 2030 PM DN  | 21,223                | 5,693                   | 16.09                          | 244,756             | 1,333             |
| 2030 PM EPS | 21,223                | 5,289                   | 14.95                          | 242,990             | 983               |

8.1.2 Impact on M11/N11 Mainline Flows

Referring to Table C.5 and C.6 (Annex C) the EPS would reduce traffic volumes on the N11 mainline between Junction 6 and 7 as traffic utilise the Herbert Road/Dargle Road link, the service roads between Junctions 6 and 7 and the improved Junction 7.

### 8.1.3 *Summary*

The EPS generates significant benefits to the overall network in both the AM and PM peak as demonstrated by the network statistics. The additional capacity of the mainline corridor combined with improved and more direct access to the regional/local road network through the various proposals, leads to substantial reductions in delay and distance travelled when compared to the 2030 Do-Nothing scenario. Due to the strategic nature of the model, the benefits of the services roads at Kilmacanogue (DS J8) are not included in the above assessment but in practice would add to the overall benefits.



## **ANNEX A**

### **2030/2050 Mainline Flows**

# Technical Note 1

Table A.1: 2030 Do-Something Scenario Mainline - M11/N11 Peak Hour Flows

| Road       | Junction No. | Junction Name                    | No. of Lanes | Northbound AM Peak (08:00 – 09:00) (vehicles/hour) |       | Southbound PM Peak (17:00 – 18:00) (vehicles/hour) |       | Do-Something Practical Capacity (vehicles/hour) |                            |       |
|------------|--------------|----------------------------------|--------------|--|-------|--|-------|---|----------------------------|-------|
|            |              |                                  |              | Demand Flow  |       | Demand Flow  |       | GDA Average                                     | Link Specific <sup>3</sup> |       |
|            |              |                                  |              | DN   | DS 1  | DN   | DS 1  |   | North                      | South |
| <b>M50</b> | 16 – 17      | Cherrywood – M11                 | 2            | 3,390  | 3,394 | 2,968  | 2,970 | 4,600   | 4,600                      | 4,600 |
| <b>M11</b> | 3 – 4        | Loughlinstown – M50              | 2            | 2,021  | 2,017 | 1,617  | 1,617 | 3,400   | 3,400                      | 3,400 |
|            | 4 – 5        | M50/M11 – Bray North             | 3+1          | 5,411  | 5,411 | 4,584  | 4,587 | 6,800   | 8,600                      | 8,600 |
|            | 5 – 6        | Bray North – Bray Central        | 3            | 4,714  | 4,729 | 4,085  | 4,085 | 5,100   | 6,900                      | 5,750 |
| <b>N11</b> | 6 – 6a       | Bray Central – Herbert Road/R117 | 3            | 4,855  | 4,856 | 4,143  | 4,141 | 5,100   | 5,450                      | 5,000 |
|            | 6a – 7       | Herbert Rd/R117 – Bray South     | 3            | 4,866  | 4,867 | 4,054  | 4,057 | 5,100   | 5,450                      | 5,000 |
|            | 7 – 8        | Bray South - Kilmacanogue        | 3            | 3,978  | 3,984 | 3,564  | 3,556 | 5,100   | 5,450                      | 5,000 |
|            | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 3,270  | 3,274 | 3,103  | 3,094 | 3,400   | 3,550                      | 3,550 |
|            | 9 – 10       | Glen of the Downs - Delgany      | 2            | 3,232  | 3,237 | 3,068  | 3,059 | 3,400   | 3,550                      | 3,550 |
|            | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 2,796  | 2,797 | 2,888  | 2,888 | 3,400   | 3,550                      | 3,550 |
|            | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 2,653  | 2,653 | 2,679  | 2,679 | 3,400   | 3,550                      | 3,550 |
|            | 12 – 13      | Newtown MK - Newcastle           | 2            | 2,040  | 2,040 | 2,160  | 2,159 | 3,400   | 3,550                      | 3,550 |
|            | 13 – 14      | Newcastle – Coyne’s Cross        | 2            | 2,125  | 2,125 | 2,366  | 2,365 | 3,400   | 3,550                      | 3,550 |
| <b>M11</b> | 14 – 15      | Coyne’s Cross - Ashford          | 2            | 2,227  | 2,227 | 2,465  | 2,464 | 3,400   | 4,600                      | 4,600 |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

<sup>3</sup> Lower southbound practical capacity due to gradient issue between Junctions 6a & 7 only. (Closure of Junction 6a and improvements at Junction 8 address previous shortcomings.)

# Technical Note 1

Table A.2: 2050 Do-Something Scenario Mainline - M11/N11 Peak Hour Flows

| Road | Junction No. | Junction Name                    | No. of Lanes | Northbound AM Peak (08:00 – 09:00) (vehicles/hour) |       | Southbound PM Peak (17:00 – 18:00) (vehicles/hour) |       | Do-Something Practical Capacity (vehicles/hour) |                            |       |
|------|--------------|----------------------------------|--------------|--|-------|--|-------|---|----------------------------|-------|
|      |              |                                  |              | Demand Flow  |       | Demand Flow  |       | GDA Average                                     | Link Specific <sup>4</sup> |       |
|      |              |                                  |              | DN   | DS 1  | DN   | DS 1  |   | North                      | South |
| M50  | 16 – 17      | Cherrywood – M11                 | 2            | 3,678  | 3,696 | 3,218  | 3,255 | 4,600   | 4,600                      | 4,600 |
| M11  | 3 – 4        | Loughlinstown – M50              | 2            | 2,168  | 2,042 | 1,693  | 1,795 | 3,400   | 3,400                      | 3,400 |
|      | 4 – 5        | M50/M11 – Bray North             | 3+1          | 5,846  | 5,738 | 4,910  | 5,050 | 6,800   | 8,600                      | 8,600 |
|      | 5 – 6        | Bray North – Bray Central        | 3            | 5,013  | 5,096 | 4,300  | 4,333 | 5,100   | 6,900                      | 5,750 |
| N11  | 6 – 6a       | Bray Central – Herbert Road/R117 | 3            | 5,038  | 5,308 | 4,468  | 4,640 | 5,100   | 5,450                      | 5,000 |
|      | 6a – 7       | Herbert Rd/R117 – Bray South     | 3            | 5,077  | 5,389 | 4,379  | 4,066 | 5,100   | 5,450                      | 5,000 |
|      | 7 – 8        | Bray South - Kilmacanogue        | 3            | 3,959  | 4,506 | 3,811  | 3,776 | 5,100   | 5,450                      | 5,000 |
|      | 8 – 9        | Kilmacanogue – Glen of the Downs | 2            | 3,326  | 3,543 | 3,292  | 3,255 | 3,400   | 3,550                      | 3,550 |
|      | 9 – 10       | Glen of the Downs - Delgany      | 2            | 3,273  | 3,503 | 3,255  | 3,221 | 3,400   | 3,550                      | 3,550 |
|      | 10 – 11      | Delgany – Greystones (Kilpedder) | 2            | 2,915  | 2,967 | 3,089  | 3,074 | 3,400   | 3,550                      | 3,550 |
|      | 11 – 12      | Greystones (Kilpedder)–Newtown   | 2            | 2,785  | 2,808 | 2,844  | 2,832 | 3,400   | 3,550                      | 3,550 |
|      | 12 – 13      | Newtown MK - Newcastle           | 2            | 2,084  | 2,095 | 2,261  | 2,259 | 3,400   | 3,550                      | 3,550 |
|      | 13 – 14      | Newcastle – Coyne’s Cross        | 2            | 2,209  | 2,210 | 2,488  | 2,488 | 3,400   | 3,550                      | 3,550 |
| M11  | 14 – 15      | Coyne’s Cross - Ashford          | 2            | 2,319  | 2,320 | 2,585  | 2,585 | 3,400   | 4,600                      | 4,600 |

Figures highlighted in red indicate that the section is operating at or above 95% of the link specific practical capacity in the peak hour

<sup>4</sup> Lower southbound practical capacity due to gradient issue between Junctions 6a & 7 only. (Closure of Junction 6a and improvements at Junction 8 address previous shortcomings.)

## **ANNEX B**

### **Network Statistics**

**ANNEX B: Network Statistics**

Table B.1 presents the modelled network statistics for the AM and PM peak hour in relation to the DS 2015 scenarios for junction upgrades. The corresponding 2015 AM and PM peak Do-Nothing Base Year (BY) scenario is also shown for comparison purposes.

*Table B.1: AM & Peak Hour Modelled Network Statistics (Do Something Scenarios - Junctions - 2015)*

| Scenario          | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|-------------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| <b>2015 AM DN</b> | <b>17,721</b>         | <b>4,648</b>            | <b>15.74</b>                   | <b>201,602</b>      | <b>997</b>        |
| 2015 AM DS J5a    | 17,721                | 4,655                   | 15.76                          | 201,565             | 1,001             |
| 2015 AM DS J5b    | 17,721                | 4,655                   | 15.76                          | 201,816             | 1,001             |
| 2015 AM DS J6     | 17,721                | 4,643                   | 15.72                          | 201,581             | 992               |
| 2015 AM DS J7     | 17,721                | 4,545                   | 15.39                          | 200,234             | 921               |
| <b>2015 PM DN</b> | <b>17,706</b>         | <b>4,445</b>            | <b>15.06</b>                   | <b>200,448</b>      | <b>807</b>        |
| 2015 PM DS J5a    | 17,706                | 4,447                   | 15.07                          | 200,571             | 806               |
| 2015 PM DS J5b    | 17,706                | 4,449                   | 15.08                          | 200,754             | 808               |
| 2015 PM DS J6     | 17,706                | 4,442                   | 15.05                          | 200,469             | 805               |
| 2015 PM DS J7     | 17,706                | 4,379                   | 14.84                          | 200,008             | 762               |

Table B.2 presents the modelled network statistics for the AM and PM peak periods in the 2015 DS scenarios for the regional and local road options. The corresponding 2015 AM and PM peak Do-Nothing scenario is also shown for comparison purposes.

*Table B.2: AM & PM Peak Hour Modelled Network Statistics (DS Scenarios – Regional/Local Roads Options - 2015)*

| Scenario          | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|-------------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| <b>2015 AM DN</b> | <b>17,721</b>         | <b>4,648</b>            | <b>15.74</b>                   | <b>201,602</b>      | <b>997</b>        |
| 2015 AM DSL1      | 17,721                | 4,502                   | 15.24                          | 200,092             | 877               |
| 2015 AM DSL2      | 17,721                | 4,494                   | 15.22                          | 199,093             | 884               |
| 2015 AM DSL3      | 17,721                | 4,636                   | 15.70                          | 201,548             | 985               |
| 2015 AM DSL4      | 17,721                | 4,578                   | 15.50                          | 201,808             | 924               |
| 2015 AM DSL5      | 17,721                | 4,563                   | 15.45                          | 201,772             | 907               |
| 2015 AM DSL6      | 17,721                | 4,667                   | 15.80                          | 201,558             | 1,014             |
| 2015 AM DSL7      | 17,721                | 4,665                   | 15.80                          | 201,411             | 1,005             |
| 2015 AM DSL8      | 17,721                | 4,619                   | 15.64                          | 200,879             | 984               |
| <b>2015 PM DN</b> |                       |                         |                                |                     |                   |
| <b>2015 PM DN</b> | <b>17,706</b>         | <b>4,445</b>            | <b>15.06</b>                   | <b>200,448</b>      | <b>807</b>        |
| 2015 PM DSL1      | 17,706                | 4,391                   | 14.88                          | 199,969             | 762               |
| 2015 PM DSL2      | 17,706                | 4,412                   | 14.95                          | 200,068             | 791               |
| 2015 PM DSL3      | 17,706                | 4,444                   | 15.06                          | 200,450             | 806               |
| 2015 PM DSL4      | 17,706                | 4,394                   | 14.89                          | 199,752             | 772               |
| 2015 PM DSL5      | 17,706                | 4,411                   | 14.95                          | 200,741             | 769               |
| 2015 PM DSL6      | 17,706                | 4,528                   | 15.35                          | 200,953             | 875               |
| 2015 PM DSL7      | 17,706                | 4,451                   | 15.08                          | 200,909             | 797               |
| 2015 PM DSL8      | 17,706                | 4,420                   | 14.98                          | 199,803             | 794               |

Table B.3 presents the modelled network statistics for the AM and PM peak periods in the 2030 DS scenarios for junctions, as well as the regional and local road options. The corresponding 2030 AM and PM peak Do-Minimum scenario is also shown for comparison purposes.

*Table B.3: AM & PM Peak Hour Modelled Network Statistics (DS Scenarios – Junctions, Regional/Local Roads Options and Emerging Preferred Strategy - 2030)*

| Scenario          | Total Trips (Vehs/hr) | Total Travel Time (hrs) | Travel Time per Vehicle (mins) | Total Distance (km) | Total Delay (hrs) |
|-------------------|-----------------------|-------------------------|--------------------------------|---------------------|-------------------|
| <b>2030 AM DN</b> | <b>21,284</b>         | <b>6,080</b>            | <b>17.14</b>                   | <b>247,835</b>      | <b>1,667</b>      |
| 2030 AM DS J7     | 21,284                | 5,548                   | 15.64                          | 246,480             | 1,180             |
| 2030 AM DSL1      | 21,284                | 5,603                   | 15.79                          | 246,172             | 1,233             |
| 2030 AM DSL4      | 21,284                | 5,709                   | 16.09                          | 248,250             | 1,303             |
| 2030 AM DS L7     | 21,284                | 5,760                   | 16.24                          | 247,965             | 1,349             |
| 2030 AM DS EPS    | 21,284                | 5,442                   | 15.34                          | 244,156             | 1,107             |
|                   |                       |                         |                                |                     |                   |
| <b>2030 PM DN</b> | <b>21,223</b>         | <b>5,693</b>            | <b>16.09</b>                   | <b>244,756</b>      | <b>1,333</b>      |
| 2030 PM DS J7     | 21,223                | 5,380                   | 15.21                          | 244,591             | 1,049             |
| 2030 PM DSL1      | 21,223                | 5,389                   | 15.23                          | 244,495             | 1,051             |
| 2030 PM DSL4      | 21,223                | 5,404                   | 15.28                          | 244,327             | 1,067             |
| 2030 PM DS L7     | 21,223                | 5,462                   | 15.44                          | 245,133             | 1,103             |
| 2030 PM EPS       | 21,223                | 5,289                   | 14.95                          | 242,990             | 983               |

## **ANNEX C**

# **Impact of DS Scenarios upon N11/M11 Mainline Flows - 2015 and 2030**



**ANNEX C: IMPACT OF DO-SOMETHING SCENARIOS ON MAINLINE FLOWS - 2015**

Table C.1: 2015 Do-Something Scenarios (Junctions) M11/N11 Northbound Peak Hour Flows (vehicles)

| Road | Junction No. | Junction Name                       | No. of Lanes | AM Peak (08:00 – 09:00) |        |        |       |       | PM Peak (17:00 – 18:00) |        |        |       |       |
|------|--------------|-------------------------------------|--------------|-------------------------|--------|--------|-------|-------|-------------------------|--------|--------|-------|-------|
|      |              |                                     |              | Flow (vehs/hr)          |        |        |       |       | Flow (vehs/hr)          |        |        |       |       |
|      |              |                                     |              | DN                      | DS J5a | DS J5b | DS J6 | DS J7 | DN                      | DS J5a | DS J5b | DS J6 | DS J7 |
| M50  | 16 - 17      | Cherrywood - M11                    | 2            | 2776                    | 2716   | 2739   | 2776  | 2774  | 1547                    | 1519   | 1519   | 1547  | 1544  |
| M11  | 3 - 4        | Loughlinstown - M50                 | 2            | 1800                    | 1774   | 1884   | 1800  | 1805  | 888                     | 821    | 902    | 887   | 891   |
|      | 4 - 5        | M50/M11 - Bray North                | 2+1          | 4576                    | 4491   | 4622   | 4576  | 4580  | 2434                    | 2340   | 2422   | 2435  | 2435  |
|      | 5 - 6        | Bray North - Bray Central           | 2            | 4160                    | 4130   | 4083   | 4164  | 4197  | 2028                    | 2075   | 2042   | 2028  | 2066  |
| N11  | 6 - 6a       | Bray Central - Herbert Rd/R117      | 2            | 4027                    | 4031   | 4028   | 4022  | 4129  | 2285                    | 2306   | 2288   | 2293  | 2267  |
|      | 6a - 7       | Herbert Rd/R117 - Bray South        | 2            | 4089                    | 4082   | 4086   | 4081  | 4228  | 2201                    | 2220   | 2204   | 2209  | 2208  |
|      | 7 - 8        | Bray South - Kilmacanogue           | 2            | 3159                    | 3159   | 3159   | 3144  | 2874  | 1529                    | 1534   | 1526   | 1530  | 1540  |
|      | 8 - 9        | Kilmacanogue - Glen of the Downs    | 2            | 2452                    | 2467   | 2468   | 2457  | 2411  | 1335                    | 1340   | 1332   | 1336  | 1341  |
|      | 9 - 10       | Glen of the Downs - Delgany         | 2            | 2419                    | 2434   | 2435   | 2424  | 2378  | 1293                    | 1298   | 1290   | 1294  | 1300  |
|      | 10 - 11      | Delgany - Greystones (Kilpedder)    | 2            | 2158                    | 2167   | 2156   | 2161  | 2156  | 1133                    | 1133   | 1134   | 1134  | 1137  |
|      | 11 - 12      | Greystones (Kilpedder) - Newtown MK | 2            | 2034                    | 2037   | 2033   | 2035  | 2032  | 1248                    | 1248   | 1248   | 1248  | 1248  |
|      | 12 - 13      | Newtown MK - Newcastle              | 2            | 1629                    | 1630   | 1630   | 1629  | 1630  | 1003                    | 1003   | 1003   | 1003  | 1003  |
|      | 13 - 14      | Newcastle - Coynes Cross            | 2            | 1711                    | 1711   | 1711   | 1711  | 1711  | 1027                    | 1027   | 1027   | 1027  | 1027  |
| M11  | 14 - 15      | Coynes Cross - Ashford              | 2            | 1698                    | 1698   | 1698   | 1698  | 1698  | 1024                    | 1024   | 1024   | 1024  | 1024  |

Figures highlighted in red indicate that the section is operating at or above 95% of the practical capacity in the peak hour

**ANNEX C: IMPACT OF DO-SOMETHING SCENARIOS ON M11/N11 MAINLINE FLOWS - 2015**

Table C.2: 2015 Do-Something Scenarios (Junctions) M11/N11 Southbound Peak Hour Flows (vehicles)

| Road | Junction No. | Junction Name                       | No. of Lanes | AM Peak (08:00 – 09:00) |        |        |       |       | PM Peak (17:00 – 18:00) |        |        |       |       |
|------|--------------|-------------------------------------|--------------|-------------------------|--------|--------|-------|-------|-------------------------|--------|--------|-------|-------|
|      |              |                                     |              | Flow (vehs/hr)          |        |        |       |       | Flow (vehs/hr)          |        |        |       |       |
|      |              |                                     |              | DN                      | DS J5a | DS J5b | DS J6 | DS J7 | DN                      | DS J5a | DS J5b | DS J6 | DS J7 |
| M50  | 16 - 17      | Cherrywood - M11                    | 2            | 1346                    | 1347   | 1346   | 1346  | 1345  | 2337                    | 2331   | 2337   | 2337  | 2337  |
| M11  | 3 - 4        | Loughlinstown - M50                 | 2            | 792                     | 795    | 795    | 792   | 793   | 1397                    | 1405   | 1407   | 1397  | 1397  |
|      | 4 - 5        | M50/M11 - Bray North                | 2+1          | 2138                    | 2142   | 2141   | 2138  | 2138  | 3734                    | 3737   | 3744   | 3734  | 3734  |
|      | 5 - 6        | Bray North - Bray Central           | 2            | 1703                    | 1773   | 1769   | 1704  | 1735  | 3371                    | 3393   | 3388   | 3343  | 3406  |
| N11  | 6 - 6a       | Bray Central - Herbert Rd/R117      | 2            | 2069                    | 2071   | 2071   | 2068  | 2116  | 3666                    | 3665   | 3663   | 3673  | 3651  |
|      | 6a - 7       | Herbert Rd/R117 - Bray South        | 2            | 2071                    | 2058   | 2062   | 2053  | 2130  | 3531                    | 3532   | 3529   | 3533  | 3379  |
|      | 7 - 8        | Bray South - Kilmacanogue           | 2            | 1623                    | 1611   | 1610   | 1604  | 1394  | 2807                    | 2807   | 2808   | 2808  | 2914  |
|      | 8 - 9        | Kilmacanogue - Glen of the Downs    | 2            | 1226                    | 1229   | 1230   | 1228  | 1241  | 2449                    | 2449   | 2450   | 2449  | 2552  |
|      | 9 - 10       | Glen of the Downs - Delgany         | 2            | 1189                    | 1192   | 1192   | 1190  | 1203  | 2415                    | 2416   | 2416   | 2416  | 2518  |
|      | 10 - 11      | Delgany - Greystones (Kilpedder)    | 2            | 1049                    | 1050   | 1049   | 1050  | 1060  | 2320                    | 2320   | 2320   | 2320  | 2321  |
|      | 11 - 12      | Greystones (Kilpedder) - Newtown MK | 2            | 1113                    | 1114   | 1113   | 1113  | 1115  | 2121                    | 2121   | 2121   | 2121  | 2125  |
|      | 12 - 13      | Newtown MK - Newcastle              | 2            | 907                     | 907    | 907    | 907   | 908   | 1706                    | 1706   | 1706   | 1706  | 1710  |
|      | 13 - 14      | Newcastle - Coynes Cross            | 2            | 936                     | 936    | 936    | 936   | 936   | 1828                    | 1828   | 1828   | 1828  | 1827  |
| M11  | 14 - 15      | Coynes Cross - Ashford              | 2            | 976                     | 976    | 976    | 976   | 976   | 1917                    | 1917   | 1917   | 1917  | 1916  |

Figures highlighted in red indicate that the section is operating at or above 95% of the practical capacity in the peak hour

**ANNEX C: IMPACT OF DO-SOMETHING SCENARIOS ON MAINLINE FLOWS - 2015**

Table C.3: 2015 Do-Something Scenarios (Regional/Local Road Options) M11/N11 Northbound Peak Hour Flows (vehicles)

| Road | Junction No. | Junction Name                       | No. of Lanes | AM Peak (08:00 – 09:00) |       |       |       |       |       |       |       |       | PM Peak (17:00 – 18:00) |       |       |       |       |       |       |       |       |
|------|--------------|-------------------------------------|--------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
|      |              |                                     |              | Flow (vehs/hr)          |       |       |       |       |       |       |       |       | Flow (vehs/hr)          |       |       |       |       |       |       |       |       |
|      |              |                                     |              | DN                      | DS L1 | DS L2 | DS L3 | DS L4 | DS L5 | DS L6 | DS L7 | DS L8 | DN                      | DS L1 | DS L2 | DS L3 | DS L4 | DS L5 | DS L6 | DS L7 | DS L8 |
| M50  | 16 - 17      | Cherrywood - M11                    | 2            | 2776                    | 2773  | 2776  | 2774  | 2775  | 2776  | 2776  | 2814  | 2774  | 1547                    | 1550  | 1547  | 1545  | 1550  | 1547  | 1545  | 1476  | 1546  |
| M11  | 3 - 4        | Loughlinstown - M50                 | 2            | 1800                    | 1797  | 1800  | 1804  | 1804  | 1799  | 1800  | 1813  | 1794  | 888                     | 888   | 887   | 892   | 886   | 888   | 892   | 917   | 887   |
|      | 4 - 5        | M50/M11 - Bray North                | 2+1          | 4576                    | 4570  | 4576  | 4578  | 4579  | 4576  | 4577  | 4627  | 4568  | 2434                    | 2438  | 2435  | 2437  | 2436  | 2435  | 2436  | 2393  | 2433  |
|      | 5 - 6        | Bray North - Bray Central           | 2            | 4160                    | 4214  | 4162  | 4192  | 4200  | 4158  | 4152  | 4159  | 4197  | 2028                    | 2086  | 2028  | 2024  | 2037  | 2001  | 2015  | 2027  | 2102  |
| N11  | 6 - 6a       | Bray Central - Herbert Rd/R117      | 2            | 4027                    | 4179  | 4043  | 4050  | 4051  | 4026  | 3502  | 4027  | 3821  | 2285                    | 2206  | 2285  | 2223  | 2301  | 2384  | 2190  | 2285  | 2119  |
|      | 6a - 7       | Herbert Rd/R117 - Bray South        | 2            | 4089                    | 3641  | 4067  | 4115  | 4112  | 4088  | 3502  | 4086  | 3884  | 2201                    | 2148  | 2196  | 2139  | 2216  | 2296  | 2190  | 2200  | 2035  |
|      | 7 - 8        | Bray South - Kilmacanogue           | 2            | 3159                    | 2869  | 3140  | 3048  | 3233  | 3147  | 3098  | 3156  | 3036  | 1529                    | 1538  | 1530  | 1419  | 1595  | 1523  | 1526  | 1529  | 1531  |
|      | 8 - 9        | Kilmacanogue - Glen of the Downs    | 2            | 2452                    | 2406  | 2445  | 2461  | 2565  | 2456  | 2479  | 2452  | 2443  | 1335                    | 1344  | 1335  | 1337  | 1404  | 1330  | 1333  | 1334  | 1333  |
|      | 9 - 10       | Glen of the Downs - Delgany         | 2            | 2419                    | 2372  | 2412  | 2428  | 2321  | 2423  | 2446  | 2419  | 2409  | 1293                    | 1303  | 1293  | 1296  | 1276  | 1290  | 1293  | 1293  | 1291  |
|      | 10 - 11      | Delgany - Greystones (Kilpedder)    | 2            | 2158                    | 2165  | 2158  | 2158  | 2151  | 2154  | 2165  | 2158  | 2179  | 1133                    | 1135  | 1133  | 1135  | 1135  | 1131  | 1132  | 1133  | 1136  |
|      | 11 - 12      | Greystones (Kilpedder) - Newtown MK | 2            | 2034                    | 2034  | 2034  | 2034  | 2028  | 2033  | 2037  | 2034  | 2039  | 1248                    | 1249  | 1248  | 1248  | 1248  | 1245  | 1247  | 1248  | 1248  |
|      | 12 - 13      | Newtown MK - Newcastle              | 2            | 1629                    | 1631  | 1629  | 1631  | 1630  | 1629  | 1629  | 1629  | 1631  | 1003                    | 1004  | 1003  | 1003  | 1004  | 1003  | 1003  | 1003  | 1003  |
|      | 13 - 14      | Newcastle - Coynes Cross            | 2            | 1711                    | 1711  | 1711  | 1711  | 1711  | 1711  | 1711  | 1711  | 1711  | 1027                    | 1028  | 1027  | 1027  | 1028  | 1027  | 1027  | 1027  | 1027  |
| M11  | 14 - 15      | Coynes Cross - Ashford              | 2            | 1698                    | 1698  | 1698  | 1698  | 1698  | 1698  | 1698  | 1698  | 1698  | 1024                    | 1024  | 1024  | 1024  | 1024  | 1024  | 1024  | 1024  | 1024  |

Figures highlighted in red indicate that the section is operating at or above 95% of the practical capacity in the peak hour

**ANNEX C: IMPACT OF DO-SOMETHING SCENARIOS ON MAINLINE FLOWS - 2015**

Table C.4: 2015 Do-Something Scenarios (Regional/Local Road Options) M11/N11 Southbound Peak Hour Flows (vehicles)

| Road | Junction No. | Junction Name                       | No. of Lanes | AM Peak (08:00 – 09:00) |       |       |       |       |       |       |       |       | PM Peak (17:00 – 18:00) |       |       |       |       |       |       |       |       |
|------|--------------|-------------------------------------|--------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
|      |              |                                     |              | Flow (vehs/hr)          |       |       |       |       |       |       |       |       | Flow (vehs/hr)          |       |       |       |       |       |       |       |       |
|      |              |                                     |              | DN                      | DS L1 | DS L2 | DS L3 | DS L4 | DS L5 | DS L6 | DS L7 | DS L8 | DN                      | DS L1 | DS L2 | DS L3 | DS L4 | DS L5 | DS L6 | DS L7 | DS L8 |
| M50  | 16 - 17      | Cherrywood - M11                    | 2            | 1346                    | 1344  | 1346  | 1344  | 1345  | 1346  | 1346  | 1343  | 1344  | 2337                    | 2337  | 2337  | 2337  | 2337  | 2337  | 2337  | 2291  | 2337  |
| M11  | 3 - 4        | Loughlinstown - M50                 | 2            | 792                     | 793   | 793   | 792   | 792   | 792   | 792   | 790   | 793   | 1397                    | 1397  | 1397  | 1397  | 1397  | 1397  | 1397  | 1413  | 1397  |
|      | 4 - 5        | M50/M11 - Bray North                | 2+1          | 2138                    | 2137  | 2139  | 2137  | 2137  | 2138  | 2138  | 2134  | 2137  | 3734                    | 3734  | 3734  | 3734  | 3734  | 3733  | 3734  | 3704  | 3734  |
|      | 5 - 6        | Bray North - Bray Central           | 2            | 1703                    | 1706  | 1711  | 1705  | 1760  | 1604  | 1694  | 1702  | 1737  | 3371                    | 3410  | 3371  | 3378  | 3393  | 3282  | 3401  | 3372  | 3447  |
| N11  | 6 - 6a       | Bray Central - Herbert Rd/R117      | 2            | 2069                    | 2046  | 2040  | 2072  | 2122  | 1957  | 1744  | 2066  | 1897  | 3666                    | 3584  | 3662  | 3614  | 3692  | 3730  | 3128  | 3665  | 3424  |
|      | 6a - 7       | Herbert Rd/R117 - Bray South        | 2            | 2071                    | 1750  | 2045  | 2031  | 2107  | 2240  | 1744  | 2068  | 1941  | 3531                    | 3556  | 3527  | 3325  | 3560  | 3730  | 3128  | 3530  | 3444  |
|      | 7 - 8        | Bray South - Kilmacanogue           | 2            | 1623                    | 1391  | 1612  | 1491  | 1647  | 1611  | 1520  | 1620  | 1519  | 2807                    | 2874  | 2807  | 2512  | 2888  | 2724  | 2742  | 2807  | 2811  |
|      | 8 - 9        | Kilmacanogue - Glen of the Downs    | 2            | 1226                    | 1238  | 1227  | 1242  | 1289  | 1230  | 1211  | 1227  | 1235  | 2449                    | 2517  | 2449  | 2555  | 2529  | 2368  | 2385  | 2449  | 2449  |
|      | 9 - 10       | Glen of the Downs - Delgany         | 2            | 1189                    | 1200  | 1190  | 1205  | 1162  | 1193  | 1174  | 1189  | 1198  | 2415                    | 2484  | 2415  | 2521  | 2327  | 2336  | 2353  | 2415  | 2415  |
|      | 10 - 11      | Delgany - Greystones (Kilpedder)    | 2            | 1049                    | 1061  | 1049  | 1052  | 1064  | 1050  | 1043  | 1049  | 1061  | 2320                    | 2317  | 2320  | 2327  | 2312  | 2295  | 2300  | 2320  | 2324  |
|      | 11 - 12      | Greystones (Kilpedder) - Newtown MK | 2            | 1113                    | 1115  | 1113  | 1115  | 1115  | 1113  | 1112  | 1113  | 1115  | 2121                    | 2121  | 2121  | 2125  | 2121  | 2119  | 2119  | 2121  | 2122  |
|      | 12 - 13      | Newtown MK - Newcastle              | 2            | 907                     | 909   | 907   | 909   | 909   | 907   | 906   | 907   | 909   | 1706                    | 1707  | 1706  | 1710  | 1706  | 1704  | 1705  | 1706  | 1708  |
|      | 13 - 14      | Newcastle - Coynes Cross            | 2            | 936                     | 937   | 936   | 937   | 936   | 936   | 936   | 936   | 937   | 1828                    | 1828  | 1828  | 1827  | 1828  | 1829  | 1828  | 1828  | 1827  |
| M11  | 14 - 15      | Coynes Cross - Ashford              | 2            | 976                     | 976   | 976   | 976   | 976   | 976   | 976   | 976   | 976   | 1917                    | 1917  | 1917  | 1916  | 1917  | 1918  | 1917  | 1917  | 1917  |

Figures highlighted in red indicate that the section is operating at or above 95% of the practical capacity in the peak hour

**ANNEX C: IMPACT OF DO-SOMETHING SCENARIOS ON MAINLINE FLOWS - 2030**

Table C.5: 2030 Do-Something Scenarios (Junctions and Regional/Local Road Options) M11/N11 Northbound Peak Hour Flows (vehicles)

| Road | Junction No. | Junction Name                       | No. of Lanes (With Widening) | AM Peak (08:00 – 09:00) |       |       |       |       |        | PM Peak (17:00 – 18:00) |       |       |       |       |        |
|------|--------------|-------------------------------------|------------------------------|-------------------------|-------|-------|-------|-------|--------|-------------------------|-------|-------|-------|-------|--------|
|      |              |                                     |                              | Flow (vehs/hr)          |       |       |       |       |        | Flow (vehs/hr)          |       |       |       |       |        |
|      |              |                                     |                              | DM                      | DS L7 | DS J7 | DS L1 | DS L4 | DS EPS | DM                      | DS L7 | DS J7 | DS L1 | DS L4 | DS EPS |
| M50  | 16 - 17      | Cherrywood - M11                    | 2                            | 3406                    | 3406  | 3406  | 3403  | 3406  | 3376   | 1902                    | 1901  | 1901  | 1902  | 1901  | 1847   |
| M11  | 3 - 4        | Loughlinstown - M50                 | 2                            | 2043                    | 2042  | 2050  | 2038  | 2044  | 2078   | 1017                    | 1017  | 1017  | 1014  | 1018  | 1022   |
|      | 4 - 5        | M50/M11 - Bray North                | 3+1                          | 5449                    | 5448  | 5457  | 5440  | 5449  | 5454   | 2918                    | 2918  | 2919  | 2916  | 2920  | 2869   |
|      | 5 - 6        | Bray North - Bray Central           | 3                            | 5147                    | 5167  | 5172  | 5136  | 5148  | 5162   | 2477                    | 2496  | 2517  | 2585  | 2483  | 2591   |
| N11  | 6 - 6a       | Bray Central - Herbert Rd/R117      | 3                            | 4969                    | 4480  | 5186  | 4773  | 4991  | 4467   | 2693                    | 2362  | 2703  | 2504  | 2625  | 2172   |
|      | 6a - 7       | Herbert Rd/R117 - Bray South        | 3                            | 5066                    | 4480  | 5346  | 4886  | 5094  | 4467   | 2579                    | 2362  | 2615  | 2390  | 2512  | 2172   |
|      | 7 - 8        | Bray South - Kilmacanogue           | 3                            | 4177                    | 4079  | 3717  | 3943  | 3994  | 3749   | 1891                    | 1889  | 1904  | 1898  | 1771  | 1909   |
|      | 8 - 9        | Kilmacanogue - Glen of the Downs    | 2                            | 3264                    | 3288  | 3142  | 3196  | 3248  | 3173   | 1676                    | 1680  | 1688  | 1682  | 1686  | 1693   |
|      | 9 - 10       | Glen of the Downs - Delgany         | 2                            | 3227                    | 3250  | 3105  | 3158  | 3211  | 3136   | 1634                    | 1640  | 1646  | 1641  | 1644  | 1652   |
|      | 10 - 11      | Delgany - Greystones (Kilpedder)    | 2                            | 2828                    | 2834  | 2829  | 2834  | 2826  | 2837   | 1471                    | 1472  | 1474  | 1474  | 1474  | 1479   |
|      | 11 - 12      | Greystones (Kilpedder) - Newtown MK | 2                            | 2663                    | 2666  | 2661  | 2663  | 2661  | 2667   | 1637                    | 1637  | 1638  | 1638  | 1638  | 1640   |
|      | 12 - 13      | Newtown MK - Newcastle              | 2                            | 2056                    | 2056  | 2057  | 2056  | 2056  | 2058   | 1211                    | 1211  | 1211  | 1211  | 1211  | 1213   |
|      | 13 - 14      | Newcastle - Coynes Cross            | 2                            | 2176                    | 2176  | 2179  | 2176  | 2176  | 2179   | 1225                    | 1225  | 1225  | 1225  | 1225  | 1225   |
| M11  | 14 - 15      | Coynes Cross - Ashford              | 2                            | 2240                    | 2240  | 2241  | 2240  | 2240  | 2241   | 1233                    | 1233  | 1233  | 1233  | 1233  | 1233   |

**ANNEX C: IMPACT OF DO-SOMETHING SCENARIOS ON MAINLINE FLOWS - 2030**

Table C.6: 2030 Do-Something Scenarios (Junctions and Regional/Local Road Options) M11/N11 Southbound Peak Hour Flows (vehicles)

| Road | Junction No. | Junction Name                       | No. of Lanes (With Widening) | AM Peak (08:00 – 09:00) |       |       |       |       |        | PM Peak (17:00 – 18:00) |       |       |       |       |        |
|------|--------------|-------------------------------------|------------------------------|-------------------------|-------|-------|-------|-------|--------|-------------------------|-------|-------|-------|-------|--------|
|      |              |                                     |                              | Flow (vehs/hr)          |       |       |       |       |        | Flow (vehs/hr)          |       |       |       |       |        |
|      |              |                                     |                              | DM                      | DS L7 | DS J7 | DS L1 | DS L4 | DS EPS | DM                      | DS L7 | DS J7 | DS L1 | DS L4 | DS EPS |
| M50  | 16 - 17      | Cherrywood - M11                    | 2                            | 1828                    | 1828  | 1828  | 1826  | 1828  | 1740   | 2996                    | 2996  | 2996  | 2996  | 2996  | 2926   |
| M11  | 3 - 4        | Loughlinstown - M50                 | 2                            | 913                     | 910   | 931   | 919   | 915   | 973    | 1625                    | 1624  | 1624  | 1625  | 1624  | 1646   |
|      | 4 - 5        | M50/M11 - Bray North                | 3+1                          | 2741                    | 2738  | 2759  | 2745  | 2743  | 2714   | 4621                    | 4621  | 4621  | 4621  | 4621  | 4572   |
|      | 5 - 6        | Bray North - Bray Central           | 3                            | 2261                    | 2230  | 2289  | 2283  | 2264  | 2295   | 4284                    | 4296  | 4332  | 4402  | 4297  | 4423   |
| N11  | 6 - 6a       | Bray Central - Herbert Rd/R117      | 3                            | 2445                    | 2453  | 2518  | 2262  | 2456  | 2316   | 4703                    | 4901  | 4700  | 4381  | 4649  | 4387   |
|      | 6a - 7       | Herbert Rd/R117 - Bray South        | 3                            | 2448                    | 2084  | 2560  | 2294  | 2398  | 2159   | 4464                    | 4117  | 4312  | 4345  | 4257  | 3985   |
|      | 7 - 8        | Bray South - Kilmacanogue           | 3                            | 2029                    | 1887  | 1701  | 1874  | 1838  | 1701   | 3583                    | 3489  | 3652  | 3590  | 3257  | 3660   |
|      | 8 - 9        | Kilmacanogue - Glen of the Downs    | 2                            | 1520                    | 1499  | 1529  | 1530  | 1532  | 1529   | 3117                    | 3028  | 3185  | 3124  | 3183  | 3194   |
|      | 9 - 10       | Glen of the Downs - Delgany         | 2                            | 1484                    | 1463  | 1494  | 1494  | 1496  | 1493   | 3082                    | 2995  | 3150  | 3089  | 3148  | 3159   |
|      | 10 - 11      | Delgany - Greystones (Kilpedder)    | 2                            | 1339                    | 1330  | 1350  | 1344  | 1341  | 1353   | 2900                    | 2879  | 2904  | 2903  | 2904  | 2907   |
|      | 11 - 12      | Greystones (Kilpedder) - Newtown MK | 2                            | 1402                    | 1400  | 1403  | 1404  | 1404  | 1404   | 2682                    | 2677  | 2685  | 2682  | 2685  | 2686   |
|      | 12 - 13      | Newtown MK - Newcastle              | 2                            | 1079                    | 1077  | 1080  | 1080  | 1081  | 1080   | 2163                    | 2162  | 2167  | 2164  | 2167  | 2168   |
|      | 13 - 14      | Newcastle - Coynes Cross            | 2                            | 1101                    | 1101  | 1101  | 1101  | 1101  | 1101   | 2375                    | 2375  | 2375  | 2375  | 2375  | 2375   |
| M11  | 14 - 15      | Coynes Cross - Ashford              | 2                            | 1146                    | 1146  | 1146  | 1146  | 1146  | 1146   | 2474                    | 2474  | 2474  | 2474  | 2474  | 2474   |

# **Appendix E**

## **Phasing Options**

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# Phasing Options

## E.1 Proposed Measures

The various proposed measures along the M11/N11 corridor between Junction 4 (M50/M11) and Junction 8 (Kilmacanogue) are illustrated indicatively in Figures E1 to E5.

## E.2 Phasing Implementation

Two phased plans to implement the various measures along the M11/N11 corridor between Junction 5 (M50/M11) and Junction 8 (Kilmacanogue) have been identified as part of this study and are discussed in the following sections.

The final measure of both phasing options considered would see the closure/reconfiguration of direct accesses and left on / left off junctions where possible, along with amendments to existing merges and diverges to comply with the appropriate standard on the section of N11 between Junction 8 (Kilmacanogue) and Junction 14 (Coynes Cross).

### E2.1 Phasing Option 1 (M50 to Kilmacanogue)

Phasing Option 1 which is illustrated in Figure E.6 can be delivered in three phases as follows:

#### *Phase 1*

Phase 1 would see the introduction of services road on a section of the N11 between Junction 7 (Bray South) and Junction 8 (Kilmacanogue). At Junction 8, the southbound lane drop diverge would act as both a diverge lane and southbound service road. In the northbound direction, with a single lane gain closer to Junction 7 which acts as the Junction 8 merge and service road. This means that the mainline speed limit can be raised back to 100km/hr.

#### *Phase 2*

Phase 2 would see the M11 corridor widened to 3 lanes in each direction to Junction 6 Bray South (Fassaroe). Alongside this, Junction 6 would be upgraded by increasing the capacity of the existing roundabouts and bringing the existing merges/diverges up to standard. The upgrading of Junction 6 would allow for the additional demand through the junction to be catered for as a result of the new bridge across the River Dargle linking Upper Dargle Road to Herbert Road.

#### *Phase 3*

The next Phase would see the extension of 3 lanes to Junction 8 (Kilmacanogue). With Phase 2 completed the level of traffic through Junction 6a (east and west of the N11) would reduce as a result of the new bridge across the River Dargle. With the introduction of parallel service roads between Junctions 6 and 7, direct access between Junction 6a and the N11 could be closed thereby improving the capacity and operation of the N11 between Junctions 6 and 7.

The major upgrade to Junction 7 itself would be included as part of this Phase. Also included in this Phase would be the local link road improvements for local movements and network resilience. These include the connection between the M50 J16 (Cherrywood) to Rathmichael/Ballycorus Road Ballycorus Road, and the Ferndale Road improvements.

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### **E.3 Phasing Implementation Option 2 (M50 to Kilmacanogue)**

Phasing Option 2 which is illustrated in Figure E.7 can be delivered in three phases as follows:

#### *Phase 1*

Phase 1 would see the M11 corridor widened to 3 lanes in each direction to Junction 6 Bray South (Fassaroe). Alongside this, the N11 between Junction 6 and Junction 8 would be upgraded to 3 lanes in the southbound direction only (this would also include the southbound services roads between Junction 6a and 7) as no land acquisition is required on the western side of the N11. Phase 1 would also see the introduction of services road on a section of the N11 between Junction 7 (Bray South) and Junction 8 (Kilmacanogue).

#### *Phase 2*

The next Phase would see the N11 upgraded to 3 lanes in the northbound direction between Junction 6 and 8 (this would also include the northbound services roads between Junction 6 and 7) and the upgrading of Junctions 6 and 7. The Dargle River crossing would be included as part of this phase.

#### *Phase 3*

This Phase would include the local link road improvements for local movements and network resilience. These include the connection between the M50 J16 (Cherrywood) to Rathmichael/Ballycorus Road Ballycorus Road, and the Ferndale Road improvements.

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Figure E.1 Summary J4 M50 to J8 Kilmacanogue



### Summary J4 M50 to J8 Kilmacanogue



Figure E.2 Junction 4 M50 to Junction 5 Bray North



### Junction 4 M50 to Junction 5 Bray North

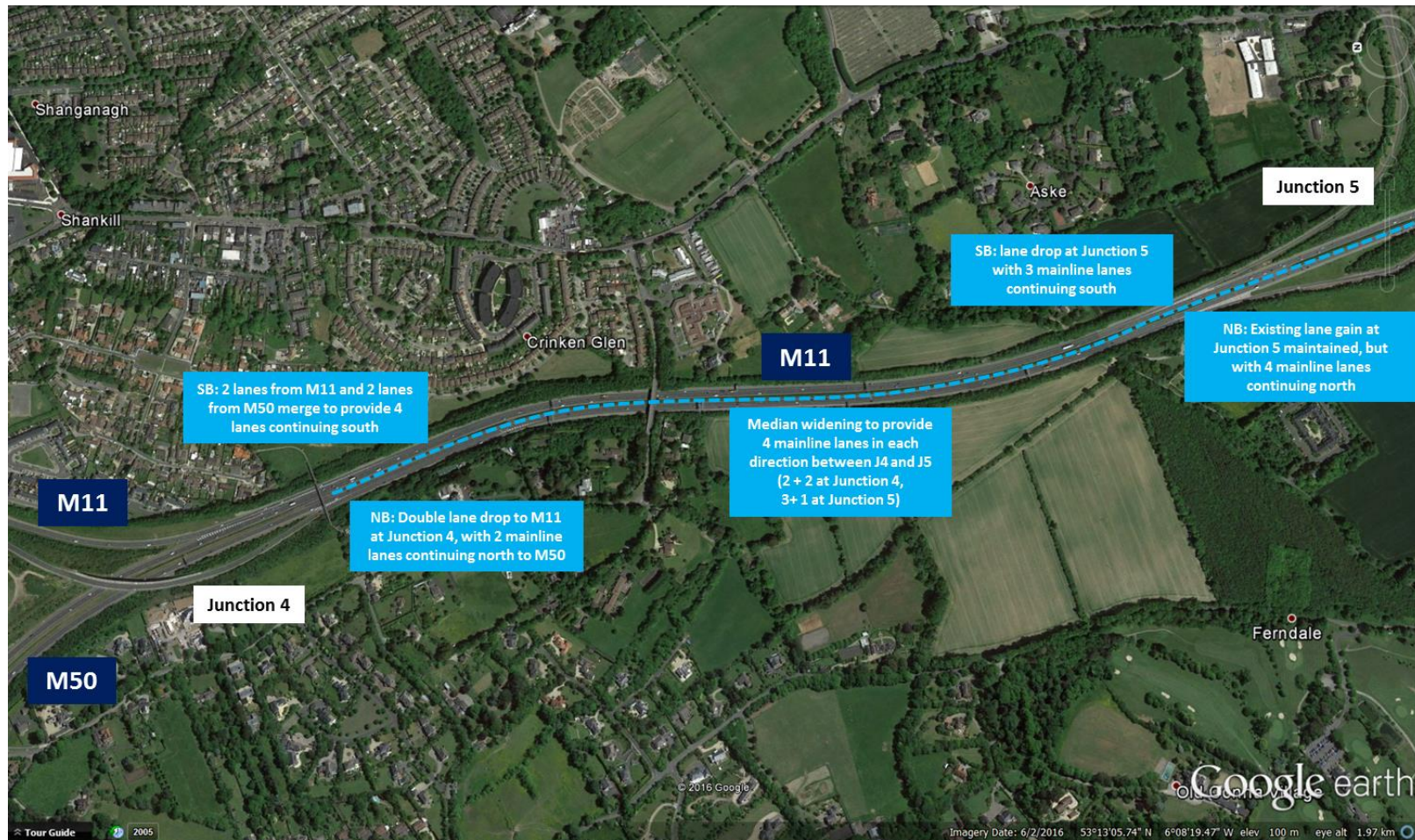




Figure E.4 Junction 6 Bray Central to Junction 7 Bray South



### Junction 6 Bray Central to Junction 7 Bray South



Figure E.5 Junction 7 Bray South to Junction 8 Kilmacanogue



### Junction 7 Bray South to Junction 8 Kilmacanogue

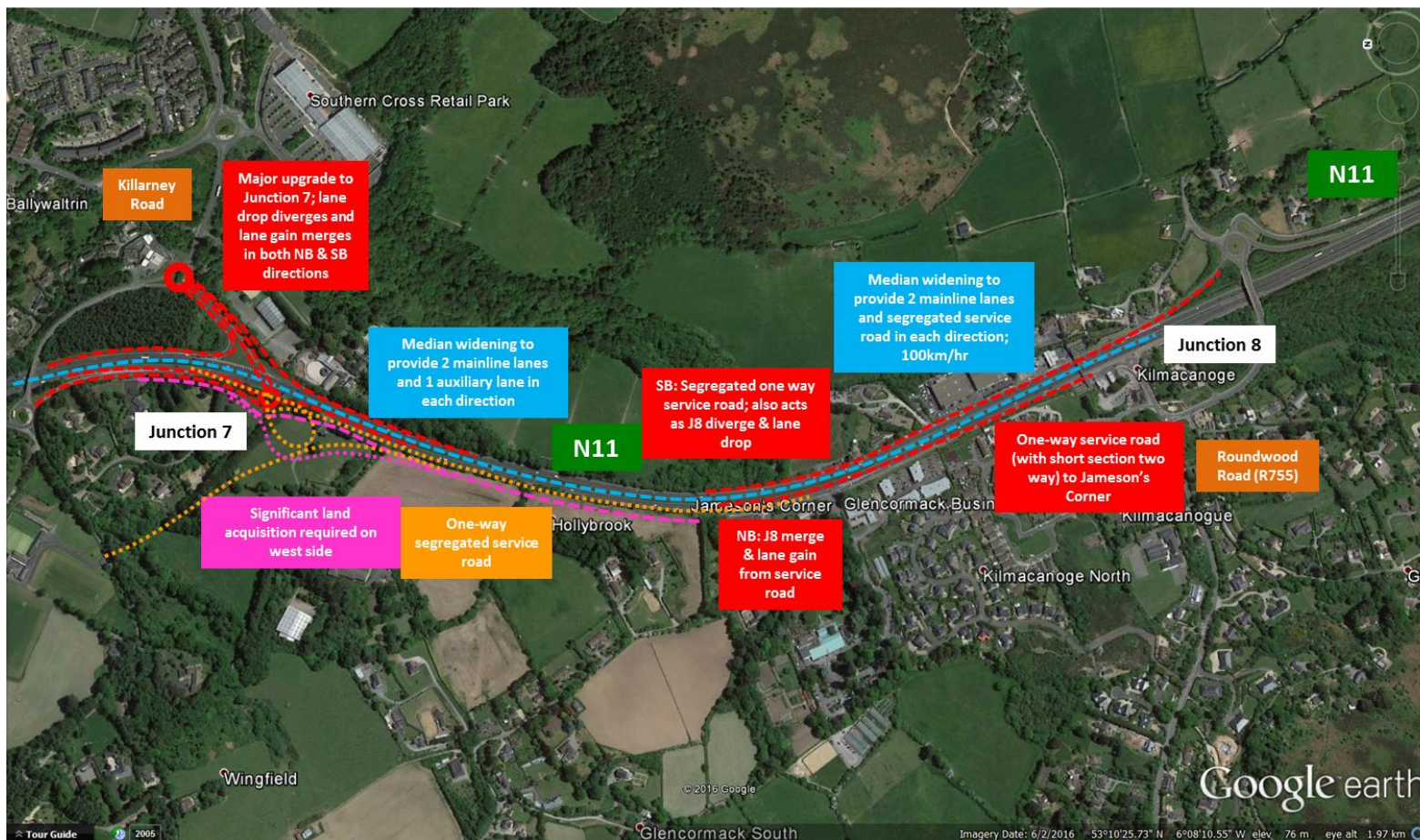


Figure E.6 Phasing Option 1 J4 (M50) to J8 (Kilmacanogue)

# Phasing Option 1 J4 (M50) to J8 (Kilmacanogue)



Figure E.7 Phasing Option 2 J4 (M50) to J8 (Kilmacanogue)

# Phasing Option 2 J4 (M50) to J8 (Kilmacanogue)





